



1987-03

A horizontal spatial requirement study of the Gulf Stream as modelled by the IFDPE acoustic model

Cease, Katherine L.

Monterey, California: U.S. Naval Postgraduate School

<http://hdl.handle.net/10945/22828>



Calhoun is a project of the Dudley Knox Library at NPS, furthering the precepts and goals of open government and government transparency. All information contained herein has been approved for release by the NPS Public Affairs Officer.

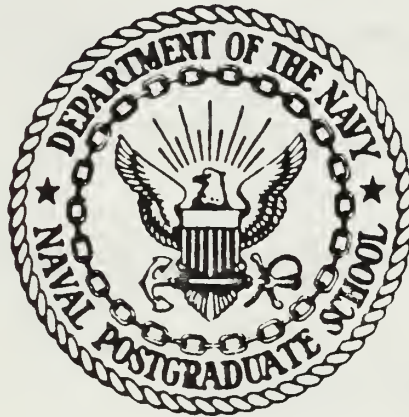
Dudley Knox Library / Naval Postgraduate School
411 Dyer Road / 1 University Circle
Monterey, California USA 93943

<http://www.nps.edu/library>

DUDLEY CHURCH LIBRARY
NAVAL POST OFFICE
MONTELEONE, CALIF. 95002

NAVAL POSTGRADUATE SCHOOL

Monterey, California



THESIS

A HORIZONTAL SPATIAL REQUIREMENT
STUDY OF THE GULF STREAM AS
MODELLED BY THE IFDPE ACOUSTIC MODEL

Katherine L. Cease

//

March 1987

Thesis Advisor:

Alan B. Coppins

Approved for public release; distribution unlimited

Prepared for:
Naval Postgraduate School
Monterey, CA 93943

T232256

Thesis
C 338343
c.1

NAVAL POSTGRADUATE SCHOOL
Monterey, Ca. 93943

Rear Admiral R. C. Austin
Superintendent

David A. Schradz
Provost

This thesis is prepared in conjunction with research sponsored in part by Naval Oceanographic and Research Activity.

Reproduction of all or part of this report is authorized.

REPORT DOCUMENTATION PAGE

REPORT SECURITY CLASSIFICATION CLASSIFIED			1b RESTRICTIVE MARKINGS		
SECURITY CLASSIFICATION AUTHORITY			3 DISTRIBUTION/AVAILABILITY OF REPORT Approved for public release; distribution unlimited		
DECLASSIFICATION/DOWNGRADING SCHEDULE					
PERFORMING ORGANIZATION REPORT NUMBER(S) S61-87-005			5 MONITORING ORGANIZATION REPORT NUMBER(S)		
NAME OF PERFORMING ORGANIZATION Naval Postgraduate School		6b OFFICE SYMBOL (If applicable) 61	7a NAME OF MONITORING ORGANIZATION Naval Postgraduate School		
ADDRESS (City, State, and ZIP Code) Monterey, California 93943-5000			7b ADDRESS (City, State, and ZIP Code) Monterey, California 93943-5000		
NAME OF FUNDING/SPONSORING ORGANIZATION ORDA		8b OFFICE SYMBOL (If applicable) 323	9 PROCUREMENT INSTRUMENT IDENTIFICATION NUMBER		
ADDRESS (City, State, and ZIP Code) St. Louis, Ms. 39529			10 SOURCE OF FUNDING NUMBERS		
			PROGRAM ELEMENT NO	PROJECT NO	TASK NO
			WORK UNIT ACCESSION NO		
TITLE (Include Security Classification) HORIZONTAL SPATIAL REQUIREMENT STUDY OF THE GULF STREAM AS MODELLED BY THE IFDPE ACOUSTIC MODEL					
PERSONAL AUTHOR(S) Case, Katherine L. in conjunction with Coppens, Alan B./ King, David					
TYPE OF REPORT Master's Thesis		13b TIME COVERED FROM TO	14 DATE OF REPORT (Year, Month, Day) 1987 March		15 PAGE COUNT 143
SUPPLEMENTARY NOTATION					
COSATI CODES			18 SUBJECT TERMS (Continue on reverse if necessary and identify by block number)		
FIELD	GROUP	SUB-GROUP	IFDPE Model, Acoustic Models, Gulf Stream Transmission Loss, Spatial Resolution		
ABSTRACT (Continue on reverse if necessary and identify by block number)					
The sampling increment in horizontal spacing for a range-dependent environment was studied with respect to accurate prediction of propagation loss through a frontal system. A transmission loss model was verified by comparing its predictions with experimental data when the sampling increment was very small. A study of the effect of altering the sampling increment produced a maximum increment which retained a reasonable agreement with the prediction for very small incrementation. Sensitivity studies were performed at three source depths to determine depth dependency.					
DISTRIBUTION/AVAILABILITY OF ABSTRACT <input checked="" type="checkbox"/> UNCLASSIFIED/UNLIMITED <input type="checkbox"/> SAME AS RPT <input type="checkbox"/> DTIC USERS			21 ABSTRACT SECURITY CLASSIFICATION UNCLASSIFIED		
NAME OF RESPONSIBLE INDIVIDUAL Alan B. Coppens			22b TELEPHONE (Include Area Code) (408) 646-2941	22c OFFICE SYMBOL 61Cz	

Approved for public release: distribution unlimited.

A Horizontal Spatial Requirement Study of
the Gulf Stream as Modeled by the IFDPE Acoustic Model

by

Katherine Leann Cease
Lieutenant, United States Navy
B.A., University of Louisville, 1981

Submitted in partial fulfillment of the
requirements for the degree

MASTER OF SCIENCE IN SYSTEMS TECHNOLOGY
(Antisubmarine Warfare)

from the

NAVAL POSTGRADUATE SCHOOL
March 1987

ABSTRACT

The sampling increment in horizontal spacing for a range-dependent environment was studied with respect to accurate prediction of propagation loss through a frontal system. A transmission loss model was verified by comparing its predictions with experimental data when the sampling increment was very small. A study of the effect of altering the sampling increment produced a maximum increment which retained a reasonable agreement with the prediction for very small incrementation. Sensitivity studies were performed at three source depths to determine depth dependency.

TABLE OF CONTENTS

ACKNOWLEDGEMENT_ _ _ _ _	5
I. INTRODUCTION_ _ _ _ _	6
II. BACKGROUND AND DEVELOPMENT OF IFDPE _ _ _ _ _	12
A. PARABOLIC EQUATION_ _ _ _ _	12
B. IFDPE MODEL_ _ _ _ _	14
C. SAMPLE IFDPE OUTPUT_ _ _ _ _	16
III. MODEL VERIFICATION_ _ _ _ _	19
A. GSFE _ _ _ _ _	19
B. VERIFICATION PROCEDURE_ _ _ _ _	20
C. RESULTS_ _ _ _ _	21
IV. HORIZONTAL SPATIAL REQUIREMENT STUDY_ _ _ _ _	29
A. IFDPE INPUT RUNSTREAM_ _ _ _ _	33
B. SENSITIVITY STUDIES_ _ _ _ _	35
C. HISTOGRAMS_ _ _ _ _	36
V. RESULTS_ _ _ _ _	40
VI. CONCLUSIONS_ _ _ _ _	43
APPENDIX A GSFE EXPERIMENTAL DATA_ _ _ _ _	46
APPENDIX B SOUND SPEED INTERPOLATION METHOD_ _ _ _ _	80
APPENDIX C SAMPLE SSP INTERPOLATIONS_ _ _ _ _	84
APPENDIX D PLOTTING METHODS_ _ _ _ _	107
APPENDIX E TL DIFFERENCE GRAPHS_ _ _ _ _	109
APPENDIX F HISTOGRAMS_ _ _ _ _	123
LIST OF REFERENCES_ _ _ _ _	138
INITIAL DISTRIBUTION LIST_ _ _ _ _	140

ACKNOWLEDGEMENT

There are numerous people without whom this report could not have been written. The people I worked with at NORDA made my stay there a most pleasant one and contributed significantly to the completion of my research. Tracy Frieze and Curtis Fabre were instrumental in various program re-writes and program implementation. George Kerr provided the answers to some sticky oceanographic questions and Bob McGirr helped out at the last minute with the sound speed field interpolation routine. Thanks also to Dr. George Heburn of the Tactical Oceanography Program. Dave and Portia King not only made my professional stay at NORDA a rewarding one but made my personal stay a comfortable one by inviting me into their home. To them, my utmost thanks.

And last, but most definitely not least, thanks to my sectionmates of IX53 who provided the right amount of zaniness to get through Postgraduate School, without sacrificing their professionalism.

I. INTRODUCTION

The commander at sea is required to have the most up-to-date environmental information available to enhance his use of ASW performance prediction systems. Accurate environmental information enables the acoustic models in the ASW system to accurately predict the propagation track of acoustic energy and thus allow optimum deployment of acoustic sensors.

Transmission loss models require environmental data as input. The more accurate the environmental input, the more accurate the simulation of acoustic propagation will be. This study is concerned with the trade-off between predictive accuracy and accuracy of the environmental input to an acoustic model.

Environmental inputs to an acoustic model consist of representations of the speed of sound profiles, bottom topography, bottom composition, and sea surface roughness as functions of space. This study will be concerned with the required spacing in range of the speed of sound profiles. Sound-speed profile data exist in the form of climatology, historical information, and on-scene XBT (Expendable Bathythermograph) and XSV (Expendable Velocimeter) readings. On-board ASW acoustic predictive systems currently use range-

independent acoustic models. These models accept only one SSP (sound speed profile), a flat ocean bottom, and a single bottom description. The next level of sophistication of acoustic modelling is range dependency. Range-dependent models require realization of the environment as a function of range. The goal of this study is to contribute to the support of range-dependent models.

Systems now available cannot provide on-board, real-time information that the operational commander can use in complex ocean environments. Usually, data collected by platforms are sent to a shore-based facility to be entered into a model which is then run and the results transmitted back. During this interval, the tactical situation can change significantly. What is required is a method of performing these calculations on board and in a timely fashion. The next generation of platform systems should provide this capability, in-situ.

Range-dependent modelling requires a considerable amount of input data. One method of supplying such data is ocean dynamic modelling. It is planned to combine maturing technologies into a system that will ultimately produce information for use in tactical scenario models. (See Fig. 1.) Data from in-situ and remote sensors will be fed into dynamic ocean models

which will then produce information used in acoustic models and then into tactical scenario models. The general question pertinent to this study is the determination of the amount of information required from the ocean dynamic models. The question is a broad one; this study examines one specific aspect of the general environmental question. What is the maximum spacing in the horizontal sound speed field that can yield an acceptably accurate acoustic field?

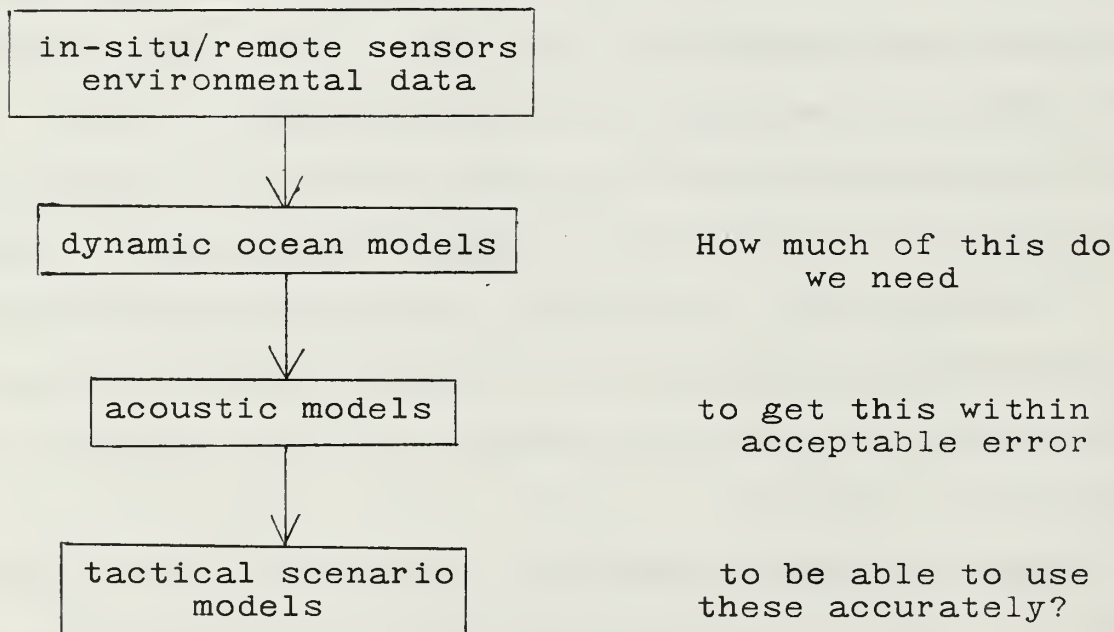


Figure 1. Combining Maturing Technologies

Current acoustic performance prediction systems, such as ICAPS (Integrated Carrier Acoustic Prediction System) and SIMAS (Sonar In-Situ Mode Assessment System), incorporate the range-independent model RAYMODE. As the systems are upgraded, a new generation of software will include the range-dependent models. This requires a more detailed environmental data base than we now have.

Specifically, we must know what is the cost in acoustic predictive accuracy if we go to larger and larger spacings in the sound speed field, both horizontally and vertically (vertical resolution is not the subject of this study). Tactical cost, computer memory and execution time are key factors, but also because use of such models is scenario dependent. Each scenario may require different spatial resolutions. A resolution too fine is a waste of valuable resources; a resolution not fine enough may affect tactical operations.

Once the problem had been defined, a procedure was needed to solve the problem. Because this study concerned the extraction of environmental data for the purpose of predicting acoustic performance, it was essential to find an environment suitable for use.

In determining what was important in horizontal spacing, an environment was chosen that would describe

a worst-case scenario. Sharp gradients found in large oceanic frontal systems (e.g. the Gulf Stream) pose unique problems, as well as require a more exacting description of the environment. Such an environment was found in the Gulf Stream Frontal Experiment (GSFE, Ref. 1). In addition to the experiment being carried out in a frontal region, acoustic data were simultaneously obtained which were valuable in the model verification (see Chapter Three).

Once an environment was chosen, the IFDPE (Implicit Finite Difference Parabolic Equation) Model (Ref. 2) was chosen for the horizontal spatial requirement study. IFDPE satisfies several requirements: 1) it is range-dependent, 2) it does not have any limitations on the amount of environmental data (other than machine limitations) input, 3) it has a good reputation for handling complex environments, and 4) it produces a full simulation of the acoustic field at all depths and ranges.

Finally, a procedure was established to complete the mechanics of the study in the form of computer program execution and analysis. The history of the IFDPE model had shown its utility and accuracy, but this was verified to ensure it was the "right tool for the job". Input files were established (more detail in Chapters Two and Four) and executed based upon a

uniform range spacing and using the 2 km resolution as a baseline.

This report breaks down into further chapters with accompanying appendices. Chapter Two details the history of the IFDPE model and why it was the model of choice for this study. Chapter Three details the verification of the model. Chapter Four details the interpolation of SSPs required, the candidate range spacings chosen for program execution, and the graphical output from the model. It also covers in detail the IFDPE input runstream and the sensitivity studies that were performed. Chapter Five analyzes the results of the statistical output of transmission loss difference graphs based upon criteria arbitrarily established by the authors. Chapter Six gives a brief conclusion to the study, inviting areas for further research.

II. BACKGROUND AND DEVELOPMENT OF IFDPE

Most current operational acoustic models used are range independent and cannot adequately describe the acoustic field.

Some models, such as Critical Angle PE (Parabolic Equation), PAREQ (Ref. 3, 4), and IFDPE are range dependent. Critical Angle PE does not handle bottom interaction well (it is poor for bottom bounce conditions); PAREQ handles bottom interaction well but not as well as IFDPE. IFDPE deals well with bottom interactions. More recently, other models such as RAREQ (Range Refraction Parabolic Equation) and the wide-angle IFDPE range dependent models have been developed (Ref. 5, 6).

Determining the path and strength of an acoustic signal requires solving the wave equation or an approximation to it. One of the easier approaches to an approximate solution is the parabolic equation approximation.

A. THE PARABOLIC EQUATION

The parabolic equation approximation is derived by assuming an acoustic pressure field of constant frequency. This reduces the wave equation to the time

independent Helmholtz equation. Assuming cylindrical symmetry, applying some range restrictions, and assuming that the variation of sound speed profile and bottom properties are sufficiently gradual, reduce the Helmholtz equation to a parabolic wave equation (Ref. 7).

The parabolic approximation is equivalent to neglecting backscattering since the values for small r (range) are not dependent upon the subsequent values obtained for larger r (Ref. 7).

Solutions to this parabolic equation may be found by incrementally increasing range ("stepping out the range solution") and solving because now "the entire acoustic field does not need to be solved for all relevant ranges and depths 'simultaneously' subject to boundary conditions on a surface surrounding the volume of interest" (Ref. 7).

One of the limitations of the simpler PE model is that the source angle is restricted to ± 20 degrees, after which the approximation breaks down. This is a narrow beam width, and energy passing out of this angle cannot be accounted for. Extensions of the PE allow for ± 40 degrees but are presently not implemented in operational TL models.

An early solution to the parabolic equation, introduced by Tappert and Hardin, was the split-step

Fast Fourier Transfer algorithm. This method is fast and accurate when the field interacts only weakly with the ocean bottom. It is less accurate when the field reacts strongly with the bottom; it has difficulty handling density or sound speed differences between two media (Ref. 2). The latter difficulty can be overcome but only with very long computer execution time.

B. IFDPE MODEL

In 1975, the Crank-Nicholson implicit finite difference (IFD) method for solving the parabolic equation was introduced by Lee and Papadakis. An IFD method was chosen over an explicit finite difference solution because the IFD solution is unconditionally stable, consistent, and converges to the theoretical solution as the range and depth increments tend to zero (Ref. 8). The IFDPE solution based upon the Crank-Nicholson method uses a second order central difference formula and places the problem in the form of a tridiagonal matrix.

The model chosen for this acoustic study is the IFDPE (Implicit Finite Difference Parabolic Equation) Model (Ref. 2). The program was written in Fortran for use on the VAX-11/780 computer.

The IFDPE model used in this study is the wide-angle version (Ref. 9) which allows a beam angle of +/-

40 degrees and thus enable the user to generate output for near-field study. (However, energy still escapes from this beamwidth which cannot be accounted for and thus is a drawback to IFDPE.) Technically, this version is no longer in parabolic equation form, but a pseudo-partial differential equation. The acoustic modelling community uses the PE nomenclature for this model and this report adheres to this convention.

The model can handle the following environments:

- 1) range dependent/range independent
- 2) shallow water/deep water
- 3) shallow-to-deep water, deep-to-shallow water, or the combination

IFDPE essentially solves the problem in layers: a water column underneath a pressure-release surface; a water-bottom interface: multiple layers in the bottom, and; an artificial acoustic basement (absorptive layer) overlying a pressure-release boundary. Both a pressure release surface boundary condition and a pressure release boundary condition at the greatest retained depth are required to terminate the solution within a finite depth interval. The basement attenuates the energy so that it is negligibly small when it encounters the bottom pressure release boundary. This ensures negligible spurious reflection back into the water column.

Each layer used in IFDPE contains an arbitrary sound speed structure (sound speed profiles provided by the user), constant density and constant attenuation.

Once the layers are defined, a program known as SSPBT (developed by NORDA oceanographers) couples the geoacoustic bottom to the water column to produce an input format easily manageable for use in creating input files for IFDPE.

C. SAMPLE IFDPE OUTPUT

Once the entire IFDPE input file is established (Chapter Four, Section A), the program is executed. Output is for all depths and ranges of the acoustic field. A sample grayscale plot is shown in Fig. 2. The darkest gray dot corresponds to a transmission loss of 100 dB or greater, decreasing in 10 uniform levels to the lightest shade of gray which represents losses of 50 dB or less.

Some features of this graph are readily apparent: the relatively flat ocean bottom at 5000 m depth, the energy propagating into the sediment layers to a depth of about 7000 m, the first convergence zone between 50 and 60 km, and the ray paths the acoustic energy followed. Also notable are the very black triangles near the source (one at the surface at around 10 km, the other penetrating down into the sediment from 0-10

km). These are areas where the acoustic energy could not be accounted for because of the source angle limitation in IFDPE. At larger range, this high angle energy would be greatly attenuated by multiple reflections from the bottom. Its absence thus does not significantly affect the sound field.

GULF STREAM 2KM RESOLUTION

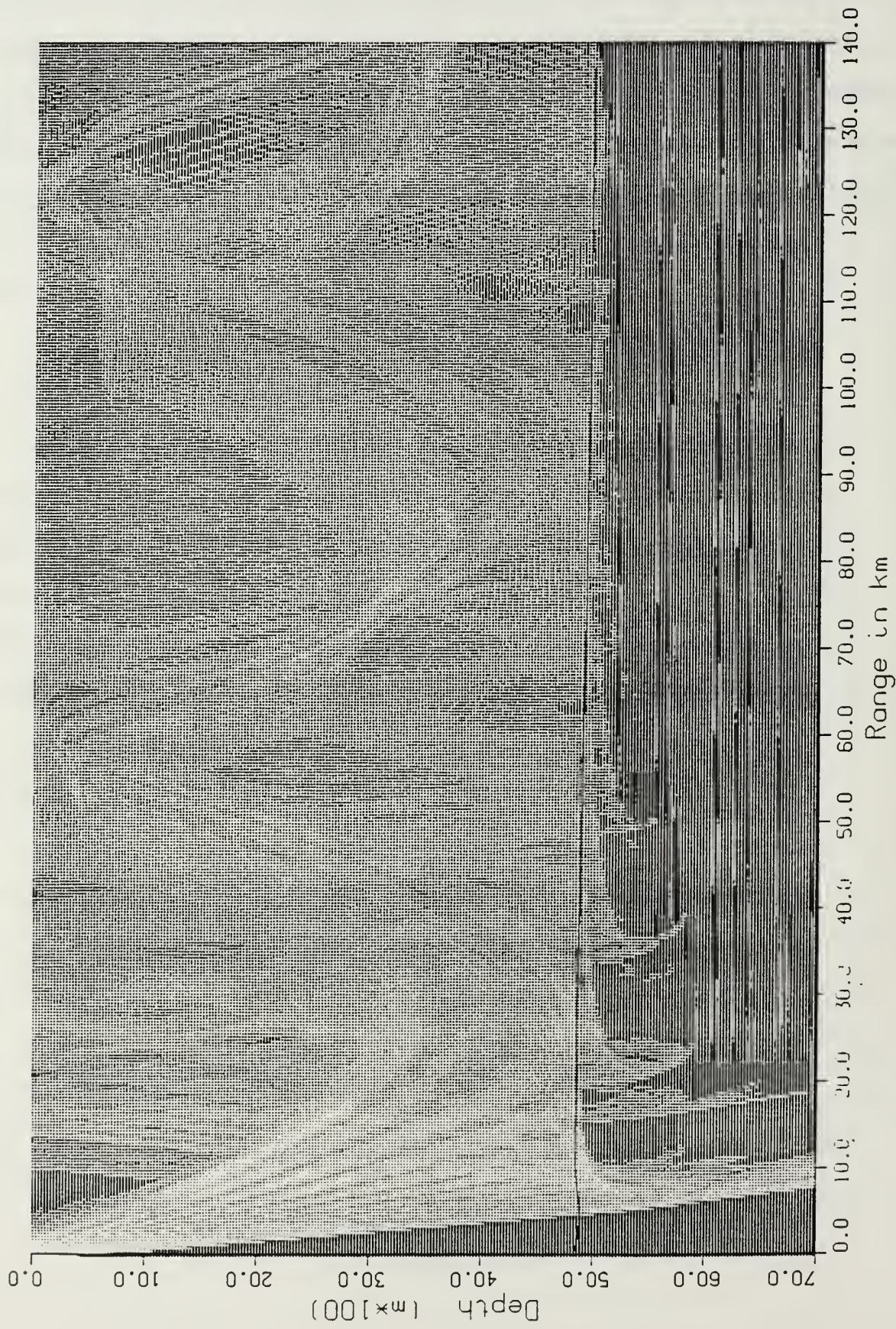


FIG. 2 Grayscale Plot 2 km Baseline Resolution

III. MODEL VERIFICATION

To ensure that the model used was appropriate for predicting acoustic propagation through the Gulf Stream, IFDPE was tested by comparing its predicted transmission loss with that measured from the NORDA/NUSC GSFE (Gulf Stream Frontal Experiment, Ref. 1). GSFE did two things--it provided the environmental data the study required and the transmission loss values needed for the computer model runs and analysis.

A. GSFE

The purpose of GFSE was to acquire an environmental/acoustic data set to evaluate the impact of the Gulf Stream frontal boundaries (North Wall and South Edge) on ASW/USW platform and weapons sonar systems performance.

Two ships were used--one as a source platform (using a multi-frequency transducer assembly capable of transmitting signals at two frequencies simultaneously), the other as a receiving platform using a six-hydrophone vertical line array (Fig. 3). Four tracks were laid out--three travelling through the Gulf Stream; the fourth, south in the Sargasso Sea (Fig. 4).

The source ship opened and closed range radially with the receiving array. It also conducted extensive XBT and XSV samplings of the various water masses. XBT drops from the receiving vessel were made about every two hours and at least one SST/SSP cast at each station.

Only data generated by the 310 Hz source were used for the verification test for two reasons: 1) higher frequencies require much longer program execution time (on the order of several hours on the VAX-780), and 2) if the model proved valid at 310 Hz, then it would also be valid at the lower frequency of 100 Hz used for this study.

B. VERIFICATION PROCEDURE

The environmental data for the four tracks (SSPs and bathymetric profiles) were first merged to create four input files for IFDPE program execution using SSPBT. SSPBT links the geoacoustic bottom data with oceanographic data for the particular area of the North Atlantic being studied (Table 1). SSPBT merges the SSP at its specific bathymetric point with the ocean bottom to provide continuity with the travelling acoustic wave, i.e. it couples the geoacoustic bottom to the water column. Once the data were merged, each track profile was then run through the IFDPE model. A plot

of transmission loss versus range was generated and compared to the measured TL plots provided by GSFE.

Comparisons between model TL output and GSFE environmental data are shown in Figures 5-8.

C. RESULTS

The model fits the data well. The measured data were extracted from the GSFE TL graphs and plotted on the same axes as the TL values predicted by the model. Since the measured data were available only in graphic form, some error was introduced, but it should not be significant. The GSFE data points fit well as is evident from a visual examination of each graph.

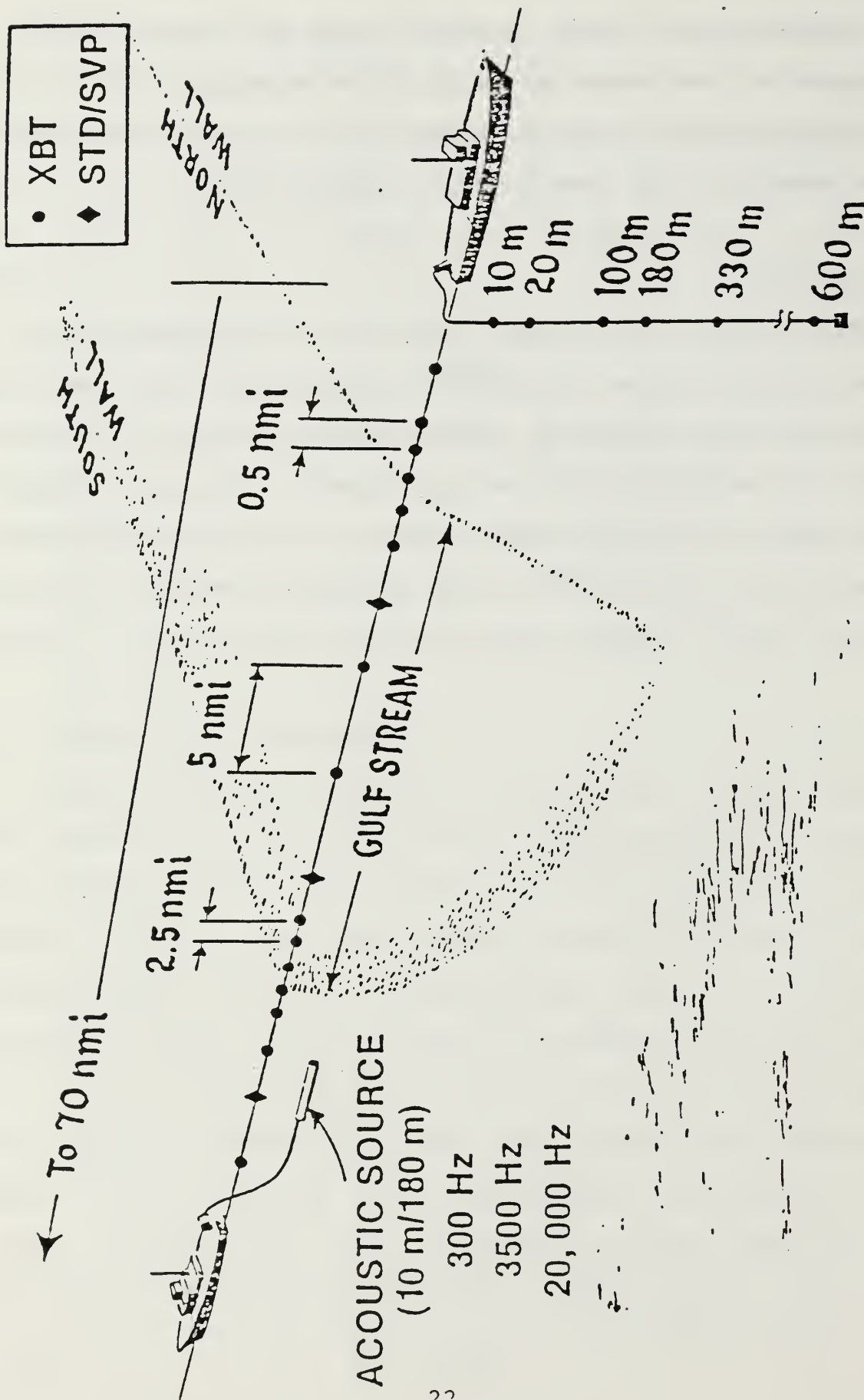


FIG. 3 GSFE Set-up (NUSC TM 811054)

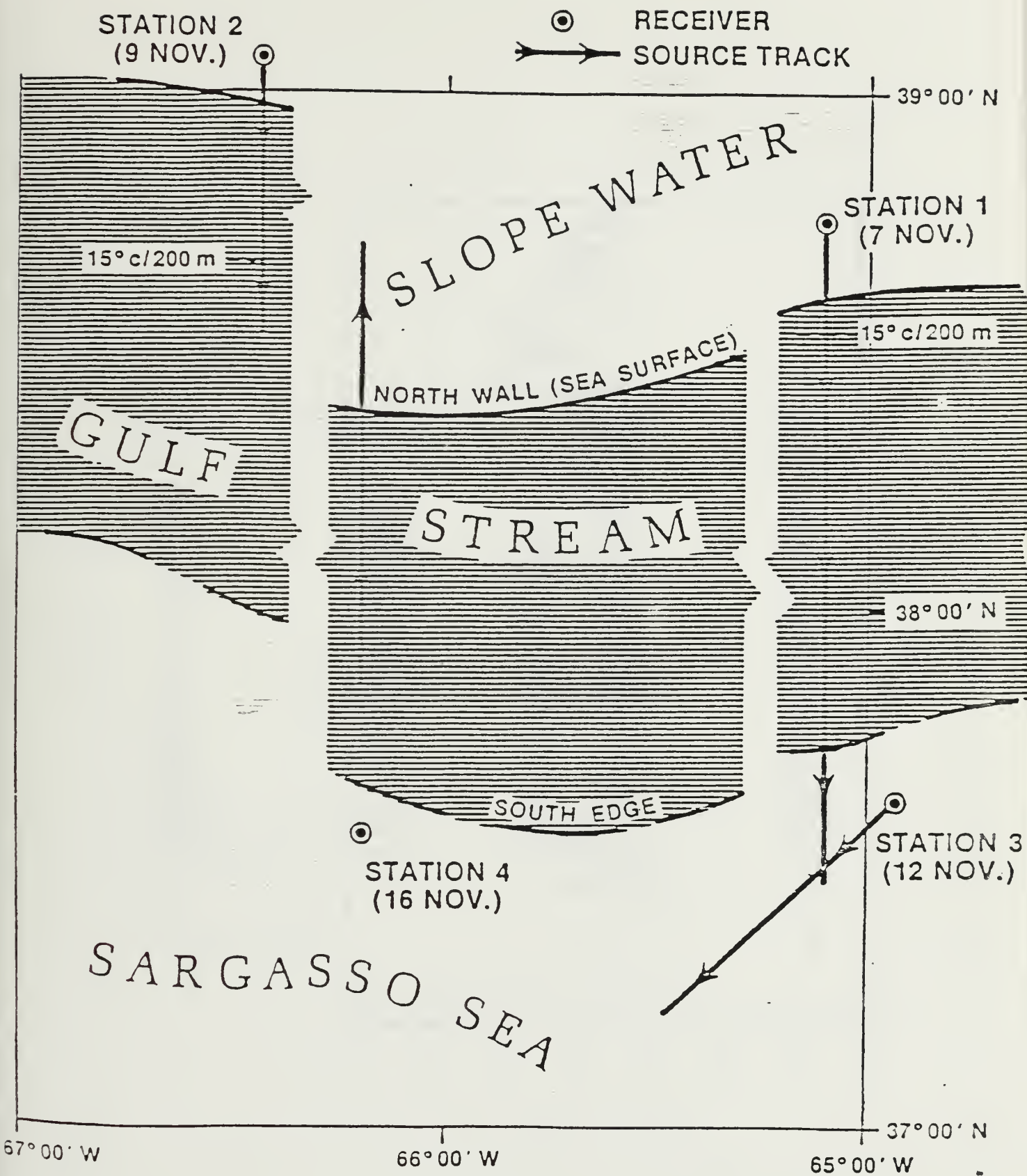


FIG. 4 GSFE Tracks Lay-out (NUSC TM 811054)

TABLE 1

GEOACOUSTIC BOTTOM MODEL			
DEPTH	VELOCITY	ATTENUATION	DENSITY
M	M/SEC	DB/HZ/KM	G/CC
0	1487	.0045	1.50
25	1519	.0060	1.53
50	1550	.0075	1.57
75	1581	.0090	1.60
100	1610	.0110	1.64
125	1638	.0120	1.67
150	1665	.0130	1.70
175	1691	.0140	1.73
200	1716	.0150	1.76
250	1763	.0170	1.81
300	1805	.0190	1.86
350	1842	.0195	1.90
400	1874	.0190	1.94
500	1922	.0160	1.99
600	1952	.0130	2.03
800	2012	.0130	2.16
1000	2072	.0130	2.16

IFD SOLUTION: TRACK ONE

INITIAL PARAMETERS

FRQ - 310.00 HZ

ZS - 150.00 M

N - 9500.00

DR - 2.00 M

DZ - 1.00 M

AVG - 100.00 M

RECEIVER DEPTH - 105.00 M

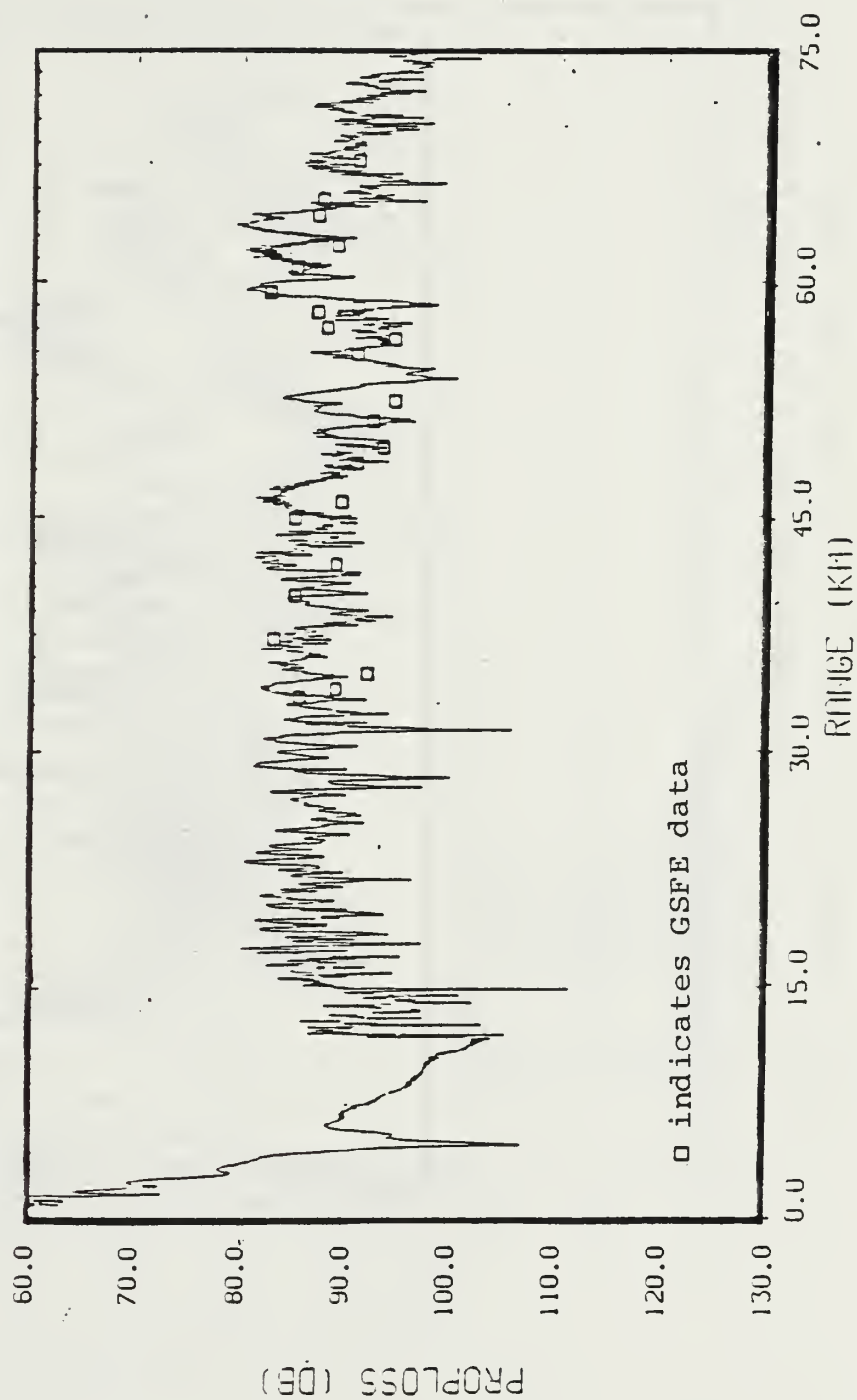


FIG. 5 Model TL vs Experimental Data Track One

IFD SOLUTION: TRACK TWO

INITIAL PARAMETERS

FRO - 310.00 HZ

ZS - 170.00 M

II - 9500.00

DR - 2.00 M

DZ - 1.00 M

AVG - 100.00 M

RECEIVER DEPTH - 30.00 M

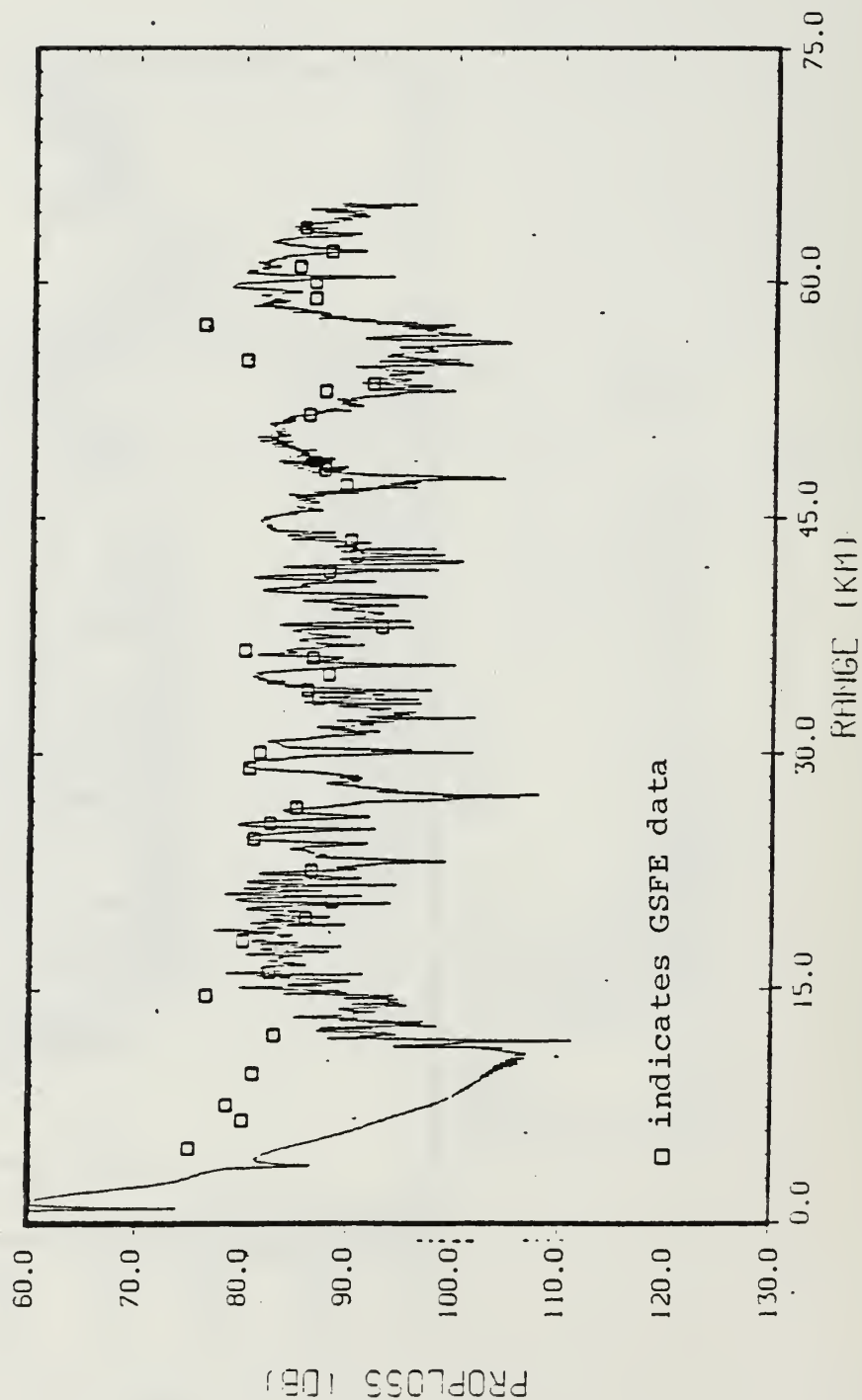


FIG. 6 Model TL vs Experimental Data Track Two

IFD SOLUTION: TRACK THREE

INITIAL PARAMETERS

FRQ - 310.00 HZ
 ZS - 180.00 H
 H - 9900.00
 DR - 2.00 H
 DZ - 1.00 H
 AVG - 100.00 H
 RECEIVER DEPTH - 30.00 H

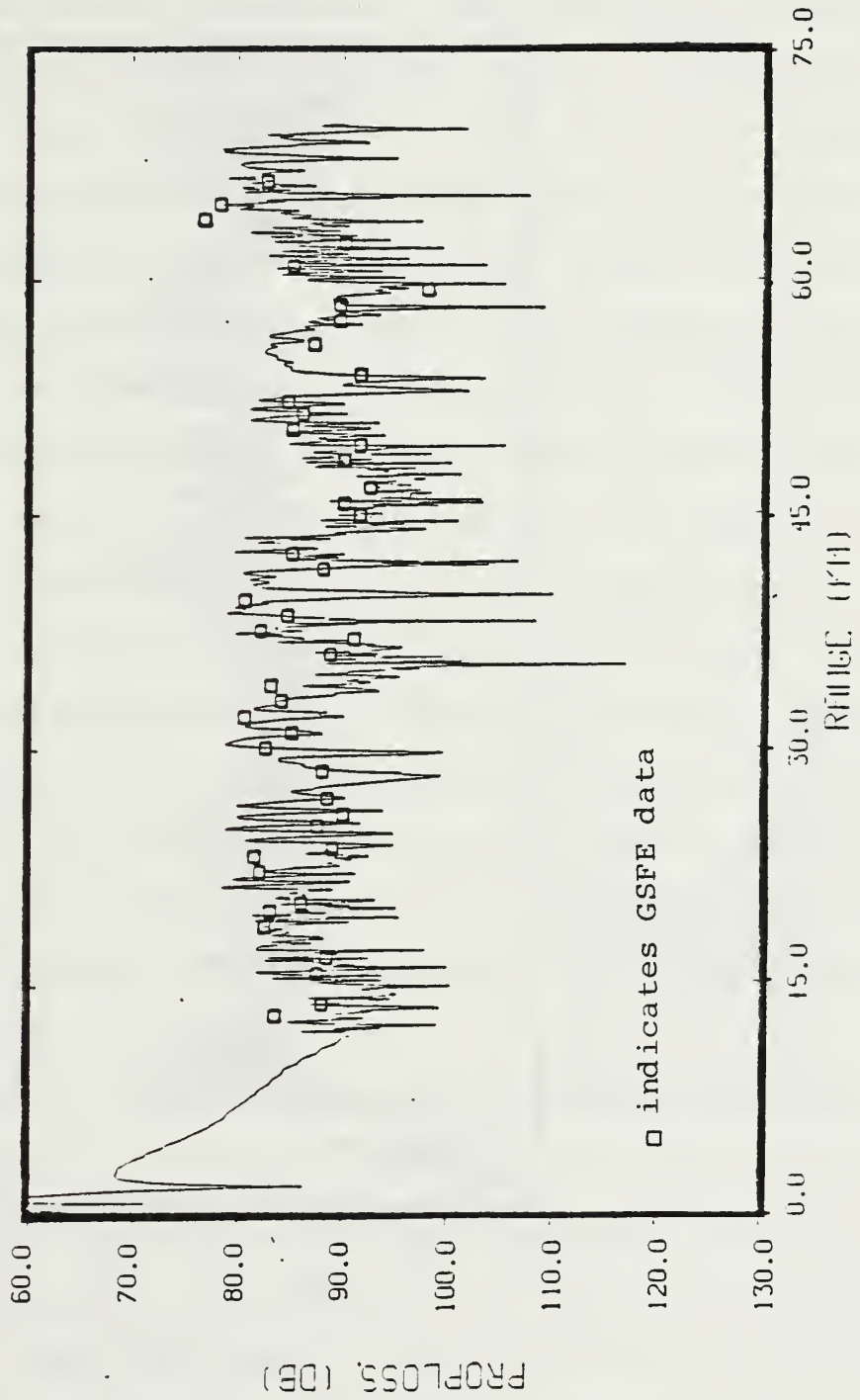


FIG. 7 Model TL vs Experimental Data Track Three

IFD SOLUTION: TRACK FOUR

INITIAL PARAMETERS

FRO - 310.00 HZ

ZS - 180.00 H

II - 9500.00

OR - 2.00 H

OZ - 1.00 H

IVG - 100.00 H

RECEIVER DEPTH - 330.00 M

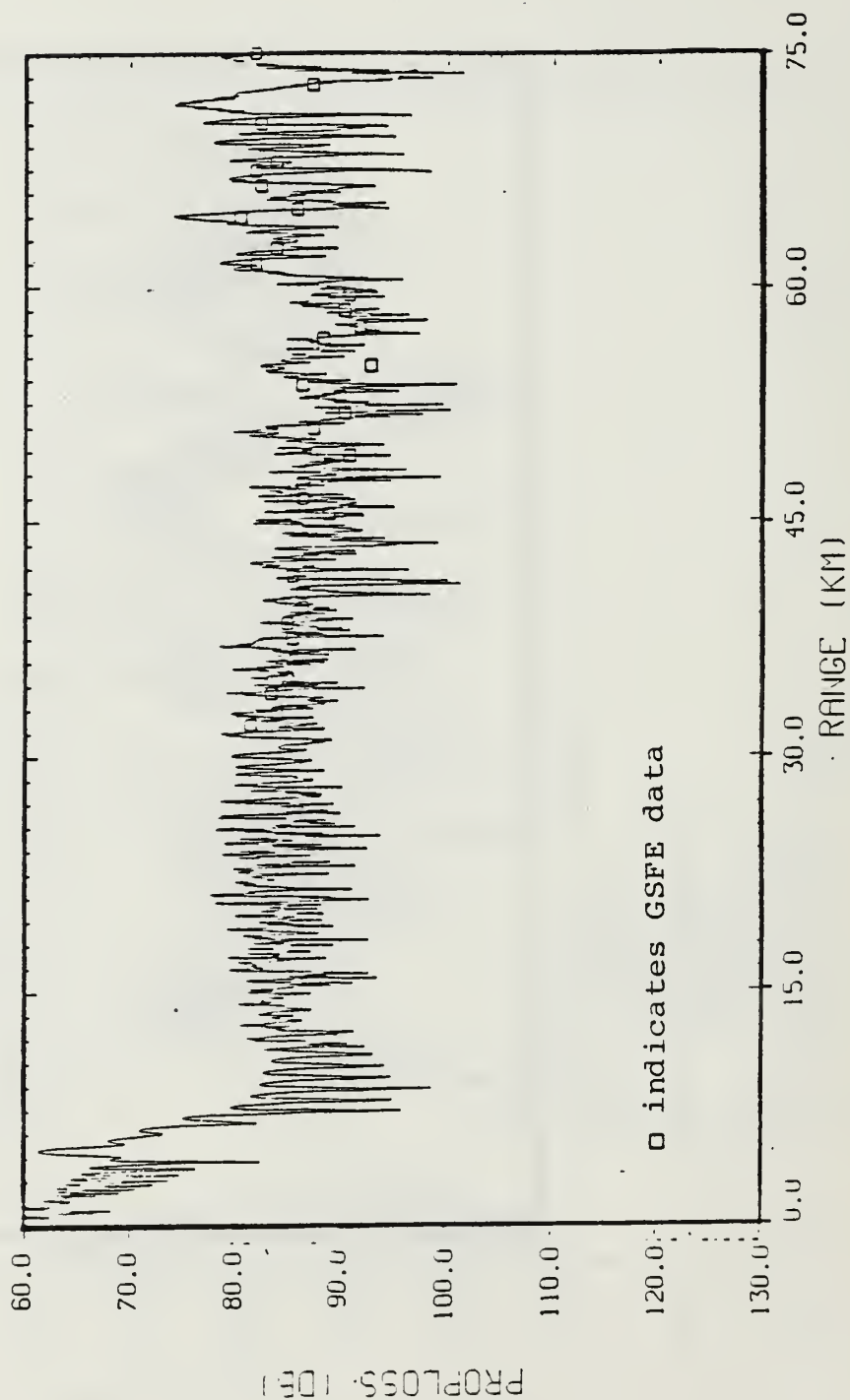


FIG. 8 Model TL vs Experimental Data Track Four

IV. HORIZONTAL SPATIAL REQUIREMENT STUDY

With verification complete, the resolution study began. However, some problems were encountered immediately. Practical considerations dictated that only one track be used to perform the study. Track One was chosen because it ran from the Slope Water into and through the Gulf Stream and entered the Sargasso Sea. It was also chosen because it presented the most complex sound speed field of the environments. The measured SSPs were not uniformly spaced in range, so they had to be supplemented by a sound speed profile interpolation routine (CFIELD, Appendix B, a part of RAYWAVE II, Ref. 10) to provide SSPs at uniform range intervals. SSPs were thus obtained at roughly two km intervals over the approximately 150 km range covered. There were 18 experimental SSPs and an additional 49 SSPs were interpolated (see Appendix C for a sampling of interpolated profiles).

After careful examination of each SSP, including those interpolated, the North Wall of the Gulf Stream was determined to be at 25.9 km downrange from the first SSP. No sea surface temperature (SST) data were available, so the location of the North Wall was determined strictly from the SSPs (Ref. 11). The profiles showed that the Gulf Stream's South Edge was

not easily identifiable because it was not well-defined. However, it appeared to be at approximately 77 km from the initial SSP taken and this was the value used (Ref. 11).

For this study, a 100 Hz source was placed at depths of 100 m, 500 m, and 1000 m.

The candidate range spacings included executing IFDPE input files established at 2, 4, 6, 8, 10, 20, 30, and 60 km. A 2 km spacing was chosen as the baseline spacing for numerous reasons. First, the model requires large computer memory and any finer resolution would probably be (and, indeed was found to be) overkill. Second, the oceanography is not well known at any finer resolution. Third, only oceanographic models can support such a fine resolution. The spacings chosen for the 10-30 km range were for reasons of economy but had to include the 25 km range because this was the position of the North Wall of the Gulf Stream. It was necessary to keep the North Wall and the first sound speed profile fixed so that errors would not be introduced because of their manipulation. Every 30 km was sampled to determine how the static data base would handle the horizontal requirement. Finally, a 60 km sample was chosen to simulate the Navy standard data base which is resolved to 0.5 degrees.

Once the SSPs needed were interpolated, they were combined with the original SSPs to form the first part of the input files required to run the IFDPE model. Each input file was created using the Track One profiles at range spacings of 2, 4, 6, 8, 10, 20, 25, 30, and 60 km. In addition to the 2 km baseline, range spacings were obtained by deleting baseline sound speed profiles that occurred between the desired spacings. For example, the 4 km sample was generated by deleting every other sound speed profile. Each sample was then processed according to the method established in the verification procedure.

For each sample resolution chosen, the distances between successive profiles were not exact, as shown in Table 2. Table 2 lists the ideal sample distances versus the true average distance actually computed and used in the study.

As the spacings were opened up (grosser resolution), it was critical that the field be produced on the same size grid (otherwise, TL differencing would not be possible). This indicated how well the field was resolved. In each input runstream (see below), therefore, depth and range grid spacing were kept constant.

Each input file was executed to produce nine acoustic fields. These fields were then used to create

grayscale and TL difference graphs (Appendix D). Each output file was initially pre-processed by PREGRAY. PREGRAY averaged the intensities of the sound speed field over a given area. The area averaged can be found from the PREGRAY log output file and is represented as a gray dot in the plots. Each gray dot represents the same averaged area only if the same type of plot (grayscale or TL difference) created was the same. In this case, each gray dot for grayscale plots represented an area 18m deep X 350m long and for transmission loss difference graphs, 9m deep X 2450m long.

Each grayscale graph was plotted with a minimum TL of 50 dB and a maximum TL of 100 dB and to a maximum depth of 5000 m. In each TL difference graph the maximum difference plotted between two samples was treated as no more than ten dB and the minimum difference (obviously) no less than zero dB. To generate each TL difference graph, the intensities were subtracted from the 2 km baseline sample; those differences were converted to transmission loss values. In this way, TL difference graphs were produced for 4, 6, 8, 10, 20, 25, 30, and 60 km. For example, the 4 km sample was created by subtracting the 4 km intensities from the 2 km intensities values (Fig. 9). TL difference graphs were plotted only to a depth of 1000

m, since instabilities generally show up in the upper 1000. These figures were useful for qualitative but not for quantitative analysis. They were used primarily to qualitatively assess the horizontal spatial requirement needed, prior to more detailed quantitative analysis. Additionally, the TLDIF program tabulated the number of gray dots within a certain dB bin, arbitrarily defined by the program. Appendix E contains all the TL difference graphs. Histograms were then produced from these data.

The above restrictions were applied in order to prevent the graphs from becoming "cluttered". These particular limits were chosen after experimentation with other values to produce uncluttered graphs.

A. IFDPE INPUT RUNSTREAM

The input runstream is prepared in free format as follows:

```
FRQ, ZS, CO, ISF, RA, ZA, N, IHNK, IYPEB, IYPES  
RMAX, DR, WDR, WDZ, PDR, PDZ, ISFLD, ISVP, IBPOT  
A, B, C, D
```

where

FRQ = Frequency (Hz), a 100 Hz frequency was
chosen as representative.

ZS = source depth (m), 100 m was chosen for the validation and resolution study; 500 m and 1000 m were chosen for the sensitivity studies.

CO = reference sound speed, a zero was chosen which sets the sound speed to the average sound speed in the layer.

ISF = starting field, a Gaussian starting field was assumed.

RA = horizontal range (m) from source depth to starting field; starting field was assumed to be the initial source range, i.e., 0.0.

ZA = depth (m) of starting field at RA, 9900m.

N = number of equispaced receivers in the starting field, 3300.

IHNK = Hankel function flag, since starting field is Gaussian, IHNK is set to 0.

ITYPEB = type of bottom, 0 sets the bottom type to that supplied by the user.

ITYPES = type of surface, 0 sets the surface as a pressure release surface.

RMAX = maximum range (m) of solution, for this study, maximum range was 150,000 m.

DR = range step (m) for marching solution, 5m.

WDR = range step (m) at which solution is written on disk, 50m.

WDZ = depth increment (m) at which solution is
written on disk, 9m.

PDR = range step (m) at which solution is written,
10,000m.

PDZ = depth increment (m) at which solution is
written, 4,000m.

ISFLD = 0, don't print starting field.

ISVP = 0, don't print sound speed profile.

IBOT = 0, don't print bottom depths.

A = 1.0

B = 0.75

C = 1.0

D = 0.25

A, B, C, and D turn on the wide-angle option for
IFDPE.

The rest of the input runstream consists of the
merged files including the water sound speed profiles,
bottom bathymetry, and sound speed profile, density and
attenuation for each bottom layer.

B. SENSITIVITY STUDIES

After the IFDPE runs were made and a general idea
of the resolution range was ascertained, two extra
source depths were executed, to determine if the
horizontal spacing required was dependent upon source
depth. The identical IFDPE input files for the

verification and resolution studies were used but the source depths were changed to 500 m for the first depth and 1000 m for the second depth. Input runs were made only for the 6, 8, 10, and 20 km samples because the results indicated that the resolution required was approximately 8 km.

C. HISTOGRAMS

Figure 10 tabulates the percentage of transmission loss values that fall into a TL (dB) range for the 2 and 4 km difference spacings at a 100 m source depth.

Obviously, no TL values could be less than zero. However, any TL values greater than 9.17 dB were put into the same bin. Bins in between 0 and 9.17 dB are delineated at 1.87, 2.92, 3.96, 5.0, 6.04, 7.08, 8.13, and 9.17 dB. For all the histograms of TL differenced values, see Appendix F.

TABLE 2.

IDEAL VS TRUE DISTANCE USED IN SAMPLES

SAMPLE	AVG DISTANCE
2 km	1.9495 km
4 km	3.8834 km
6 km	5.8254 km
8 km	7.8385 km
10 km	9.8583 km
20 km	16.7783 km
30 km	
60 km	

GULF STREAM DIFF RES 2KM AND 4KM

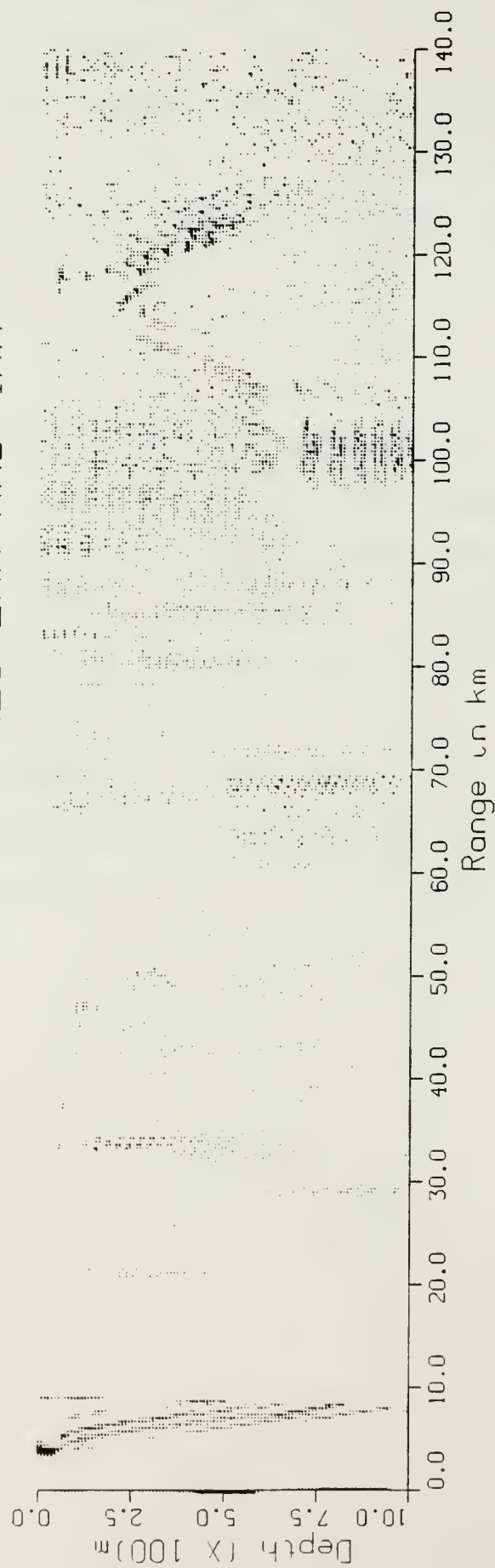


FIG. 9 2-4 km TL Difference Sample

GULF STREAM DIFF RES 2KM AND 4KM
 SOURCE DEPTH = 100M
 CALCULATED STATISTICS ON TL VALUES ABOVE 1000M



FIG 10 Histogram Sample of 2-4 km TT Difference Graph

V. RESULTS

Table 3 shows the percent difference values that fall below 2.92 dB for various criteria. Fig. 11 plots those TL percent differences versus range spacings. A cut-off of 2.92 dB was chosen because tactical operations are most affected for TL differences of 3.0 dB or more. These criteria are arbitrary and can be changed to suit the user's requirements. Table 4 shows the TL differences below 2.92 dB for the 100, 500, and 1000 m source depths at each one's respective candidate spacings after TL differencing.

Succinctly, the 100 m source depth requires an approximate horizontal spatial requirement of 8 km; the 500 m source depth, 6 km, and; the 1000 m source depth, 4 km. It is obvious that the horizontal spatial requirements are source depth dependent.

TABLE 3

PERCENT CRITERIA AND RANGE SPACING REQUIRED

Percent	Depth (m)		
	100	500	1000
90%	4 km	n/a	n/a
80	8	4	2
75	8-10	6	4

TABLE 4

RANGE SPACING AND PERCENT FOR $\Delta TL < 2.92$ dB

Range Spacing (km)	Depth (m)		
	100	500	1000
4 km	90.92%		
6	83.09	77.48	72.00
8	76.92	70.74	65.11
10	73.62	67.94	62.16
20		56.50	56.10
25	65.61		
30	65.02		
60	59.41		

TL PERCENT' VS RANGE SPACINGS

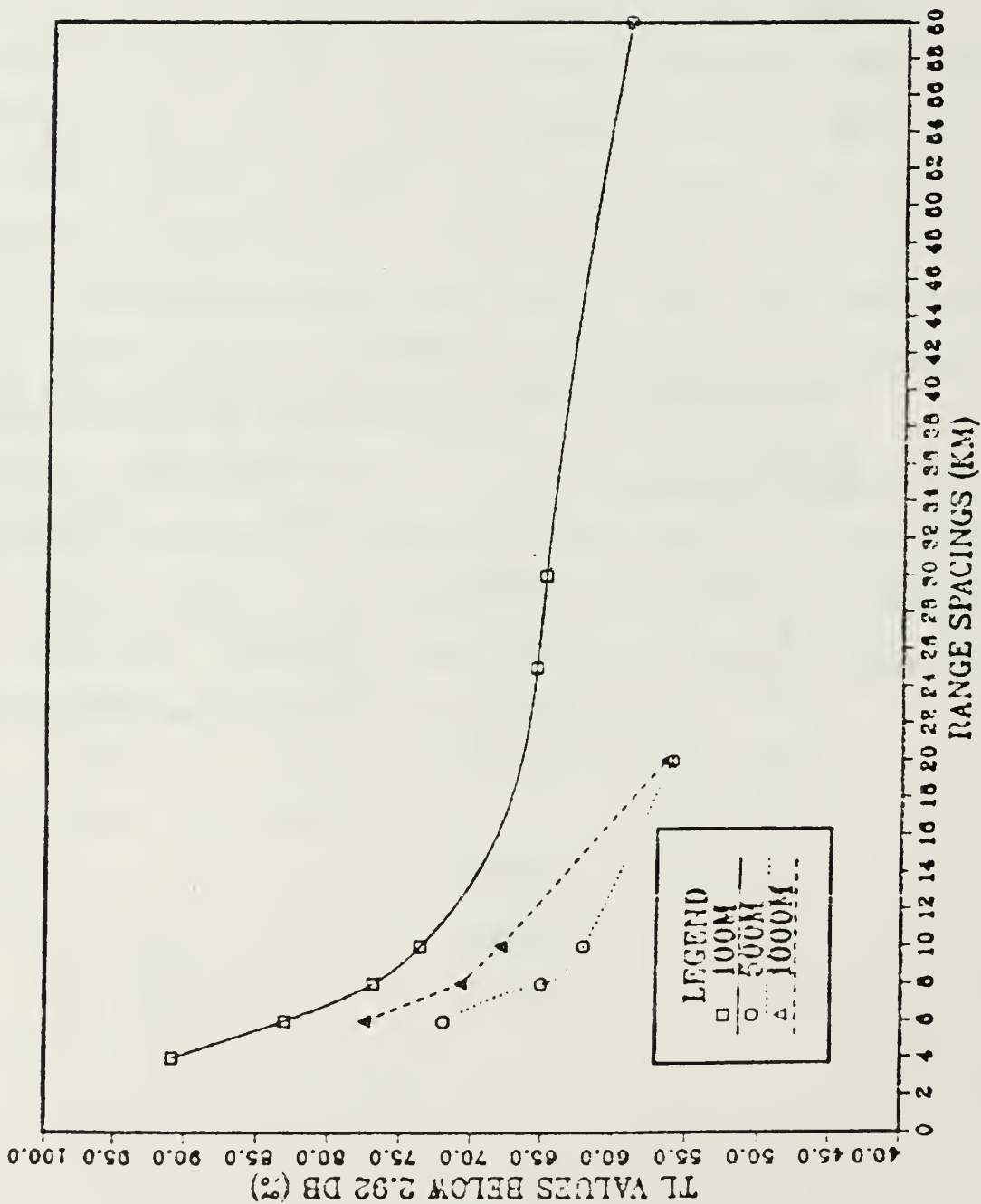


FIG. 11 Percent TL Difference vs Range Spacing

VI. CONCLUSIONS

Other studies have attempted to answer the question this study posed: how does the data base have to be resolved to minimize transmission loss errors for range-dependent models?

Daubin, Tappert, and Nghiem-Phu (Ref. 12) addressed the pertinent issue of the size of a data base—how large a data base is required? In a second study (Ref. 13), they discussed the accuracy of a data base (how accurate must it be? how accurate can it be?)

Unlike the results of this study, Daubin, Tappert, and Nghiem-Phu find that there "was no clearly discernible effect of source depth". This study clearly shows that there is a source depth dependency based upon the transmission loss percent criteria chosen.

Henrick (Ref. 14) argues that using single sound speed profiles for range intervals exceeding about every three km may produce errors and recommends incorporating an interpolation routine. Such a routine was indeed necessary in this study to obtain additional sound speed profiles. This feature may be required in operational range-dependent acoustic propagation loss models.

Other problems regarding the environment needed in an operational range-dependent model need to be

addressed. What happens to the horizontal spacing required if the first sound speed profile is moved in relation to the North Wall of the Gulf Stream? Since sound speed is temperature/salinity dependent, what happens to the spacing requirement because of seasonal changes? This study used data obtained in the winter; what if the same procedure were used for data obtained in the summer? Does it make a difference in the spacing required if the acoustic field were travelling from the warm waters of the Sargasso Sea into the cold waters of the Slope Water? What effect do multiple density discontinuities (eddies and fronts) have on the spacing required?

Other questions to be answered involve the resolution of the vertical spatial requirements and the need to resolve specific spacings through a front. The vertical question is more difficult to solve than that of the horizontal spatial needs, but efforts are underway to answer it. For horizontal spacings, maybe an 8 km resolution at 100 m source depth is not required through the entire front. Perhaps, in the specific environment chosen here, 8 km is needed only to define acoustic transmission around the North Wall of the Gulf Stream but a grosser resolution is needed at the South Edge.

The tactical question also must be answered. How are these results (and others revolving around the general environment question) to be used in a tactical environment? in tactical scenario models? This is 1990's technology. However, before that technology can be implemented, the fundamental oceanographic problems must be resolved first.

APPENDIX A
GSFE EXPERIMENTAL DATA

Enclosed are the data from the Gulf Stream Frontal Experiment used in this report.

ORIGINAL BATHYMETRY PROFILE (in nm) TRACK ONE

RANGE	DEPTH		
0.0	4836		
1.0	4874	50.0	4932
2.0	4888	51.0	4935
3.0	4884	52.0	4937
4.0	4869	53.0	4939
5.0	4856	54.0	4940
6.0	4850	55.0	4941
7.0	4850	56.0	4942
8.0	4852	57.0	4944
9.0	4855	58.0	4945
10.0	4856	59.0	4947
11.0	4855	60.0	4949
12.0	4854	61.0	4950
13.0	4852	62.0	4951
14.0	4852	63.0	4952
15.0	4852	64.0	4953
16.0	4853	65.0	4954
17.0	4856	66.0	4955
18.0	4860	67.0	4956
19.0	4865	68.0	4957
20.0	4869	69.0	4958
21.0	4874	70.0	4959
22.0	4876	71.0	4960
23.0	4877	72.0	4961
24.0	4878	73.0	4962
25.0	4879	74.0	4963
26.0	4880		
27.0	4882		
28.0	4884		
29.0	4886		
30.0	4888		
31.0	4891		
32.0	4893		
33.0	4896		
34.0	4898		
35.0	4901		
36.0	4904		
37.0	4907		
38.0	4909		
39.0	4911		
40.0	4914		
41.0	4916		
42.0	4918		
43.0	4920		
44.0	4922		
45.0	4924		
46.0	4925		
47.0	4926		
48.0	4928		
49.0	4930		

BATHYMETRY PROFILE (in nm) TRACK TWO

RANGE

DEPTH

0.0	3560		31.9	4731.9	*
0.1	3590	*	32.0	4732	
0.25	3636.75	*	33.0	4733	
0.40	3682.80	*	33.4	4733.4	*
0.50	3713.50	*	34.0	4734	
0.75	3790.20	*	35.0	4735	
0.90	3836.30	*	35.6	4735.6	*
1.0	3867		36.0	4736	
1.9	4170.3	*			
2.0	4204				
2.4	4320	*	(*) indicates ranges and depths interpolated due to the rapid sloping of the shelf		
2.8	4437.8	*			
3.0	4496				
3.4	4566.8	*			
3.8	4637.6	*			
4.0	4673				
4.1	4678.7	*			
4.4	4695.8	*			
5.0	4730				
5.8	4713.2	*			
6.0	4709				
6.5	4681.5	*			
7.0	4654				
7.5	4630.5	*			
8.0	4607				
8.8	4587	*			
9.0	4582				
10.0	4576				
11.0	4585				
12.0	4608				
13.0	4638				
14.0	4669				
14.4	4680.2	*			
15.0	4697				
16.0	4716				
17.0	4727				
18.0	4729				
19.0	4726				
20.0	4718				
21.0	4708				
22.0	4700				
23.0	4694				
23.4	4694	*			
24.0	4694				
25.0	4698				
26.0	4705				
27.0	4712				
27.4	4715.2	*			
28.0	4720				
29.0	4725				
29.2	4725.6	*			
30.0	4728				
31.0	4731				

BATHYMETRY PROFILE (in nm) TRACK THREE

RANGE	DEPTH	
0.0	4959	
1.0	4961	
2.0	4963	
3.0	4964	
3.7	4964	*
4.0	4964	
5.0	4964	
6.0	4962	
7.0	4960	
8.0	4957	
9.0	4954	
10.0	4951	
11.0	4950	
12.0	4949	
13.0	4950	
13.7	4951.4	*
14.0	4952	
15.0	4954	
16.0	4957	
17.0	4959	
18.0	4961	
19.0	4963	
20.0	4965	
21.0	4966	
22.0	4967	
23.0	4969	
24.0	4970	
25.0	4972	
26.0	4973	
27.0	4975	
28.0	4976	
29.0	4976	
30.0	4976	
31.0	4976	
32.0	4975	
33.0	4973	
34.0	4972	
35.0	4971	
36.0	4970	
37.0	4929	
37.5	4929	*
38.0	4929	
39.0	4929	

(*) indicates ranges and depths interpolated due to bottom irregularities

BATHYMETRY PROFILE (in nm) TRACK FOUR

RANGE

DEPTH

0.0	4875		44.0	4760	
1.0	4873		45.0	4759	
2.0	4872		46.0	4759	
3.0	4870		46.5	4758	*
4.0	4869		47.0	4757	
5.0	4868		47.9	4757	*
6.0	4867		48.0	4757	
6.2	4866.6	*	49.0	4755	
7.0	4865		49.8	4754.2	*
8.0	4864		50.0	4754	
9.0	4862		51.0	4752	
10.0	4860		51.3	4751.7	*
11.0	4859		52.0	4751	
12.0	4857		52.7	4750.3	*
13.0	4856		53.0	4750	
14.0	4855		54.0	4750	
15.0	4854		55.0	4750	
16.0	4853		55.1	4750	*
17.0	4852		56.0	4750	
18.0	4850		57.0	4748	
19.0	4848		58.0	4746	
20.0	4844		58.6	4743.6	*
21.0	4837		59.0	4742	
22.0	4826		60.0	4737	
23.0	4815		61.0	4730	
23.3	4811.7	*	61.1	4729.4	*
24.0	4804		62.0	4724	
25.0	4795		63.0	4721	
25.5	4792	*	64.0	4722	
26.0	4789		65.0	4731	
27.0	4786		65.6	4738.8	*
28.0	4784		66.0	4744	
29.0	4782		67.0	4759	
30.0	4780		68.0	4773	
31.0	4779		68.8	4784.2	*
32.0	4777		69.0	4787	
33.0	4775				
34.0	4773				
35.0	4771				
35.2	4770.6	*	(*) indicates ranges and depths interpolated due to bottom irregular		
36.0	4769				
37.0	4767				
38.0	4766				
39.0	4765				
40.0	4763				
40.8	4762.2	*			
41.0	4762				
42.0	4761				
43.0	4760				
43.8	4760	*			

SOUND SPEED PROFILES TRACK ONE (empirical data)

NOTE: Depth is in meters; sound speed is in meters/second

RANGE 0.0 NM

DEPTH	SOUND SPEED
0.0	1515.3
10.0	1514.9
30.0	1516.2
60.0	1518.6
75.0	1514.4
95.0	1509.4
105.0	1509.6
125.0	1505.5
135.0	1503.8
150.0	1503.2
200.0	1498.3
250.0	1491.8
270.0	1488.9
300.0	1487.4
320.0	1486.5
350.0	1482.6
370.0	1483.7
400.0	1483.0
450.0	1481.6
480.0	1481.3
520.0	1481.3
560.0	1480.3
600.0	1480.7
650.0	1480.9
700.0	1481.3
740.0	1481.2
800.0	1481.9
900.0	1483.0
1000.0	1484.2
1100.0	1485.4
1200.0	1486.7
1300.0	1488.0
1400.0	1489.3
1500.0	1490.7
1600.0	1492.1
1800.0	1494.9
2000.0	1497.9
2200.0	1500.5
2500.0	1504.5
3000.0	1511.2
3500.0	1519.0
4000.0	1526.9
4500.0	1535.9
4874.0	1542.6

RANGE 2.8 NM

DEPTH	SOUND SPEED
0.0	1518.0
10.0	1517.9
30.0	1518.3
55.0	1518.8
70.0	1518.2
100.0	1510.2
110.0	1509.4
120.0	1510.2
150.0	1504.0
200.0	1499.4
250.0	1493.5
280.0	1489.6
300.0	1488.5
350.0	1485.4
400.0	1482.6
450.0	1481.3
480.0	1481.2
510.0	1480.6
540.0	1480.7
580.0	1480.2
650.0	1480.8
700.0	1481.0
750.0	1481.5
790.0	1481.8
900.0	1483.0
1000.0	1484.2
1100.0	1485.4
1200.0	1486.7
1300.0	1488.0
1400.0	1489.3
1500.0	1490.7
1600.0	1492.1
1800.0	1494.9
2000.0	1497.9
2200.0	1500.5
2500.0	1504.5
3000.0	1511.2
3500.0	1519.0
4000.0	1526.9
4500.0	1535.9
4885.0	1542.8

RANGE 5.7 NM

DEPTH	SOUND SPEED
0.0	1519.1
10.0	1518.8
25.0	1519.1
50.0	1520.0
75.0	1520.8
105.0	1510.9
120.0	1512.5
130.0	1510.1
135.0	1510.8
155.0	1507.5
165.0	1508.8
200.0	1502.2
250.0	1498.1
300.0	1492.0
350.0	1488.6
380.0	1486.3
410.0	1485.4
430.0	1483.4
480.0	1482.0
510.0	1481.3
540.0	1481.7
570.0	1481.7
600.0	1481.5
650.0	1481.9
700.0	1482.2
750.0	1482.6
790.0	1482.7
900.0	1483.0
1000.0	1484.2
1100.0	1485.4
1200.0	1486.7
1300.0	1488.0
1400.0	1489.3
1500.0	1490.7
1600.0	1492.1
1800.0	1494.9
2000.0	1497.9
2200.0	1500.5
2500.0	1504.5
3000.0	1511.2
3500.0	1519.0
4000.0	1526.9
4500.0	1535.9
4852.0	1542.2

RANGE 8.8 NM

DEPTH	SOUND SPEED
0.0	1519.7
25.0	1520.1
50.0	1520.5
60.0	1520.2
75.0	1520.5
95.0	1521.3
125.0	1513.3
150.0	1509.6
180.0	1507.2
200.0	1505.9
220.0	1505.2
250.0	1500.3
300.0	1495.5
360.0	1490.7
380.0	1490.4
400.0	1488.9
440.0	1485.7
460.0	1485.6
500.0	1483.8
550.0	1482.5
590.0	1482.8
650.0	1482.6
710.0	1482.0
750.0	1482.6
800.0	1483.2
870.0	1483.9
890.0	1483.7
1000.0	1485.0
1100.0	1485.7
1200.0	1487.1
1300.0	1488.2
1400.0	1490.1
1500.0	1491.4
1600.0	1493.0
1800.0	1495.7
2000.0	1498.6
2200.0	1501.3
2500.0	1505.4
3000.0	1512.1
3500.0	1519.2
4000.0	1527.1
4500.0	1535.9
4852.0	1542.2

RANGE 14.4 NM	
DEPTH	SOUND SPEED
0.0	1533.7
25.0	1534.0
50.0	1529.1
75.0	1525.2
95.0	1526.1
125.0	1518.4
150.0	1515.1
200.0	1512.6
250.0	1508.7
300.0	1503.5
350.0	1500.6
400.0	1496.8
450.0	1492.2
500.0	1489.8
550.0	1487.4
600.0	1486.0
650.0	1484.8
700.0	1484.1
750.0	1484.0
800.0	1483.9
850.0	1484.5
900.0	1484.8
1000.0	1485.4
1100.0	1486.4
1200.0	1487.1
1300.0	1488.6
1400.0	1489.9
1500.0	1491.3
1600.0	1492.6
1700.0	1494.2
1800.0	1495.6
2000.0	1498.6
2200.0	1501.3
2500.0	1505.4
3000.0	1512.1
3500.0	1519.2
4000.0	1527.1
4500.0	1535.9
4852.0	1542.2

RANGE 15.3 NM	
DEPTH	SOUND SPEED
0.0	1534.0
10.0	1434.2
35.0	1534.8
50.0	1530.5
75.0	1525.1
100.0	1526.1
120.0	1524.6
160.0	1516.0
200.0	1513.2
250.0	1509.4
290.0	1508.3
350.0	1501.3
400.0	1498.4
430.0	1495.0
500.0	1490.7
550.0	1488.0
570.0	1487.9
600.0	1486.6
650.0	1485.3
700.0	1484.7
750.0	1484.2
770.0	1484.4
830.0	1484.1
910.0	1484.6
930.0	1484.5
1000.0	1485.3
1100.0	1486.6
1200.0	1487.5
1300.0	1488.6
1400.0	1489.8
1500.0	1491.4
1600.0	1492.5
1700.0	1494.1
1800.0	1495.5
2000.0	1498.6
2200.0	1501.3
2500.0	1505.4
3000.0	1512.1
3500.0	1519.2
4000.0	1527.1
4500.0	1535.9
4852.0	1542.2

RANGE 17.0 NM	
DEPTH	SOUND SPEED
0.0	1534.1
20.0	1534.5
40.0	1534.9
65.0	1535.5
80.0	1533.1
100.0	1526.3
125.0	1528.2
150.0	1521.4
200.0	1513.0
250.0	1508.8
300.0	1505.0
330.0	1503.1
340.0	1503.0
400.0	1497.4
420.0	1496.0
440.0	1495.4
500.0	1491.1
550.0	1489.2
600.0	1486.7
620.0	1485.8
640.0	1486.3
700.0	1485.5
730.0	1484.9
750.0	1485.0
820.0	1484.4
850.0	1484.6
900.0	1484.9
1000.0	1485.3
1100.0	1486.6
1200.0	1487.5
1300.0	1488.6
1400.0	1489.8
1500.0	1491.4
1600.0	1492.5
1700.0	1494.1
1800.0	1495.5
2000.0	1498.6
2200.0	1501.3
2500.0	1505.4
3000.0	1512.1
3500.0	1519.2
4000.0	1527.1
4500.0	1535.9
4856.0	1542.3

RANGE 18.8 NM	
DEPTH	SOUND SPEED
0.0	1535.3
25.0	1535.8
50.0	1536.0
75.0	1537.2
100.0	1532.6
115.0	1529.0
125.0	1528.9
150.0	1526.3
175.0	1517.6
185.0	1519.8
200.0	1518.5
250.0	1512.1
300.0	1507.2
350.0	1504.7
400.0	1501.9
450.0	1498.5
510.0	1493.8
540.0	1493.0
600.0	1488.5
640.0	1486.6
650.0	1486.8
680.0	1485.4
700.0	1485.4
730.0	1485.0
780.0	1485.5
800.0	1485.5
820.0	1485.7
850.0	1485.2
900.0	1485.6
950.0	1485.6
1000.0	1485.6
1100.0	1486.6
1200.0	1487.8
1300.0	1489.1
1400.0	1490.3
1500.0	1491.8
1600.0	1493.0
1700.0	1494.2
1800.0	1495.6
2000.0	1498.6
2200.0	1501.3
2500.0	1505.4
3000.0	1512.1
3500.0	1519.2
4000.0	1527.1
4500.0	1535.9
4864.0	1542.4

RANGE 20.2 NM

DEPTH	SOUND SPEED
0.0	1534.9
25.0	1535.2
50.0	1535.5
75.0	1536.7
85.0	1536.8
100.0	1536.5
125.0	1529.5
150.0	1527.3
200.0	1520.9
230.0	1514.5
240.0	1516.2
270.0	1514.6
300.0	1510.1
350.0	1506.3
400.0	1503.6
450.0	1501.2
500.0	1497.4
550.0	1493.9
570.0	1493.0
580.0	1492.9
620.0	1489.9
630.0	1489.8
680.0	1486.1
690.0	1486.0
710.0	1484.8
760.0	1485.0
810.0	1484.5
850.0	1485.1
870.0	1485.4
930.0	1485.4
1000.0	1485.9
1100.0	1486.8
1200.0	1487.8
1300.0	1489.1
1400.0	1490.3
1500.0	1491.7
1600.0	1492.9
1700.0	1494.1
1800.0	1495.7
2000.0	1498.6
2200.0	1501.3
2500.0	1505.4
3000.0	1512.1
3500.0	1519.2
4000.0	1527.1
4500.0	1535.9
4870.0	1542.6

RANGE 26.0 NM

DEPTH	SOUND SPEED
0.0	1535.8
25.0	1536.3
50.0	1536.6
75.0	1537.0
105.0	1537.4
125.0	1534.6
150.0	1531.7
200.0	1525.3
230.0	1522.4
250.0	1521.9
300.0	1520.5
350.0	1518.3
380.0	1516.7
440.0	1512.2
460.0	1507.9
500.0	1503.9
550.0	1500.1
600.0	1498.0
650.0	1495.1
700.0	1492.7
800.0	1485.8
870.0	1485.1
900.0	1485.4
1000.0	1485.8
1100.0	1486.7
1200.0	1487.7
1300.0	1488.9
1400.0	1490.4
1500.0	1491.7
1600.0	1493.0
1700.0	1494.5
1800.0	1495.7
2000.0	1498.6
2200.0	1501.3
2500.0	1505.4
3000.0	1512.1
3500.0	1519.2
4000.0	1527.1
4500.0	1535.9
4880.0	1542.7

RANGE 31.3 NM

DEPTH	SOUND SPEED
0.0	1536.0
25.0	1536.3
50.0	1536.5
75.0	1536.8
100.0	1537.0
125.0	1537.9
135.0	1537.2
150.0	1537.7
200.0	1531.1
250.0	1527.7
280.0	1522.7
290.0	1522.5
350.0	1515.9
400.0	1511.8
450.0	1508.6
500.0	1506.5
550.0	1503.1
600.0	1500.1
650.0	1496.8
700.0	1494.4
750.0	1491.7
800.0	1488.4
900.0	1486.1
1000.0	1485.6
1100.0	1486.7
1200.0	1487.7
1300.0	1488.9
1400.0	1490.4
1500.0	1491.7
1600.0	1493.0
1700.0	1494.5
1800.0	1495.7
2000.0	1498.6
2200.0	1501.3
2500.0	1505.4
3000.0	1512.1
3500.0	1519.2
4000.0	1527.1
4500.0	1535.9
4892.0	1543.0

RANGE 36.6 NM

DEPTH	SOUND SPEED
0.0	1536.0
25.0	1536.3
50.0	1536.7
75.0	1536.8
100.0	1537.2
135.0	1537.9
160.0	1536.6
200.0	1532.6
220.0	1531.7
230.0	1531.7
250.0	1529.5
290.0	1525.4
310.0	1524.4
350.0	1520.4
410.0	1516.4
420.0	1516.0
450.0	1513.2
500.0	1510.1
550.0	1508.0
600.0	1505.8
650.0	1503.2
700.0	1501.0
800.0	1496.6
900.0	1492.9
1000.0	1489.8
1050.0	1488.5
1100.0	1489.2
1200.0	1490.0
1300.0	1491.9
1400.0	1492.6
1500.0	1493.8
1600.0	1495.0
1700.0	1496.1
1800.0	1497.6
2000.0	1499.6
2200.0	1502.4
2500.0	1506.4
3000.0	1512.1
3500.0	1519.2
4000.0	1527.1
4500.0	1535.9
4905.0	1543.2

RANGE 42.1 NM	
DEPTH	SOUND SPEED
0.0	1536.1
50.0	1537.0
75.0	1537.1
100.0	1537.4
125.0	1537.8
150.0	1534.7
170.0	1534.0
175.0	1534.2
200.0	1532.3
250.0	1528.3
280.0	1526.0
300.0	1525.3
330.0	1523.4
340.0	1523.5
400.0	1520.6
450.0	1517.5
500.0	1514.6
550.0	1510.4
600.0	1508.0
660.0	1503.0
680.0	1502.0
720.0	1499.8
750.0	1498.5
780.0	1496.2
840.0	1494.4
900.0	1493.5
1000.0	1490.7
1100.0	1490.0
1200.0	1490.9
1300.0	1491.9
1400.0	1492.6
1500.0	1493.8
1600.0	1495.0
1700.0	1496.1
1800.0	1497.6
2000.0	1499.6
2200.0	1502.4
2500.0	1506.3
3000.0	1512.1
3500.0	1519.2
4000.0	1527.1
4500.0	1535.9
4918.0	1543.4

RANGE 47.5 NM	
DEPTH	SOUND SPEED
0.0	1537.0
25.0	1537.3
50.0	1537.6
80.0	1538.1
95.0	1537.9
110.0	1538.0
125.0	1537.9
150.0	1534.6
165.0	1533.1
185.0	1532.6
200.0	1531.2
250.0	1527.8
270.0	1526.6
300.0	1526.0
350.0	1524.8
420.0	1523.5
520.0	1519.6
550.0	1515.7
600.0	1513.1
670.0	1507.1
750.0	1502.5
780.0	1500.5
810.0	1500.0
850.0	1497.7
900.0	1495.2
950.0	1493.9
1000.0	1492.6
1070.0	1491.7
1100.0	1491.0
1170.0	1490.7
1250.0	1491.8
1280.0	1491.6
1300.0	1491.9
1350.0	1491.9
1400.0	1492.6
1500.0	1493.8
1600.0	1495.0
1700.0	1496.1
1800.0	1497.6
2000.0	1499.6
2200.0	1502.4
2500.0	1506.3
3000.0	1512.1
3500.0	1519.2
4000.0	1527.1
4500.0	1535.9
4927.0	1543.6

RANGE 53.2 NM	
DEPTH	SOUND SPEED
0.0	1535.8
5.0	1535.9
35.0	1534.4
50.0	1534.6
75.0	1535.1
100.0	1535.5
130.0	1536.0
140.0	1535.9
150.0	1534.5
195.0	1528.8
200.0	1528.8
230.0	1527.3
270.0	1525.7
320.0	1524.6
400.0	1524.6
470.0	1523.5
550.0	1520.0
600.0	1515.8
630.0	1513.6
670.0	1512.5
700.0	1510.2
750.0	1506.0
800.0	1502.4
850.0	1499.5
900.0	1496.3
1000.0	1492.6
1100.0	1491.0
1200.0	1490.9
1300.0	1491.9
1400.0	1492.6
1500.0	1493.8
1600.0	1495.0
1700.0	1496.1
1800.0	1497.6
2000.0	1499.6
2200.0	1502.4
2500.0	1506.3
3000.0	1512.1
3500.0	1519.2
4000.0	1527.1
4500.0	1535.9
4939.0	1543.8

RANGE 58.7 NM	
DEPTH	SOUND SPEED
0.0	1536.5
10.0	1536.6
25.0	1536.0
50.0	1535.1
70.0	1534.6
100.0	1534.9
125.0	1535.0
150.0	1531.3
170.0	1528.8
180.0	1528.7
230.0	1525.8
270.0	1525.2
310.0	1525.2
340.0	1525.0
390.0	1525.2
420.0	1525.2
460.0	1524.9
520.0	1525.3
540.0	1525.2
560.0	1524.6
610.0	1522.9
630.0	1519.4
650.0	1518.8
700.0	1516.2
750.0	1513.0
800.0	1510.4
870.0	1504.9
900.0	1503.9
930.0	1502.1
1000.0	1499.0
1100.0	1496.5
1200.0	1492.9
1300.0	1492.0
1400.0	1492.4
1500.0	1493.4
1600.0	1494.5
1700.0	1495.3
1800.0	1496.5
2000.0	1499.6
2500.0	1506.3
3000.0	1512.1
3500.0	1519.2
4000.0	1527.1
4500.0	1535.9
4945.0	1544.0

RANGE 63.8 NM	
DEPTH	SOUND SPEED
0.0	1536.4
25.0	1536.7
50.0	1534.0
65.0	1533.7
90.0	1534.0
115.0	1534.5
150.0	1529.5
175.0	1526.7
200.0	1525.5
250.0	1524.2
340.0	1524.2
400.0	1524.5
460.0	1524.6
490.0	1525.0
530.0	1524.8
580.0	1523.7
590.0	1524.0
600.0	1523.3
650.0	1520.0
700.0	1517.2
750.0	1513.9
800.0	1510.8
850.0	1506.9
900.0	1502.8
1000.0	1498.0
1100.0	1494.8
1200.0	1492.9
1300.0	1492.0
1400.0	1492.4
1500.0	1493.4
1600.0	1494.5
1700.0	1495.3
1800.0	1496.5
2000.0	1499.6
2500.0	1506.3
3000.0	1512.1
3500.0	1519.2
4000.0	1527.1
4500.0	1535.9
4853.0	1544.1

RANGE 69.2 NM	
DEPTH	SOUND SPEED
0.0	1536.3
10.0	1536.4
30.0	1535.4
55.0	1534.3
75.0	1534.3
110.0	1534.6
150.0	1528.9
200.0	1525.5
240.0	1524.0
290.0	1523.7
320.0	1523.8
350.0	1523.6
400.0	1523.9
450.0	1524.7
520.0	1525.6
560.0	1525.5
580.0	1525.1
620.0	1525.1
650.0	1525.3
700.0	1521.3
750.0	1517.7
800.0	1514.3
850.0	1509.8
910.0	1506.1
960.0	1502.8
970.0	1502.2
1000.0	1500.5
1100.0	1496.5
1210.0	1492.7
1250.0	1492.1
1280.0	1491.9
1300.0	1492.0
1400.0	1492.4
1500.0	1493.4
1600.0	1494.5
1700.0	1495.3
1800.0	1496.5
2000.0	1499.6
2500.0	1506.3
3000.0	1512.1
3500.0	1519.2
4000.0	1527.1
4500.0	1535.9
4958.0	1544.1

SOUND SPEED PROFILES TRACK TWO

NOTE: Depth is in meters; sound speed is in meters/second

RANGE 0.0 NM

DEPTH	SOUND SPEED
0.0	1502.9
30.0	1520.5
58.0	1521.0
75.0	1517.6
100.0	1513.6
125.0	1509.9
150.0	1507.4
198.0	1502.1
252.0	1498.7
259.0	1498.7
300.0	1495.6
357.0	1491.6
370.0	1491.5
401.0	1489.4
429.0	1487.6
442.0	1487.5
471.0	1485.7
484.0	1485.6
497.0	1484.6
600.0	1482.2
650.0	1482.0
700.0	1482.4
800.0	1482.6
900.0	1483.3
1000.0	1484.1
1100.0	1485.1
1200.0	1486.4
1300.0	1487.9
1400.0	1489.2
1500.0	1490.7
1600.0	1491.9
1800.0	1494.9
2000.0	1497.8
2200.0	1500.4
2500.0	1504.6
3000.0	1511.3
3560.0	1520.0

RANGE 1.9 NM

DEPTH	SOUND SPEED
0.0	1522.3
40.0	1521.4
55.0	1521.4
75.0	1516.8
100.0	1512.4
130.0	1508.6
145.0	1508.4
160.0	1505.5
200.0	1501.8
250.0	1498.5
290.0	1496.5
310.0	1494.5
350.0	1492.0
400.0	1489.6
450.0	1487.0
500.0	1484.8
540.0	1484.6
600.0	1481.9
660.0	1481.5
700.0	1481.9
720.0	1481.7
750.0	1482.0
800.0	1482.6
850.0	1482.8
900.0	1483.3
1000.0	1484.1
1100.0	1485.1
1200.0	1486.4
1300.0	1487.9
1400.0	1489.2
1500.0	1490.7
1600.0	1491.9
1700.0	1493.4
1800.0	1494.8
2000.0	1497.8
2200.0	1500.4
2500.0	1504.6
3000.0	1511.3
3500.0	1519.0
4000.0	1526.9
4170.0	1530.0

RANGE 4.1 NM

DEPTH	SOUND SPEED
0.0	1522.4
30.0	1522.6
60.0	1523.1
75.0	1520.5
105.0	1512.2
110.0	1512.1
135.0	1508.0
155.0	1506.6
165.0	1506.2
205.0	1503.0
240.0	1501.0
270.0	1498.4
300.0	1496.7
350.0	1492.6
400.0	1490.5
450.0	1487.5
500.0	1485.3
520.0	1487.8
550.0	1482.4
600.0	1481.6
640.0	1481.4
700.0	1482.0
750.0	1482.5
790.0	1483.1
830.0	1483.1
900.0	1483.6
950.0	1483.8
1000.0	1484.4
1100.0	1485.0
1200.0	1486.6
1300.0	1488.0
1400.0	1489.3
1500.0	1490.6
1600.0	1491.9
1700.0	1493.4
1800.0	1495.0
2000.0	1497.8
2200.0	1500.4
2500.0	1504.6
3000.0	1511.3
3500.0	1519.0
4000.0	1526.9
4680.0	1539.1

RANGE 5.8 NM

DEPTH	SOUND SPEED
0.0	1527.6
5.0	1527.6
20.0	1522.3
30.0	1523.2
55.0	1523.7
90.0	1514.5
95.0	1514.5
135.0	1507.2
150.0	1506.7
175.0	1505.2
200.0	1503.8
250.0	1500.2
300.0	1496.8
340.0	1493.0
400.0	1490.9
440.0	1488.2
460.0	1487.2
500.0	1486.0
530.0	1485.4
570.0	1483.2
600.0	1482.3
640.0	1482.7
670.0	1482.5
700.0	1482.6
750.0	1482.8
800.0	1483.4
850.0	1483.8
900.0	1484.0
950.0	1484.3
1000.0	1484.4
1100.0	1485.0
1200.0	1486.6
1300.0	1488.0
1400.0	1489.3
1500.0	1490.6
1600.0	1491.9
1700.0	1493.4
1800.0	1495.0
2000.0	1497.8
2200.0	1500.4
2500.0	1504.6
3000.0	1511.3
3500.0	1519.0
4000.0	1526.9
4713.0	1539.7

RANGE 8.8 NM	
DEPTH	SOUND SPEED
0.0	1529.0
15.0	1528.8
20.0	1530.0
35.0	1523.8
40.0	1524.3
50.0	1523.3
65.0	1523.5
80.0	1521.3
100.0	1511.5
115.0	1508.9
125.0	1508.8
150.0	1505.4
175.0	1503.5
210.0	1500.5
220.0	1500.2
250.0	1498.2
300.0	1495.6
350.0	1491.9
400.0	1488.4
450.0	1486.1
500.0	1483.4
550.0	1482.3
570.0	1482.5
610.0	1482.1
630.0	1482.2
660.0	1481.9
700.0	1482.0
750.0	1482.4
800.0	1482.6
900.0	1483.1
1000.0	1484.3
1100.0	1485.4
1200.0	1486.4
1300.0	1487.5
1400.0	1488.9
1500.0	1490.5
1600.0	1491.2
1800.0	1494.5
2000.0	1497.8
2200.0	1500.4
2500.0	1504.6
3000.0	1511.3
3500.0	1519.0
4000.0	1526.9
4587.0	1537.5

RANGE 14.4 NM	
DEPTH	SOUND SPEED
0.0	1529.7
10.0	1529.4
40.0	1522.8
55.0	1523.9
65.0	1523.0
80.0	1524.0
100.0	1514.4
125.0	1509.8
135.0	1509.6
150.0	1507.6
175.0	1504.8
200.0	1503.2
250.0	1499.6
290.0	1496.2
300.0	1496.2
350.0	1493.4
380.0	1491.5
420.0	1490.5
460.0	1488.1
470.0	1488.1
500.0	1486.2
550.0	1484.5
580.0	1482.9
630.0	1482.4
680.0	1482.5
740.0	1482.1
780.0	1482.3
810.0	1482.2
850.0	1482.4
940.0	1483.9
1000.0	1484.3
1100.0	1485.4
1200.0	1486.4
1300.0	1487.5
1400.0	1488.9
1500.0	1490.5
1600.0	1491.2
1700.0	1492.9
1800.0	1494.5
2000.0	1497.8
2200.0	1500.4
2500.0	1504.6
3000.0	1511.3
3500.0	1519.0
4000.0	1526.9
4681.0	1539.2

RANGE 19.0 NM	
DEPTH	SOUND SPEED
0.0	1533.0
20.0	1533.5
40.0	1527.3
60.0	1524.7
75.0	1526.2
100.0	1521.8
125.0	1517.3
140.0	1515.2
145.0	1515.9
175.0	1512.5
200.0	1509.4
250.0	1503.6
300.0	1500.0
350.0	1495.4
390.0	1491.8
400.0	1491.6
450.0	1489.1
470.0	1488.1
480.0	1488.2
550.0	1484.9
600.0	1484.4
650.0	1483.9
700.0	1482.4
750.0	1481.6
800.0	1482.0
900.0	1483.4
1000.0	1484.4
1100.0	1485.4
1200.0	1486.9
1300.0	1488.1
1400.0	1489.3
1500.0	1490.6
1600.0	1491.8
1800.0	1494.8
2000.0	1497.8
2200.0	1500.4
2500.0	1504.6
3000.0	1511.3
3500.0	1519.0
4000.0	1526.9
4726.0	1540.0

RANGE 23.4 NM	
DEPTH	SOUND SPEED
0.0	1530.2
25.0	1530.4
50.0	1528.3
70.0	1523.4
80.0	1527.2
100.0	1523.4
110.0	1518.9
115.0	1519.6
140.0	1515.9
160.0	1511.2
200.0	1507.7
250.0	1504.8
300.0	1501.1
330.0	1498.6
340.0	1498.4
400.0	1495.2
430.0	1493.1
450.0	1492.7
500.0	1489.1
540.0	1486.0
560.0	1485.7
620.0	1483.8
650.0	1484.2
690.0	1482.3
720.0	1481.8
760.0	1481.6
800.0	1482.0
860.0	1483.1
880.0	1483.0
950.0	1483.8
990.0	1484.4
1020.0	1484.2
1100.0	1485.4
1200.0	1486.9
1300.0	1488.1
1400.0	1489.3
1500.0	1490.6
1600.0	1491.8
1700.0	1493.5
1800.0	1494.8
2000.0	1497.8
2200.0	1500.4
2500.0	1504.6
3000.0	1511.3
3500.0	1519.0
4000.0	1526.9
4694.0	1539.4

RANGE 27.4 NM

DEPTH	SOUND SPEED
0.0	1533.5
25.0	1534.0
50.0	1534.6
75.0	1527.9
105.0	1520.4
115.0	1524.0
125.0	1521.5
160.0	1515.0
195.0	1508.4
200.0	1508.4
220.0	1506.4
230.0	1506.3
270.0	1503.0
320.0	1500.0
330.0	1499.8
360.0	1496.7
370.0	1496.4
400.0	1494.2
450.0	1492.0
500.0	1489.6
550.0	1486.7
600.0	1485.0
650.0	1484.0
690.0	1482.3
710.0	1482.5
740.0	1482.2
800.0	1482.5
900.0	1483.4
1000.0	1484.4
1100.0	1485.4
1200.0	1486.9
1300.0	1488.1
1400.0	1489.3
1500.0	1490.6
1600.0	1491.8
1800.0	1494.8
2000.0	1497.8
2200.0	1500.4
2500.0	1504.6
3000.0	1511.3
3500.0	1519.0
4000.0	1526.9
4715.0	1539.8

RANGE 29.2 NM

DEPTH	SOUND SPEED
0.0	1533.7
30.0	1534.4
60.0	1535.1
70.0	1535.0
90.0	1523.2
100.0	1521.5
110.0	1520.3
115.0	1520.6
120.0	1519.7
125.0	1522.2
150.0	1518.3
180.0	1512.1
195.0	1512.8
240.0	1505.5
250.0	1505.3
300.0	1502.6
340.0	1499.1
370.0	1498.4
400.0	1496.0
450.0	1493.0
500.0	1490.4
550.0	1488.2
590.0	1486.4
600.0	1486.5
650.0	1485.1
690.0	1483.6
710.0	1484.1
750.0	1483.3
800.0	1483.0
900.0	1484.1
1000.0	1485.6
1100.0	1486.7
1200.0	1487.6
1300.0	1488.9
1400.0	1490.0
1500.0	1491.2
1600.0	1492.6
1800.0	1495.5
2000.0	1498.6
2200.0	1501.3
2500.0	1505.4
3000.0	1512.1
3500.0	1519.2
4000.0	1527.1
4726.0	1540.0

RANGE 31.9 NM	
DEPTH	SOUND SPEED
0.0	1534.5
25.0	1534.8
50.0	1535.1
90.0	1536.3
125.0	1528.1
150.0	1523.5
175.0	1519.4
200.0	1515.3
250.0	1511.4
270.0	1507.6
300.0	1506.1
350.0	1501.6
400.0	1498.2
440.0	1495.3
450.0	1495.3
500.0	1492.9
540.0	1490.7
600.0	1488.3
650.0	1486.3
700.0	1484.7
760.0	1483.3
780.0	1483.4
800.0	1483.0
850.0	1483.4
900.0	1484.1
950.0	1484.6
1000.0	1485.6
1100.0	1486.7
1200.0	1487.6
1300.0	1488.9
1400.0	1490.0
1500.0	1491.2
1600.0	1492.9
1700.0	1493.9
1800.0	1495.5
2000.0	1498.6
2200.0	1501.3
2500.0	1505.4
3000.0	1512.1
3500.0	1519.2
4000.0	1527.1
4732.0	1540.1

RANGE 33.4 NM	
DEPTH	SOUND SPEED
0.0	1534.3
25.0	1535.2
50.0	1535.5
75.0	1536.8
95.0	1537.1
125.0	1530.4
140.0	1527.4
145.0	1527.4
170.0	1524.2
175.0	1524.0
200.0	1520.3
250.0	1514.6
300.0	1510.8
310.0	1510.5
350.0	1506.0
400.0	1501.1
450.0	1497.3
470.0	1495.7
490.0	1495.5
550.0	1492.4
590.0	1490.3
610.0	1490.1
650.0	1488.5
700.0	1486.9
750.0	1485.1
800.0	1484.5
850.0	1484.2
900.0	1485.0
1000.0	1485.8
1100.0	1487.2
1200.0	1488.0
1300.0	1489.3
1400.0	1490.5
1500.0	1491.9
1600.0	1493.4
1800.0	1496.4
2000.0	1498.6
2200.0	1501.3
2500.0	1505.4
3000.0	1512.1
3500.0	1519.2
4000.0	1527.1
4733.0	1540.1

RANGE 35.6 NM

DEPTH	SOUND SPEED
0.0	1534.7
25.0	1535.2
50.0	1535.5
75.0	1535.8
95.0	1536.1
125.0	1531.6
150.0	1529.0
175.0	1527.0
200.0	1524.1
250.0	1518.4
300.0	1513.7
330.0	1511.8
340.0	1511.6
400.0	1505.0
450.0	1499.6
500.0	1495.6
550.0	1493.2
600.0	1490.8
650.0	1489.0
700.0	1487.2
750.0	1485.8
800.0	1484.5
830.0	1484.1
880.0	1485.1
900.0	1485.0
950.0	1485.2
1000.0	1485.8
1100.0	1487.2
1200.0	1488.0
1300.0	1489.3
1400.0	1490.5
1500.0	1491.9
1600.0	1493.4
1800.0	1496.4
2000.0	1498.6
2200.0	1501.3
2500.0	1505.4
3000.0	1512.1
3500.0	1519.2
4000.0	1527.1
4736.0	1540.1

SOUND SPEED PROFILES TRACK THREE

NOTE: Depth is in meters; sound speed is in meters/second

RANGE 0.0 NM

DEPTH	SOUND SPEED
0.0	1533.8
25.0	1534.0
50.0	1534.4
70.0	1534.7
85.0	1535.0
100.0	1534.4
125.0	1534.1
150.0	1530.9
175.0	1528.0
200.0	1526.9
250.0	1524.8
290.0	1524.6
350.0	1524.5
400.0	1524.7
450.0	1524.8
470.0	1524.7
490.0	1524.8
550.0	1523.4
600.0	1521.6
650.0	1519.7
700.0	1517.5
750.0	1514.5
800.0	1511.2
860.0	1506.3
870.0	1506.1
900.0	1504.8
1000.0	1499.9
1100.0	1495.6
1200.0	1493.6
1230.0	1493.0
1300.0	1493.1
1400.0	1493.4
1500.0	1494.4
1600.0	1494.5
1800.0	1496.7
2000.0	1499.6
2200.0	1502.4
2500.0	1506.4
3000.0	1512.6
3500.0	1519.6
4000.0	1527.3
4500.0	1535.9
4959.0	1544.2

RANGE 2.0 NM

DEPTH	SOUND SPEED
0.0	1533.6
25.0	1533.9
50.0	1534.2
65.0	1534.4
75.0	1534.0
100.0	1533.8
120.0	1533.4
150.0	1530.2
175.0	1527.5
200.0	1525.7
230.0	1524.8
290.0	1524.6
350.0	1524.7
430.0	1524.9
470.0	1524.7
500.0	1524.8
550.0	1523.9
600.0	1522.3
650.0	1520.6
700.0	1518.3
750.0	1515.5
800.0	1512.7
850.0	1509.0
900.0	1504.7
950.0	1502.5
1000.0	1499.9
1050.0	1498.0
1100.0	1495.6
1150.0	1494.8
1200.0	1493.6
1230.0	1493.0
1260.0	1493.4
1300.0	1493.1
1400.0	1493.4
1500.0	1494.4
1600.0	1494.5
1800.0	1496.7
2000.0	1499.7
2200.0	1502.4
2500.0	1506.4
3000.0	1512.6
3500.0	1519.6
4000.0	1527.3
4500.0	1535.9
4963.0	1544.2

RANGE 3.7 NM

DEPTH	SOUND SPEED
0.0	1533.7
25.0	1534.1
50.0	1534.3
75.0	1534.8
90.0	1533.9
105.0	1533.8
120.0	1534.0
140.0	1531.0
160.0	1528.6
165.0	1528.6
200.0	1526.0
250.0	1525.0
300.0	1524.5
350.0	1524.7
410.0	1525.1
430.0	1525.0
470.0	1525.0
500.0	1524.7
550.0	1524.2
600.0	1522.6
650.0	1520.4
700.0	1518.2
750.0	1516.0
800.0	1513.3
850.0	1509.6
900.0	1505.4
910.0	1505.1
960.0	1502.3
970.0	1502.2
1000.0	1500.5
1050.0	1498.2
1100.0	1496.2
1150.0	1495.1
1180.0	1494.4
1200.0	1494.4
1240.0	1493.2
1260.0	1493.3
1300.0	1493.0
1330.0	1492.9
1400.0	1493.6
1500.0	1494.1
1600.0	1494.6
1800.0	1496.7
2000.0	1499.6
2200.0	1502.4
2500.0	1506.4
3000.0	1512.6
3500.0	1519.6
4000.0	1527.3
4500.0	1535.9
4964.0	1544.2

RANGE 13.7 NM

DEPTH	SOUND SPEED
0.0	1534.0
25.0	1534.4
50.0	1534.7
80.0	1535.2
90.0	1534.6
105.0	1534.5
115.0	1534.0
125.0	1533.0
145.0	1529.8
150.0	1529.6
175.0	1527.3
200.0	1525.8
230.0	1524.9
270.0	1524.9
300.0	1525.2
350.0	1525.5
420.0	1525.7
450.0	1525.6
480.0	1525.7
510.0	1525.5
550.0	1525.4
600.0	1524.1
650.0	1521.4
700.0	1519.6
750.0	1517.4
800.0	1514.3
850.0	1511.1
900.0	1507.6
950.0	1504.7
1000.0	1502.7
1100.0	1496.2
1200.0	1494.4
1250.0	1493.3
1300.0	1493.0
1400.0	1493.6
1500.0	1494.1
1600.0	1494.6
1800.0	1496.7
2000.0	1499.6
2200.0	1502.4
2500.0	1506.4
3000.0	1512.6
3500.0	1519.6
4000.0	1527.3
4500.0	1535.9
4952.0	1544.0

RANGE 20.0 NM	
DEPTH	SOUND SPEED
0.0	1533.7
25.0	1534.0
50.0	1534.3
80.0	1534.6
95.0	1533.6
105.0	1533.6
110.0	1533.2
120.0	1533.3
150.0	1528.8
155.0	1529.1
175.0	1526.4
200.0	1524.8
230.0	1524.0
260.0	1524.1
300.0	1524.2
350.0	1524.4
400.0	1524.8
450.0	1524.9
500.0	1524.8
550.0	1524.6
600.0	1523.2
650.0	1520.2
680.0	1519.7
700.0	1519.7
750.0	1516.6
800.0	1513.2
850.0	1508.9
880.0	1508.1
950.0	1504.7
1000.0	1500.5
1100.0	1496.2
1200.0	1494.4
1250.0	1493.3
1300.0	1493.0
1400.0	1493.6
1500.0	1494.1
1600.0	1494.6
1800.0	1496.7
2000.0	1499.6
2200.0	1502.4
2500.0	1506.4
3000.0	1512.6
3500.0	1519.6
4000.0	1527.3
4500.0	1535.9
4965.0	1544.2

RANGE 37.5 NM	
DEPTH	SOUND SPEED
0.0	1534.2
25.0	1534.5
50.0	1534.7
75.0	1534.8
100.0	1535.0
125.0	1535.6
150.0	1531.6
175.0	1529.5
200.0	1527.9
230.0	1526.3
270.0	1525.3
310.0	1525.4
330.0	1525.3
390.0	1525.7
450.0	1525.4
500.0	1525.2
550.0	1525.0
600.0	1524.1
650.0	1522.5
700.0	1520.2
750.0	1517.4
800.0	1514.9
850.0	1511.7
900.0	1507.9
950.0	1505.4
1000.0	1502.6
1050.0	1499.8
1100.0	1497.1
1150.0	1495.1
1180.0	1494.1
1210.0	1493.6
1270.0	1494.1
1290.0	1493.5
1320.0	1493.8
1400.0	1494.2
1500.0	1495.1
1600.0	1496.2
1800.0	1497.7
2000.0	1499.6
2200.0	1502.4
2500.0	1506.4
3000.0	1512.6
3500.0	1519.6
4000.0	1527.3
4500.0	1535.9
4929.0	1543.6

SOUND SPEED PROFILES TRACK FOUR

NOTE: Depth is in meters; sound speed is in meters/second

RANGE 0.0 NM

DEPTH	SOUND SPEED
0.0	1532.8
25.0	1533.3
50.0	1533.7
65.0	1533.9
75.0	1533.3
100.0	1530.6
125.0	1528.0
150.0	1525.8
175.0	1525.0
200.0	1524.2
230.0	1523.8
270.0	1523.7
300.0	1523.8
350.0	1524.0
400.0	1524.5
460.0	1524.8
500.0	1524.5
550.0	1523.9
600.0	1522.2
650.0	1519.9
700.0	1516.0
730.0	1512.0
750.0	1511.4
810.0	1506.2
850.0	1505.4
900.0	1503.7
1000.0	1498.3
1100.0	1494.2
1200.0	1492.4
1250.0	1492.2
1300.0	1492.4
1400.0	1492.8
1500.0	1493.8
1600.0	1494.8
1800.0	1496.9
2000.0	1499.6
2200.0	1502.4
2500.0	1506.4
3000.0	1512.6
3500.0	1519.6
4000.0	1527.3
4500.0	1535.9
4875.0	1542.6

RANGE 6.2 NM

DEPTH	SOUND SPEED
0.0	1534.0
25.0	1534.6
35.0	1534.8
40.0	1534.3
60.0	1534.6
75.0	1534.7
100.0	1532.5
125.0	1528.3
150.0	1526.9
175.0	1525.2
200.0	1524.5
240.0	1524.2
300.0	1524.4
350.0	1524.6
400.0	1524.8
440.0	1524.8
500.0	1524.3
550.0	1522.6
600.0	1519.8
650.0	1517.8
700.0	1514.9
750.0	1510.0
800.0	1507.2
900.0	1503.7
1000.0	1498.3
1100.0	1494.2
1200.0	1492.4
1250.0	1492.2
1300.0	1492.4
1400.0	1492.8
1500.0	1493.8
1600.0	1494.8
1800.0	1496.9
2000.0	1499.6
2200.0	1502.4
2500.0	1506.4
3000.0	1512.6
3500.0	1519.6
4000.0	1527.3
4500.0	1535.9
4867.0	1542.5

RANGE 17.0 NM	
DEPTH	SOUND SPEED
0.0	1533.8
35.0	1534.4
50.0	1533.8
75.0	1534.1
100.0	1530.2
125.0	1527.9
130.0	1527.8
150.0	1526.6
180.0	1524.5
210.0	1524.0
250.0	1523.7
300.0	1523.7
350.0	1523.8
380.0	1523.9
410.0	1523.7
440.0	1523.9
490.0	1523.7
550.0	1521.7
600.0	1518.3
650.0	1515.4
700.0	1514.1
750.0	1510.1
800.0	1505.0
850.0	1502.0
900.0	1499.1
950.0	1496.2
1000.0	1493.5
1100.0	1491.0
1200.0	1490.5
1300.0	1491.0
1400.0	1492.4
1500.0	1493.8
1600.0	1494.8
1800.0	1496.9
2000.0	1499.6
2200.0	1502.4
2500.0	1506.4
3000.0	1512.6
3500.0	1519.6
4000.0	1527.3
4500.0	1535.9
4852.0	1542.2

RANGE 23.3 NM	
DEPTH	SOUND SPEED
0.0	1533.1
25.0	1533.3
50.0	1533.7
75.0	1531.7
100.0	1529.5
125.0	1526.4
150.0	1524.7
175.0	1523.8
200.0	1523.5
250.0	1523.6
300.0	1523.3
400.0	1523.3
450.0	1523.1
500.0	1522.3
550.0	1520.8
600.0	1516.1
650.0	1512.5
700.0	1509.1
750.0	1505.7
800.0	1501.2
820.0	1499.6
840.0	1499.0
900.0	1494.3
950.0	1492.0
1000.0	1489.9
1050.0	1489.7
1100.0	1489.5
1150.0	1489.4
1200.0	1489.8
1250.0	1490.3
1300.0	1491.1
1400.0	1492.3
1500.0	1493.8
1600.0	1494.8
1800.0	1496.9
2000.0	1499.6
2200.0	1502.4
2500.0	1506.4
3000.0	1512.6
3500.0	1519.6
4000.0	1527.3
4500.0	1535.9
4812.0	1541.5

RANGE 25.5 NM	
DEPTH	SOUND SPEED
0.0	1532.7
25.0	1533.3
50.0	1533.7
65.0	1533.9
75.0	1532.4
100.0	1528.6
115.0	1527.0
120.0	1527.1
150.0	1525.2
175.0	1524.1
200.0	1523.6
230.0	1523.3
260.0	1523.4
310.0	1523.3
340.0	1523.1
390.0	1523.3
450.0	1522.4
500.0	1520.9
550.0	1518.2
600.0	1513.7
660.0	1506.8
680.0	1506.0
750.0	1499.9
800.0	1496.3
850.0	1493.9
900.0	1491.5
1000.0	1488.7
1100.0	1488.3
1200.0	1489.2
1300.0	1490.4
1400.0	1490.8
1500.0	1492.3
1600.0	1493.2
1800.0	1496.0
2000.0	1499.6
2200.0	1502.4
2500.0	1506.4
3000.0	1512.6
3500.0	1519.6
4000.0	1527.3
4500.0	1535.9
4792.0	1541.2

RANGE 32.0 NM	
DEPTH	SOUND SPEED
0.0	1532.9
25.0	1533.2
50.0	1533.4
75.0	1533.7
90.0	1529.1
100.0	1529.1
125.0	1526.5
150.0	1524.6
175.0	1523.8
200.0	1523.3
250.0	1523.2
300.0	1523.4
350.0	1523.1
400.0	1522.3
440.0	1520.9
460.0	1520.8
500.0	1518.7
550.0	1513.8
600.0	1509.0
650.0	1503.3
700.0	1499.7
750.0	1496.7
800.0	1493.6
850.0	1491.3
900.0	1489.7
950.0	1488.7
990.0	1488.8
1030.0	1488.1
1070.0	1488.3
1100.0	1488.3
1150.0	1488.9
1220.0	1489.4
1240.0	1489.2
1300.0	1490.4
1360.0	1490.5
1380.0	1490.4
1400.0	1490.8
1500.0	1492.3
1600.0	1493.2
1800.0	1496.0
2000.0	1499.9
2200.0	1502.4
2500.0	1506.4
3000.0	1512.6
3500.0	1519.6
4000.0	1527.3
4500.0	1535.9
4777.0	1540.9

RANGE 35.2 NM

DEPTH SOUND SPEED

0.0	1532.8
35.0	1533.2
65.0	1533.6
74.0	1532.2
99.0	1528.6
123.0	1526.3
148.0	1524.5
168.0	1523.5
201.0	1523.0
245.0	1522.3
301.0	1522.5
353.0	1522.2
398.0	1521.1
450.0	1519.2
497.0	1513.8
520.0	1510.6
535.0	1510.0
559.0	1506.6
599.0	1501.8
653.0	1498.3
690.0	1495.5
703.0	1495.0
750.0	1492.1
798.0	1489.8
832.0	1488.3
900.0	1487.0
950.0	1486.8
1000.0	1487.1
1100.0	1488.0
1200.0	1488.6
1300.0	1489.6
1400.0	1490.4
1500.0	1492.0
1600.0	1493.1
1800.0	1496.4
2000.0	1499.6
2200.0	1502.4
2500.0	1506.4
3000.0	1512.6
3500.0	1519.6
4000.0	1527.3
4500.0	1535.9
4771.0	1540.8

RANGE 40.8 NM

DEPTH SOUND SPEED

0.0	1534.8
25.0	1535.2
50.0	1535.6
65.0	1535.5
100.0	1531.5
125.0	1525.0
150.0	1523.3
200.0	1522.2
250.0	1521.6
300.0	1521.4
350.0	1520.2
400.0	1516.8
450.0	1510.9
500.0	1505.0
600.0	1495.8
610.0	1495.6
640.0	1494.4
700.0	1491.0
770.0	1488.4
820.0	1488.1
860.0	1487.1
900.0	1486.5
930.0	1486.9
960.0	1486.8
1000.0	1487.1
1050.0	1487.3
1100.0	1488.0
1130.0	1488.5
1150.0	1488.2
1200.0	1488.6
1300.0	1489.6
1400.0	1490.4
1500.0	1492.0
1600.0	1493.1
1800.0	1496.4
2000.0	1499.6
2200.0	1502.4
2500.0	1506.4
3000.0	1512.6
3500.0	1519.6
4000.0	1527.3
4500.0	1535.9
4761.0	1540.6

RANGE 43.8 NM	
DEPTH	SOUND SPEED
0.0	1534.8
25.0	1535.3
50.0	1535.8
85.0	1536.5
100.0	1532.8
125.0	1529.0
150.0	1526.2
175.0	1523.9
190.0	1522.5
200.0	1522.1
250.0	1520.6
260.0	1520.4
280.0	1520.4
300.0	1519.2
350.0	1515.2
380.0	1509.1
420.0	1505.9
450.0	1503.1
500.0	1498.4
550.0	1493.7
580.0	1492.9
600.0	1491.4
650.0	1488.4
680.0	1487.2
710.0	1487.4
730.0	1487.1
800.0	1486.0
850.0	1485.5
900.0	1486.2
1000.0	1487.1
1100.0	1488.0
1200.0	1488.6
1300.0	1489.6
1400.0	1490.4
1500.0	1492.0
1600.0	1493.1
1800.0	1496.4
2000.0	1499.6
2200.0	1502.4
2500.0	1506.4
3000.0	1512.6
3500.0	1519.6
4000.0	1527.3
4500.0	1535.9
4761.0	1540.6

RANGE 46.5 NM	
DEPTH	SOUND SPEED
0.0	1534.2
25.0	1534.6
50.0	1535.0
75.0	1536.6
85.0	1536.7
95.0	1533.2
100.0	1533.1
105.0	1532.6
110.0	1532.4
120.0	1529.5
125.0	1529.5
150.0	1527.5
175.0	1524.2
200.0	1521.4
240.0	1518.1
280.0	1510.3
300.0	1508.8
350.0	1505.6
400.0	1501.4
450.0	1497.8
500.0	1494.2
530.0	1492.7
540.0	1492.8
600.0	1489.4
650.0	1486.7
700.0	1486.1
750.0	1485.7
800.0	1484.8
900.0	1485.4
1000.0	1486.2
1100.0	1486.5
1200.0	1487.8
1300.0	1488.7
1400.0	1489.7
1500.0	1491.2
1600.0	1492.6
1800.0	1495.7
2000.0	1499.6
2200.0	1502.4
2500.0	1506.4
3000.0	1512.6
3500.0	1519.6
4000.0	1527.3
4500.0	1535.9
4758.0	1540.5

RANGE 47.9 NM

DEPTH	SOUND SPEED
0.0	1533.7
25.0	1534.3
50.0	1535.1
75.0	1535.8
100.0	1531.6
125.0	1529.1
150.0	1525.6
175.0	1522.7
200.0	1517.7
250.0	1509.6
260.0	1509.6
300.0	1506.4
340.0	1503.9
350.0	1503.6
400.0	1499.9
450.0	1495.9
510.0	1493.4
530.0	1493.5
550.0	1491.6
600.0	1490.0
650.0	1488.1
700.0	1486.9
750.0	1485.4
800.0	1484.9
820.0	1484.8
850.0	1484.9
900.0	1485.4
970.0	1486.3
990.0	1486.2
1040.0	1486.3
1070.0	1486.2
1100.0	1486.5
1200.0	1487.8
1300.0	1488.7
1400.0	1489.7
1500.0	1491.2
1600.0	1492.6
1800.0	1495.7
2000.0	1498.2
2200.0	1501.3
2500.0	1505.4
3000.0	1512.1
3500.0	1519.2
4000.0	1527.1
4500.0	1535.9
4757.0	1540.5

RANGE 49.8 NM

DEPTH	SOUND SPEED
0.0	1533.7
20.0	1534.0
45.0	1534.9
70.0	1531.5
85.0	1534.2
100.0	1531.4
125.0	1526.0
150.0	1519.3
160.0	1520.8
180.0	1511.9
195.0	1510.8
200.0	1510.4
250.0	1507.0
300.0	1503.7
340.0	1501.2
350.0	1501.0
400.0	1498.0
470.0	1493.6
490.0	1493.8
550.0	1490.2
560.0	1490.2
620.0	1487.4
640.0	1487.3
690.0	1485.1
720.0	1484.9
760.0	1484.3
780.0	1484.4
800.0	1484.2
850.0	1484.9
900.0	1485.2
920.0	1485.1
970.0	1485.2
1000.0	1485.8
1100.0	1486.1
1200.0	1486.9
1300.0	1488.1
1400.0	1489.2
1500.0	1490.5
1600.0	1492.3
1800.0	1495.1
2000.0	1498.0
2200.0	1501.3
2500.0	1505.4
3000.0	1512.1
3500.0	1519.2
4000.0	1527.1
4500.0	1535.9
4754.0	1540.5

RANGE 51.3 NM	
DEPTH	SOUND SPEED
0.0	1532.5
25.0	1533.0
40.0	1531.9
55.0	1531.0
65.0	1530.9
85.0	1532.9
100.0	1524.7
115.0	1522.0
125.0	1525.3
150.0	1515.3
175.0	1509.7
185.0	1508.5
200.0	1509.1
250.0	1505.4
300.0	1502.3
350.0	1498.7
400.0	1495.4
440.0	1493.8
450.0	1493.8
510.0	1490.0
520.0	1490.2
560.0	1487.6
600.0	1487.2
650.0	1485.6
700.0	1484.5
740.0	1483.9
770.0	1484.2
810.0	1484.2
830.0	1484.4
870.0	1484.1
900.0	1484.4
980.0	1485.2
1000.0	1485.1
1050.0	1485.5
1100.0	1486.1
1200.0	1486.8
1300.0	1488.0
1400.0	1489.2
1500.0	1490.5
1600.0	1492.3
1800.0	1495.1
2000.0	1498.0
2200.0	1501.3
2500.0	1505.4
3000.0	1512.1
3500.0	1519.2
4000.0	1527.1
4500.0	1535.9
4752.0	1540.4

RANGE 52.7 NM	
DEPTH	SOUND SPEED
0.0	1530.4
15.0	1530.5
35.0	1529.8
60.0	1530.2
75.0	1527.4
85.0	1530.0
100.0	1528.6
110.0	1522.8
120.0	1527.7
150.0	1510.1
160.0	1511.6
175.0	1510.0
200.0	1508.6
250.0	1504.3
300.0	1500.8
350.0	1497.7
400.0	1494.3
420.0	1494.3
450.0	1492.3
510.0	1489.0
530.0	1488.9
550.0	1488.1
600.0	1485.9
650.0	1485.2
700.0	1484.5
720.0	1484.4
750.0	1484.7
810.0	1484.5
850.0	1484.8
900.0	1485.2
1000.0	1485.4
1060.0	1486.1
1090.0	1485.7
1150.0	1486.8
1200.0	1487.7
1300.0	1488.5
1400.0	1489.7
1500.0	1491.3
1600.0	1492.4
1800.0	1495.1
2000.0	1498.0
2200.0	1501.3
2500.0	1505.4
3000.0	1512.1
3500.0	1519.2
4000.0	1527.1
4500.0	1535.9
4750.0	1540.4

RANGE 55.1 NM	
DEPTH	SOUND SPEED
0.0	1529.1
20.0	1529.2
40.0	1528.3
55.0	1528.6
75.0	1522.5
85.0	1520.9
95.0	1521.5
130.0	1515.0
140.0	1516.9
150.0	1513.4
155.0	1513.8
175.0	1509.7
200.0	1505.8
250.0	1502.6
300.0	1498.9
350.0	1496.2
400.0	1493.6
450.0	1491.5
500.0	1488.9
550.0	1486.7
600.0	1485.3
650.0	1484.4
690.0	1483.9
710.0	1484.0
750.0	1483.7
780.0	1483.6
800.0	1483.8
860.0	1483.8
900.0	1484.0
950.0	1484.4
990.0	1484.8
1000.0	1485.4
1100.0	1485.8
1200.0	1487.7
1300.0	1488.5
1400.0	1489.7
1500.0	1491.3
1600.0	1492.4
1800.0	1495.6
2000.0	1498.3
2200.0	1501.3
2500.0	1505.4
3000.0	1512.1
3500.0	1519.2
4000.0	1527.1
4500.0	1535.9
4750.0	1540.4

RANGE 58.6 NM	
DEPTH	SOUND SPEED
0.0	1525.5
20.0	1525.8
40.0	1524.8
65.0	1520.7
70.0	1521.0
75.0	1520.9
90.0	1524.4
100.0	1521.3
125.0	1517.4
150.0	1513.0
175.0	1510.2
200.0	1505.7
250.0	1501.5
260.0	1501.2
300.0	1497.4
350.0	1493.9
360.0	1493.7
400.0	1490.8
420.0	1489.7
440.0	1489.5
490.0	1486.1
500.0	1486.0
550.0	1484.7
600.0	1483.3
660.0	1482.6
690.0	1482.7
710.0	1482.4
750.0	1482.8
780.0	1482.3
820.0	1482.9
870.0	1483.3
950.0	1484.7
1000.0	1485.2
1100.0	1486.3
1200.0	1487.1
1300.0	1488.2
1400.0	1489.7
1500.0	1491.2
1600.0	1492.6
1800.0	1495.2
2000.0	1498.0
2200.0	1500.4
2500.0	1504.6
3000.0	1511.3
3500.0	1519.0
4000.0	1526.9
4500.0	1535.9
4744.0	1540.3

RANGE 61.1 NM	
DEPTH	SOUND SPEED
0.0	1526.8
20.0	1527.1
45.0	1526.5
60.0	1525.7
65.0	1525.8
75.0	1521.8
80.0	1521.8
100.0	1518.4
105.0	1519.5
125.0	1511.4
145.0	1508.0
150.0	1508.1
185.0	1506.3
200.0	1505.1
220.0	1504.3
230.0	1504.3
290.0	1498.4
310.0	1497.3
350.0	1495.6
390.0	1491.8
400.0	1491.4
460.0	1488.3
500.0	1487.1
530.0	1486.1
600.0	1484.5
650.0	1483.2
700.0	1482.4
740.0	1482.0
800.0	1482.7
850.0	1483.0
900.0	1483.8
950.0	1484.8
1000.0	1485.2
1100.0	1486.3
1200.0	1487.1
1300.0	1488.2
1400.0	1489.7
1500.0	1491.2
1600.0	1492.6
1800.0	1495.2
2000.0	1498.0
2200.0	1500.4
2500.0	1504.6
3000.0	1511.3
3500.0	1519.0
4000.0	1526.9
4500.0	1535.9
4729.0	1540.0

RANGE 65.6 NM	
DEPTH	SOUND SPEED
0.0	1525.2
27.0	1525.7
61.0	1518.0
69.0	1520.1
75.0	1516.6
82.0	1521.7
101.0	1512.5
132.0	1508.8
169.0	1506.0
184.0	1506.2
205.0	1504.8
219.0	1504.0
249.0	1501.4
302.0	1497.3
338.0	1492.9
394.0	1490.3
448.0	1488.4
501.0	1485.3
548.0	1483.7
598.0	1482.6
618.0	1481.7
633.0	1481.8
671.0	1481.1
685.0	1481.3
713.0	1481.0
750.0	1481.3
799.0	1481.9
855.0	1482.7
900.0	1483.3
1000.0	1484.3
1100.0	1485.4
1200.0	1487.2
1300.0	1488.8
1400.0	1490.2
1500.0	1491.3
1600.0	1492.7
1800.0	1495.6
2000.0	1498.6
2200.0	1501.3
2500.0	1505.4
3000.0	1512.1
3500.0	1519.2
4000.0	1527.1
4500.0	1535.9
4739.0	1540.2

RANGE 68.8 NM

DEPTH SOUND SPEED

0.0	1523.2
15.0	1523.3
45.0	1520.6
60.0	1520.9
75.0	1519.0
85.0	1521.6
95.0	1516.0
105.0	1512.3
120.0	1515.0
140.0	1513.6
150.0	1513.5
175.0	1511.5
200.0	1509.1
250.0	1502.2
300.0	1498.4
350.0	1493.9
400.0	1491.1
450.0	1488.0
500.0	1485.6
550.0	1484.0
600.0	1482.7
620.0	1482.3
650.0	1482.8
680.0	1482.3
720.0	1482.9
750.0	1482.7
790.0	1482.4
850.0	1482.9
900.0	1483.3
950.0	1483.8
1000.0	1484.3
1100.0	1485.4
1200.0	1487.2
1300.0	1488.8
1400.0	1490.2
1500.0	1491.3
1600.0	1492.7
1800.0	1495.6
1900.0	1497.0
2000.0	1498.0
2200.0	1501.3
2500.0	1505.4
3000.0	1512.1
4000.0	1527.1
4500.0	1535.9
4783.0	1540.8

APPENDIX B

CFIELD SOUND SPEED INTERPOLATION METHOD

Sound speed profile interpolations were constructed using CFIELD; the particular version of CFIELD used for this study was established from Ref. 10, RAYWAVE II. RAYWAVE II is a long-range, low-frequency transmission loss model. Ray theory and wave theory are combined to obtain low-frequency transmission loss estimates. The initial intent of RAYWAVE was to address local environmental conditions, i.e. evaluate in a detailed manner the performance of a single array under very specific environmental conditions. Thus, RAYWAVE was ideal to use for interpolation of SSPs over the restricted environmental area this study was concerned with.

The unique technique used is called the Triangular Sector Method (Ref. 10). It involves constructing triangle cross-sections from adjacent sound speed profile depth values (Figure B1).

Two sound speed profiles, from which the interpolation is to be implemented, are constructed from constant gradient segments. Interface depths are established as points on the gradient segments that are joined and then these depths are positioned on a vertical line at sound speed profile ranges R_A and R_B

(In Figure B1 these line segments join to become the sides of triangles.) These points are connected across each profile to create a series of triangular sectors running from the surface to the sea floor.

The first triangle thus constructed is a right triangle--its vertex is at the profile having the greatest second interface depth, or if the second interface depths coincide, the vertex is placed on the profile with the greatest sound speed gradient.

The other triangles, which generally are not right triangles, are constructed differently. The vertices of the next triangles are placed at depths representing sound speed minima. If neither is a minimum, the triangle sides are selected to subtend the gradient which is closest to the gradient of the preceding triangle. To prevent extreme imbalance in triangle side slope, an additional algorithm is set up such that selected points on a profile may not extend below the next two points on the adjacent profile.

These triangles so generated are the basis for computing the sound speed field used in ray path computations. For determining $C(R,Z)$ for all possible triangular configurations, the following expression is applied (see Figure B2):

$$C(R,Z) = C_v +/ - g_r (R-R_v) + g_z (Z_v-Z)$$

where

$g_z = \frac{C_2 - C_1}{Z_2 - Z_1}$, is the sound speed gradient in the
z-direction

$g_r = \frac{C_V - C_X}{R_V - R_S}$, is the sound speed gradient in the R
direction

$$\text{and } C_X = C_1 + g_z (Z_V - Z_1)$$

Z_V = vertex point depth

C_V = vertex point sound speed

Z_1, C_1 = upper point of open triangle side

Z_2, C_2 = lower point of open triangle side

R_V = range of vertex point

R_S = range of open side of triangle

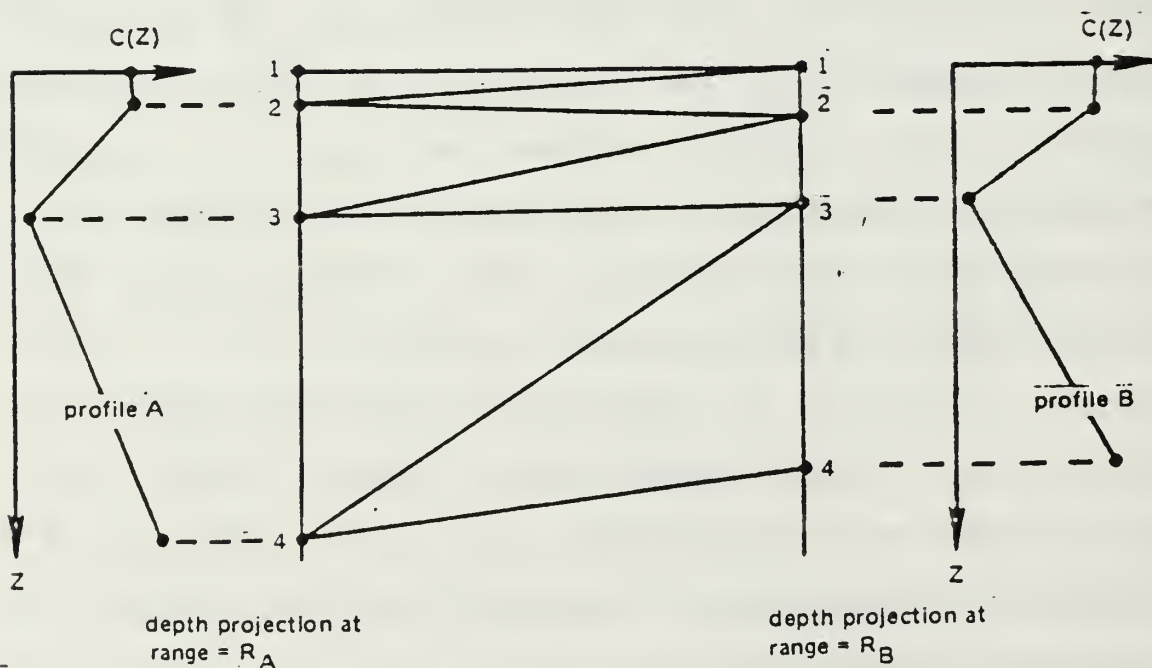


Figure B1. Triangular Sector Description (after Watson, McGirr 1975)

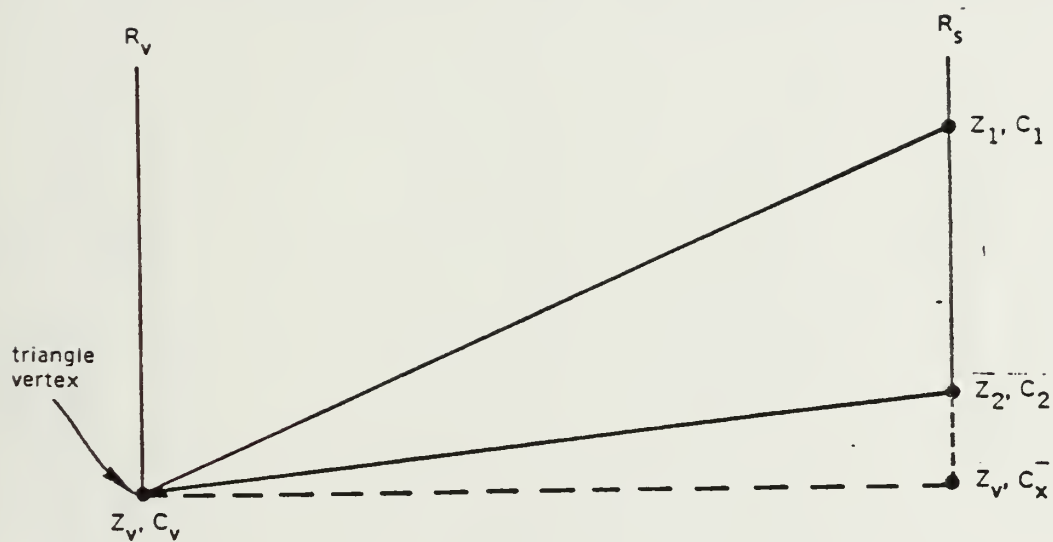


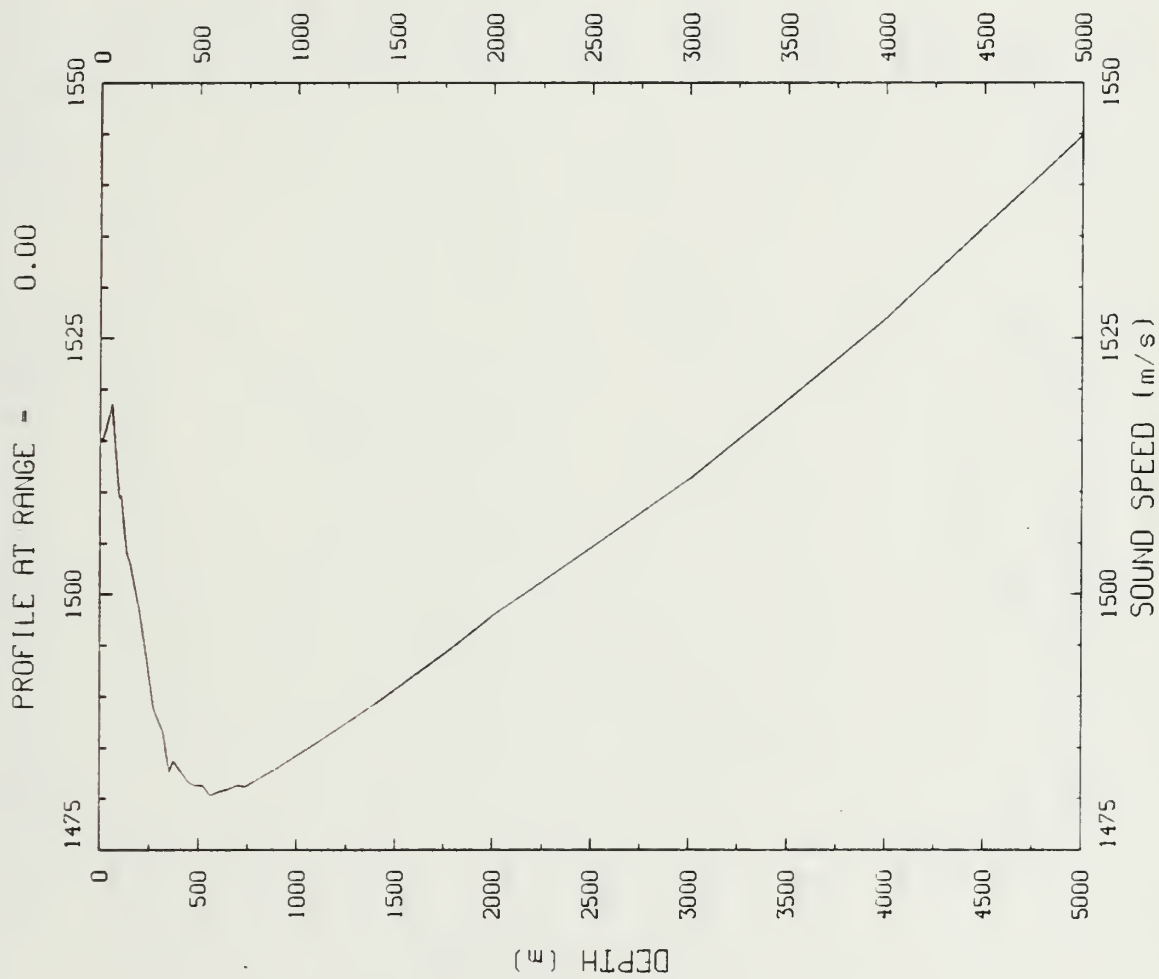
Figure B2. Typical Triangle with Generalized Labels
(after Watson and McGirr, 1975)

APPENDIX C

SAMPLE SSP INTERPOLATIONS

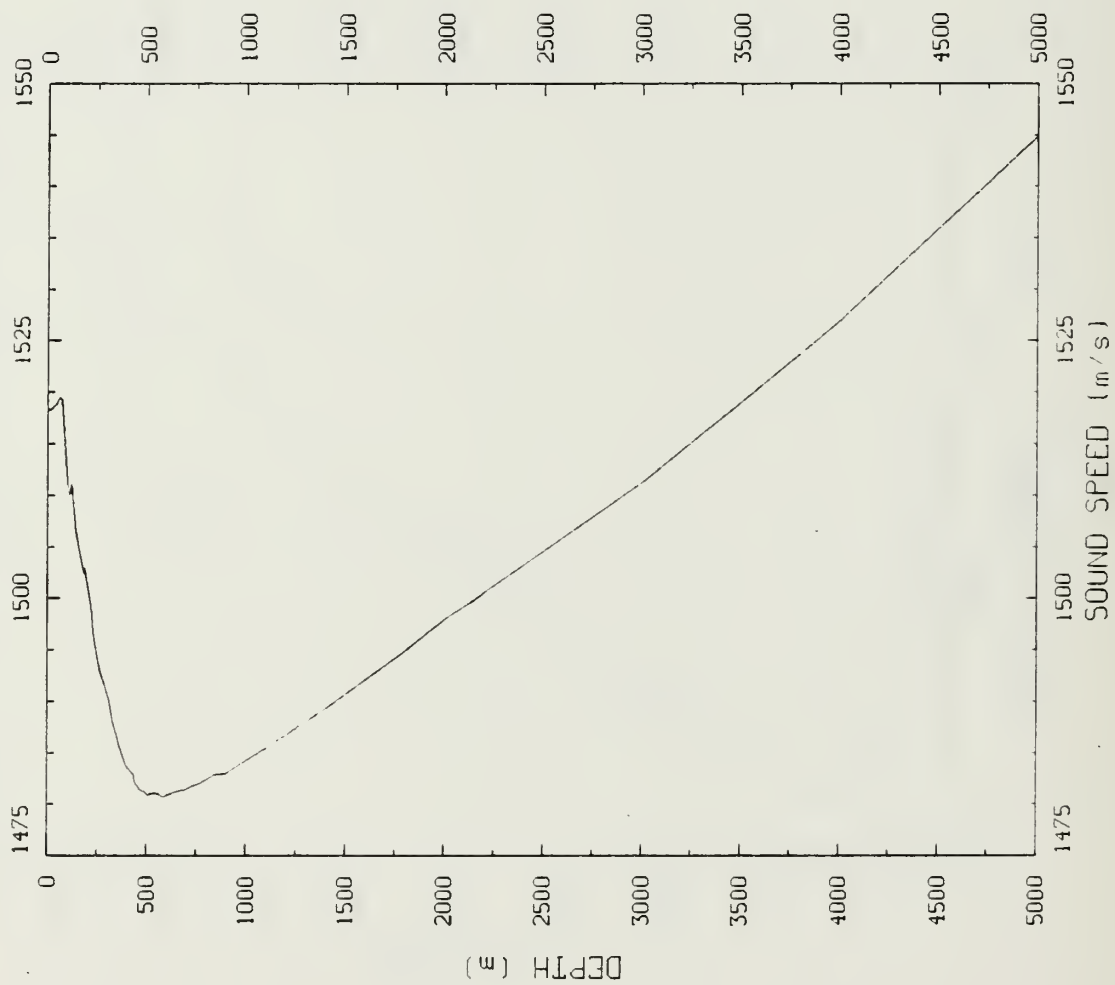
Enclosed are samples of interpolated sound speed profiles generated by CFIELD.

1TRACK1



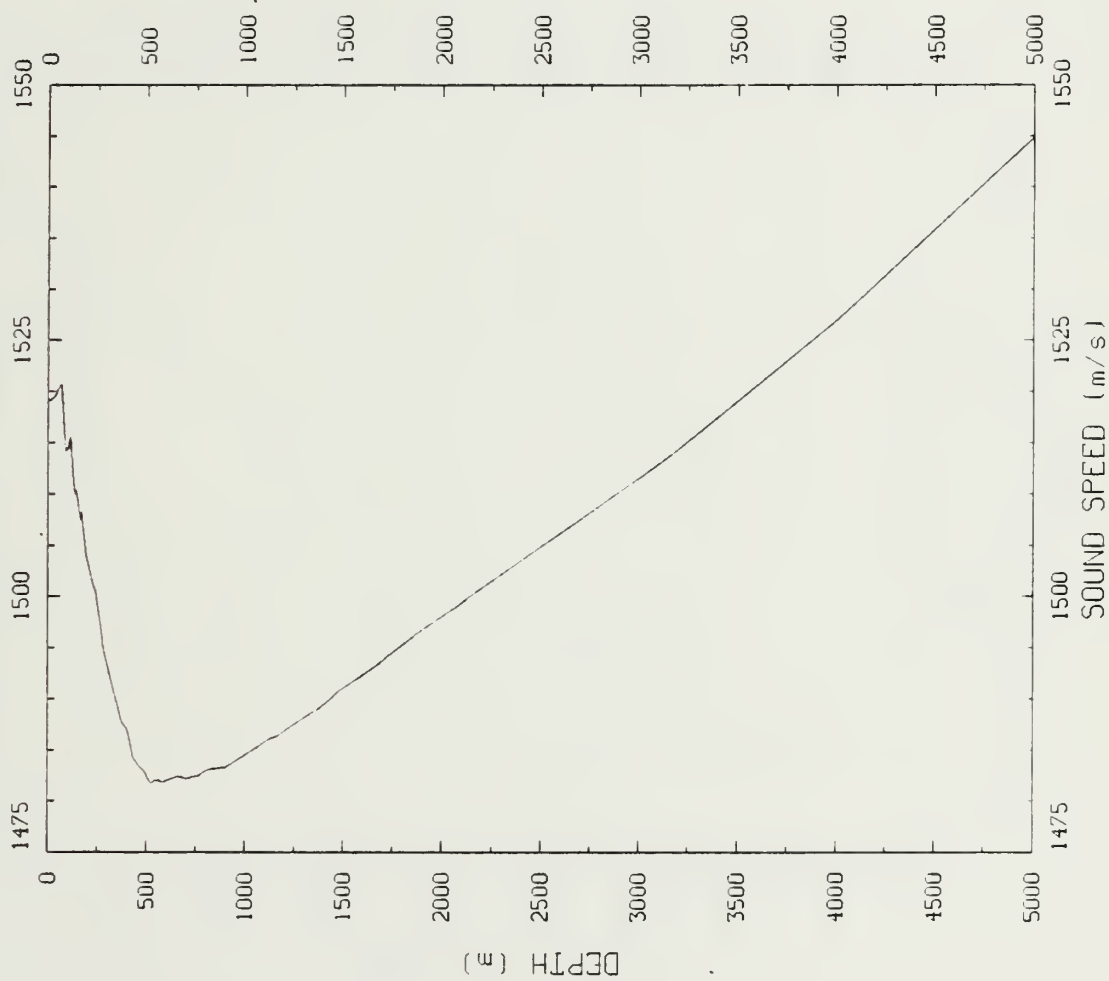
2TRACK1

PROFILE INTERPOLATED AT RANGE - 7.185



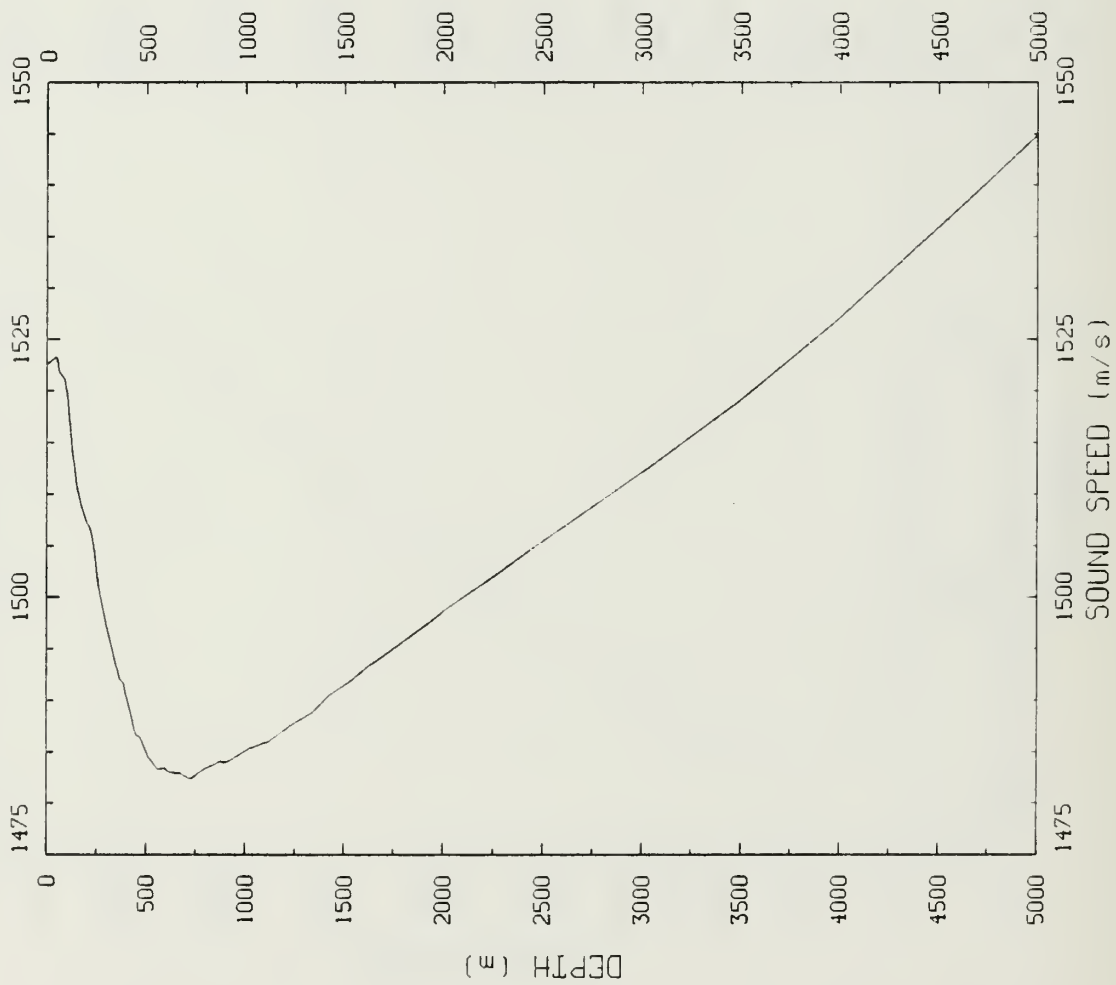
3TRACK1

PROFILE INTERPOLATED AT RANGE = 12.556



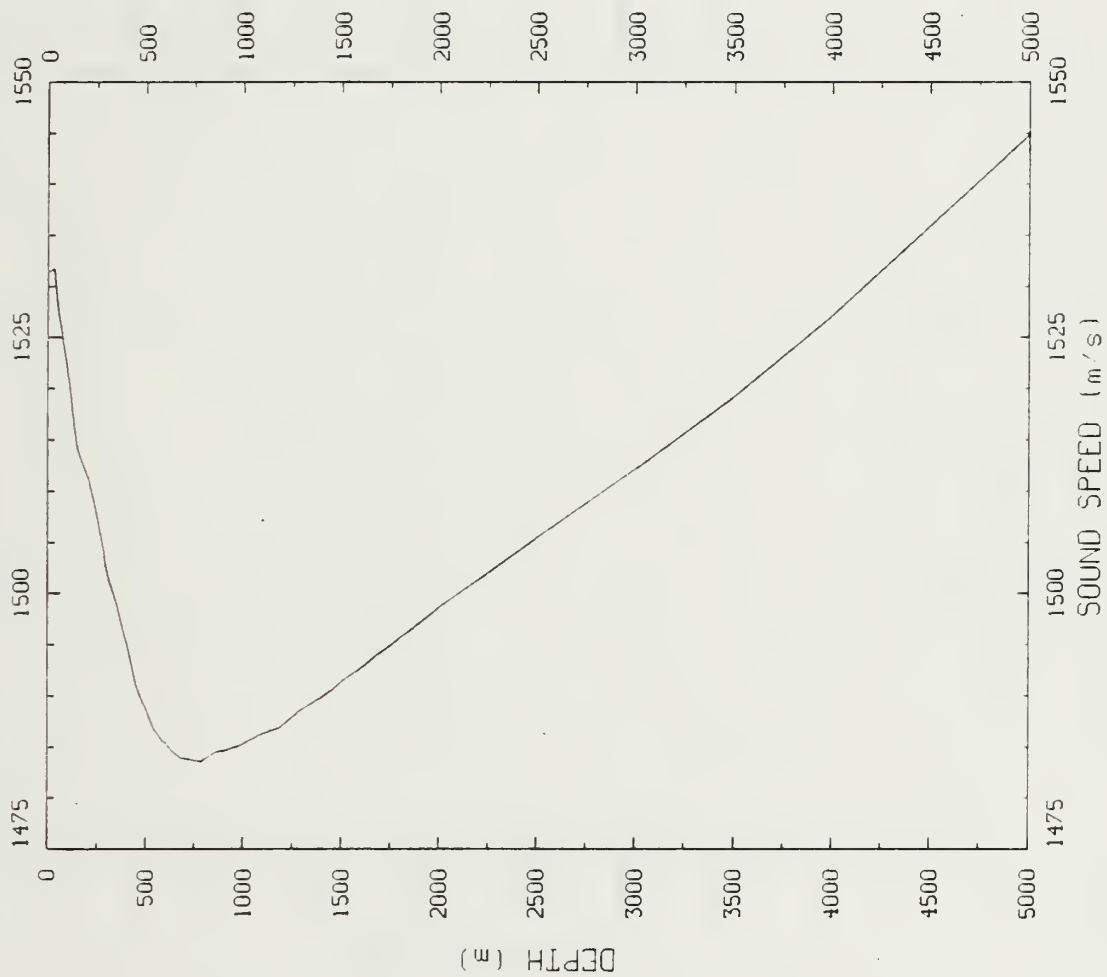
4TRACK1

PROFILE INTERPOLATED AT RANGE = 18.297



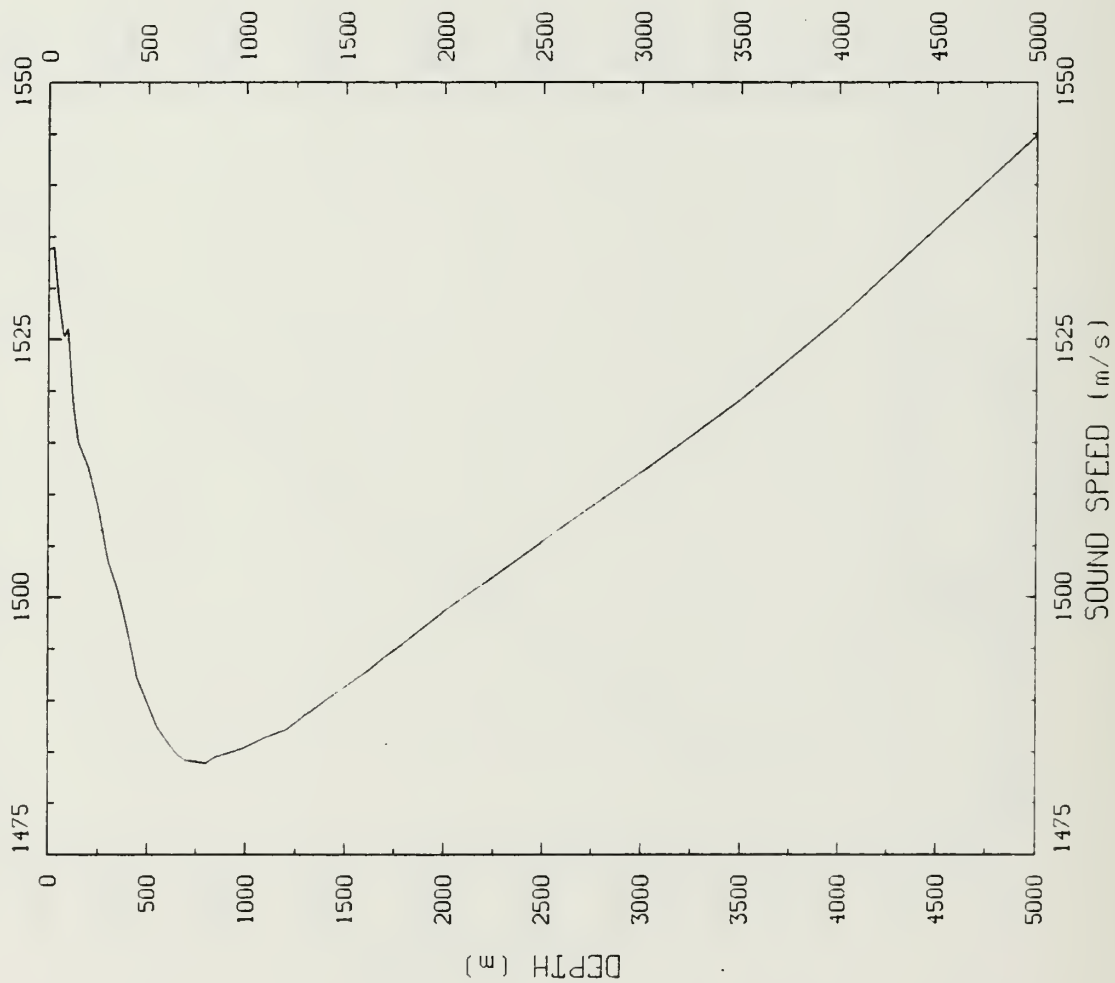
4TRACK1

PROFILE INTERPOLATED AT RANGE - 24.297



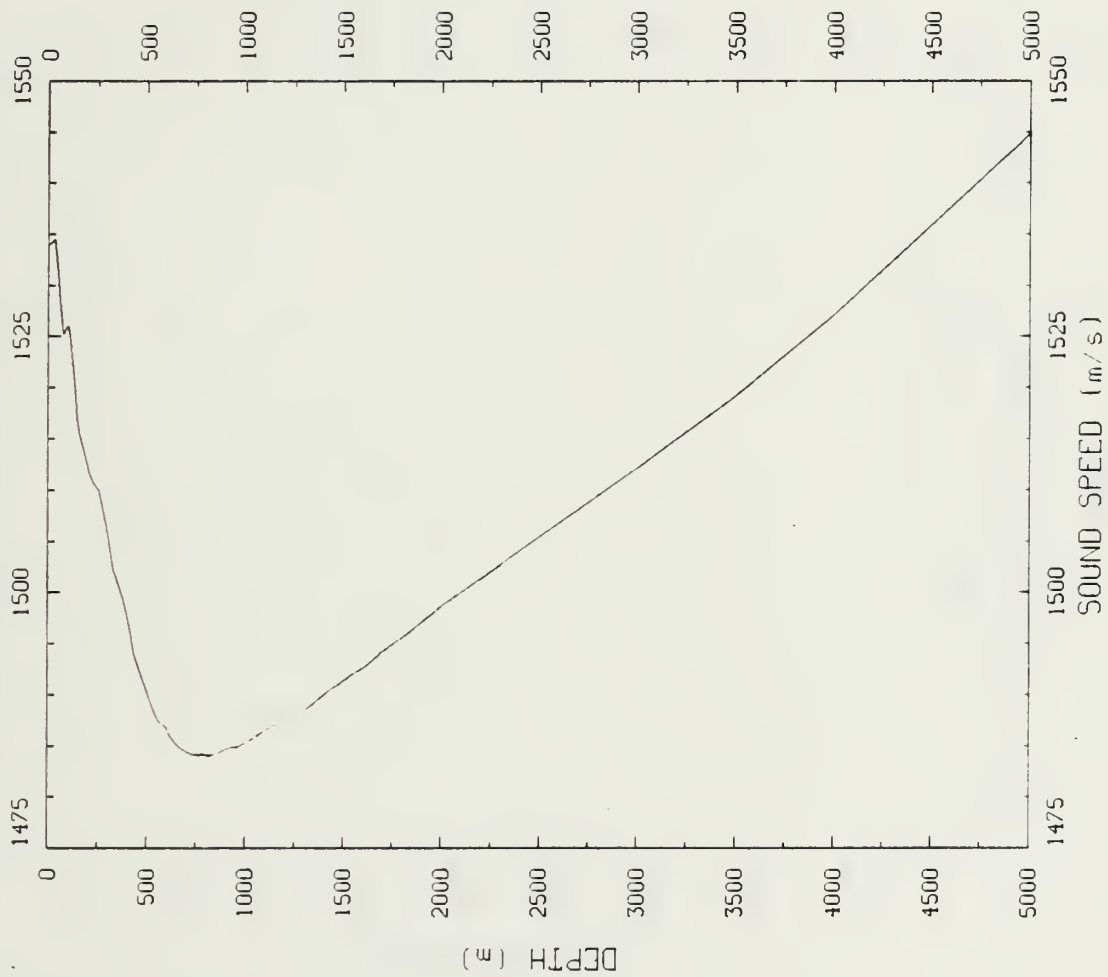
5TRACK1

PROFILE AT RANGE = 25.928



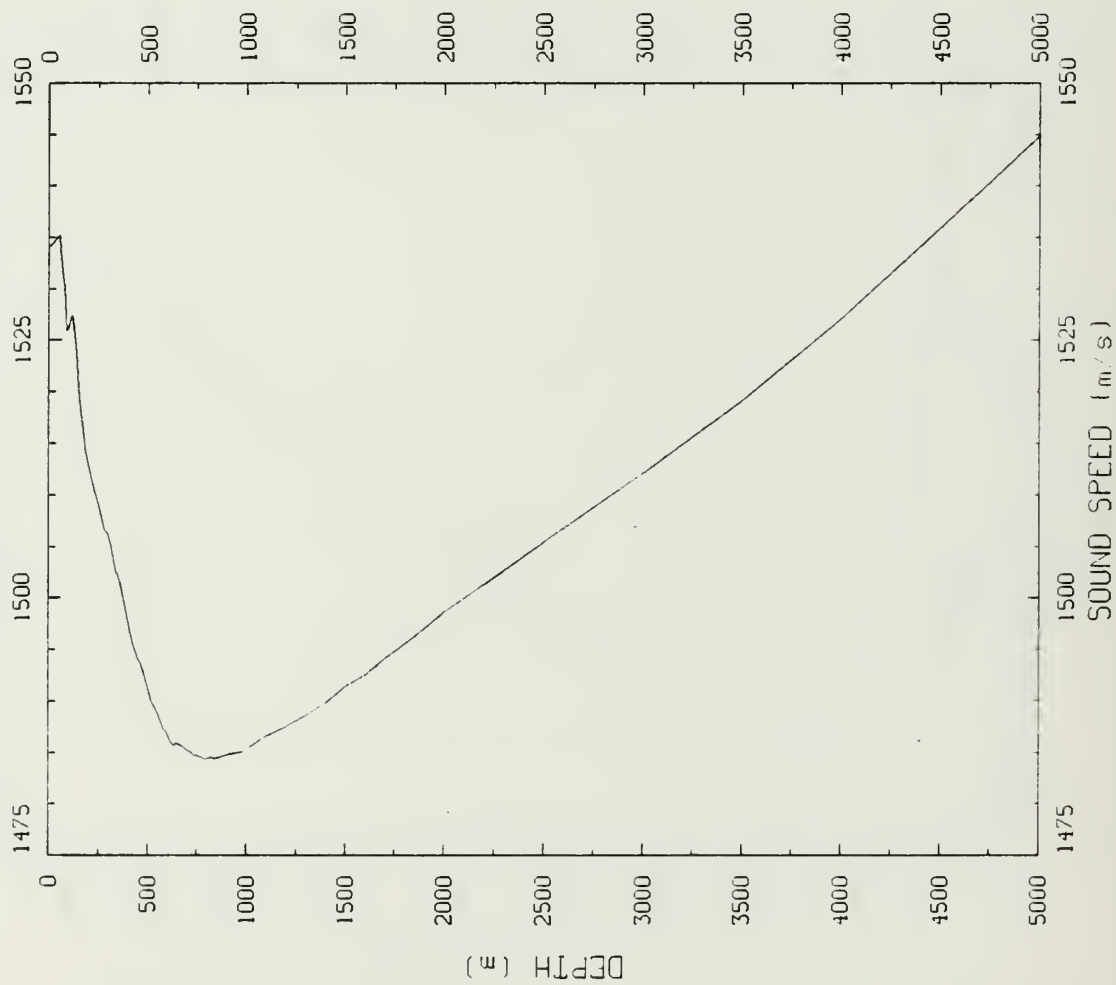
STRACK1

PROFILE INTERPOLATED AT RANGE - 27.428

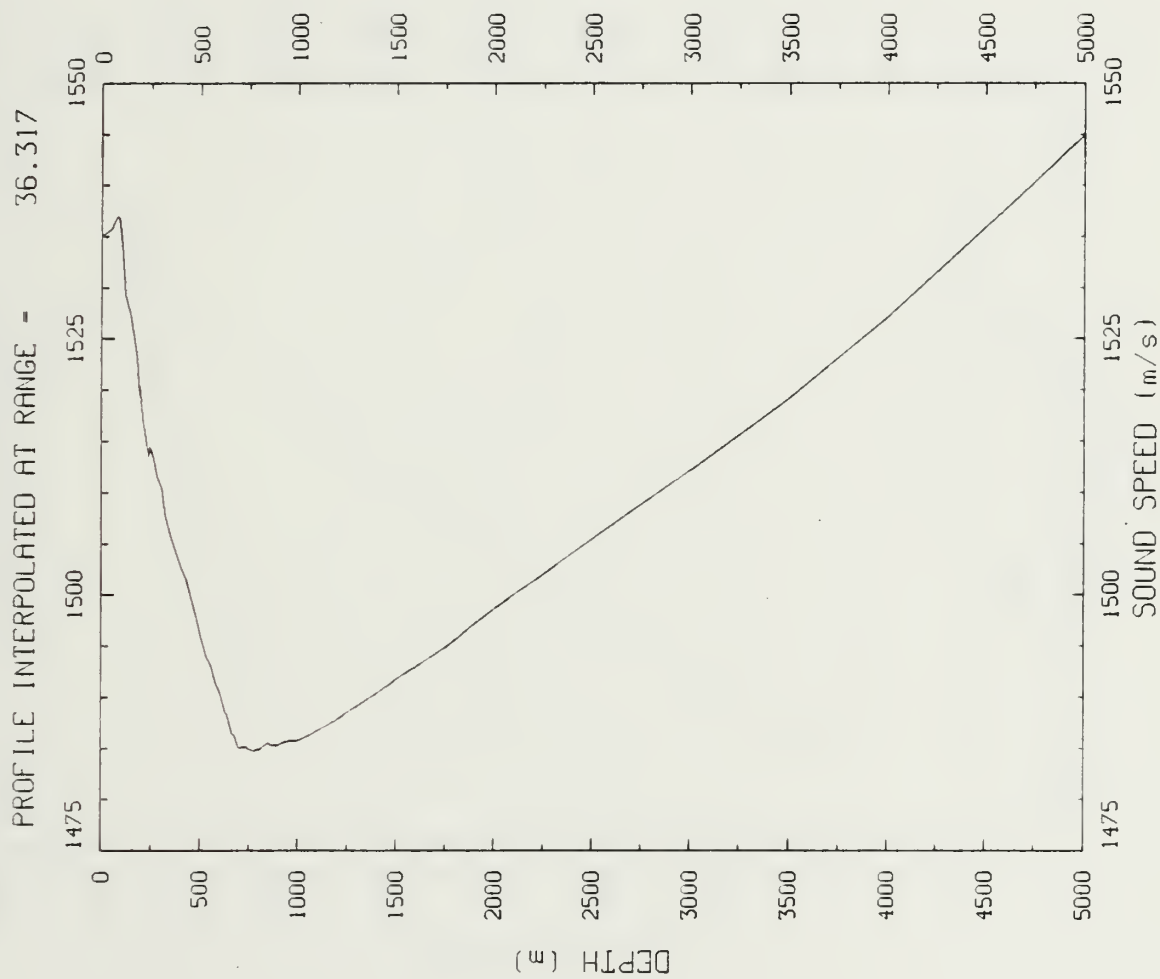


6TRACK1

PROFILE INTERPOLATED AT RANGE - 30.335

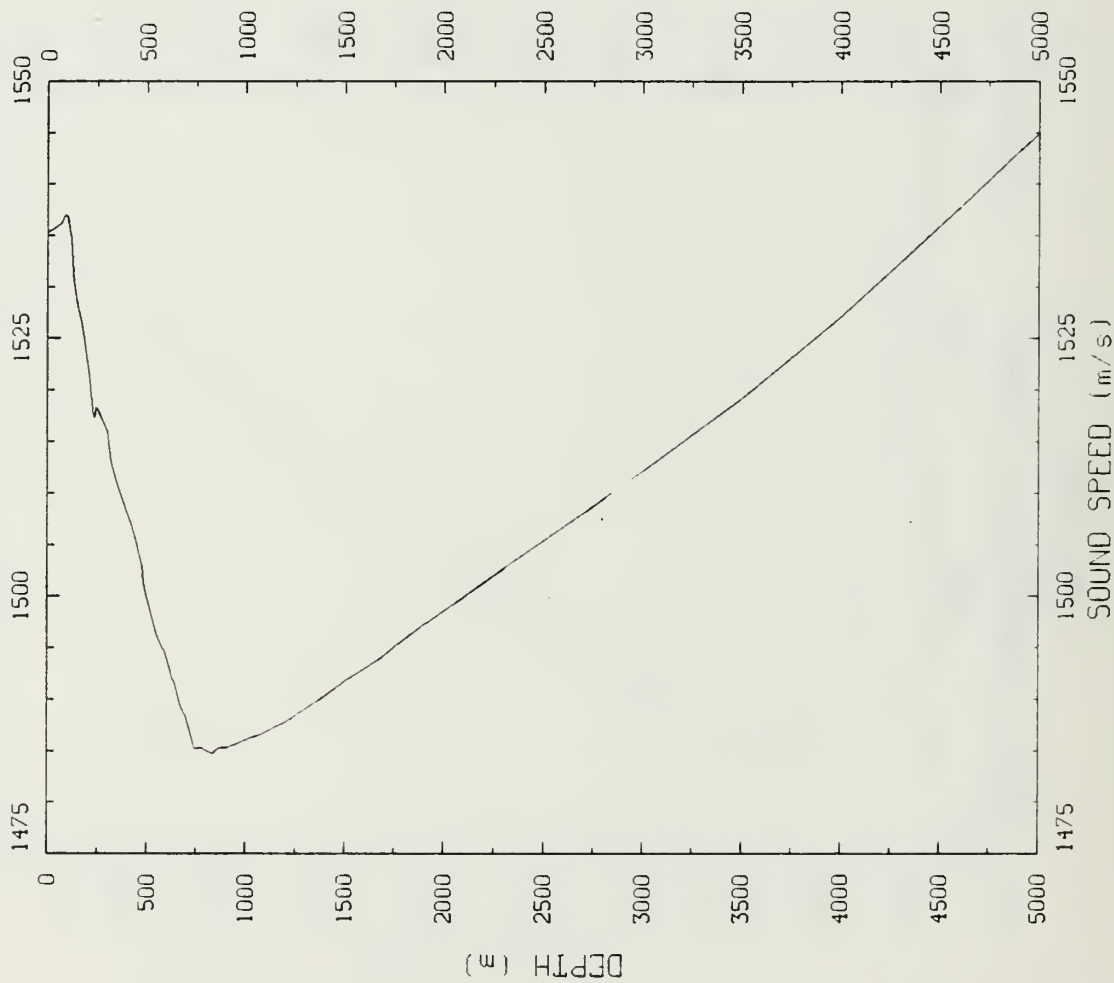


8TRACK1



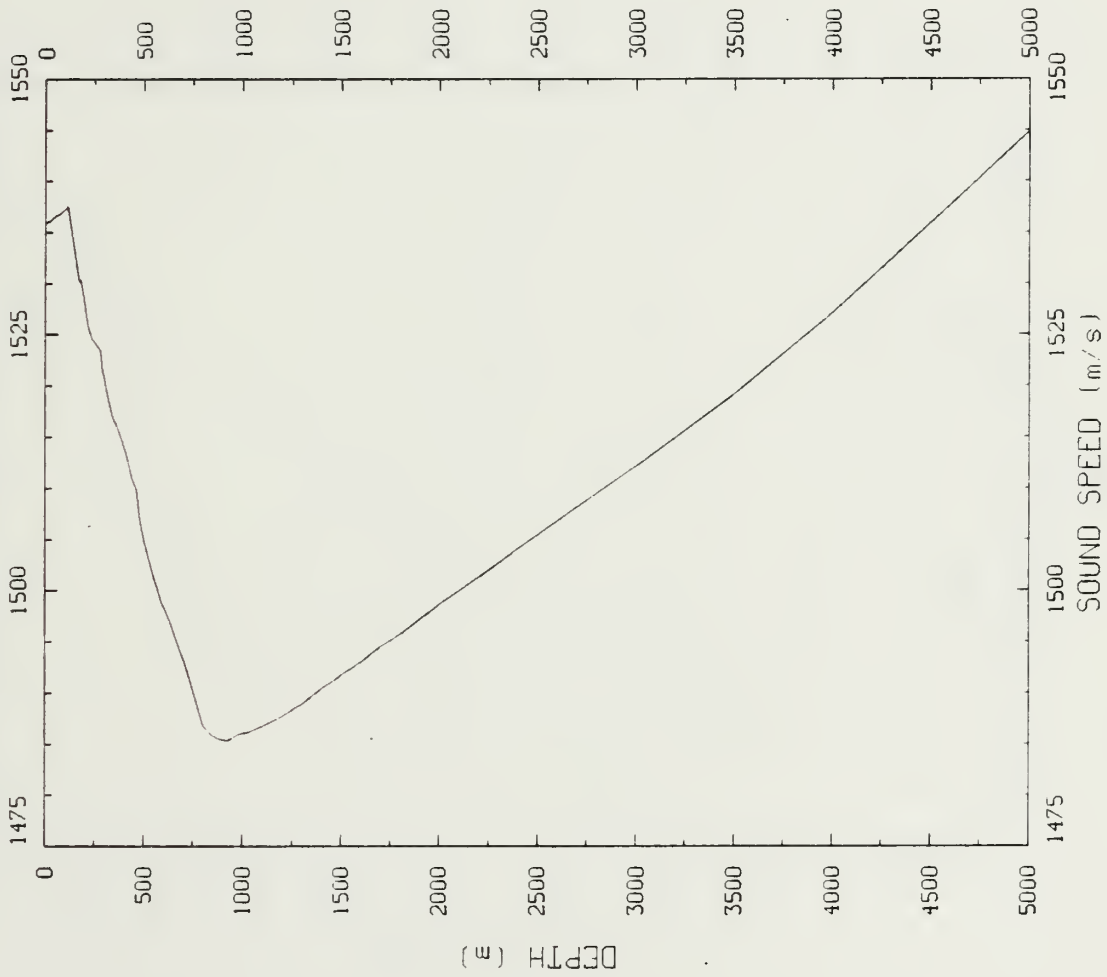
9TRACK1

PROFILE INTERPOLATED AT RANGE - 41.410



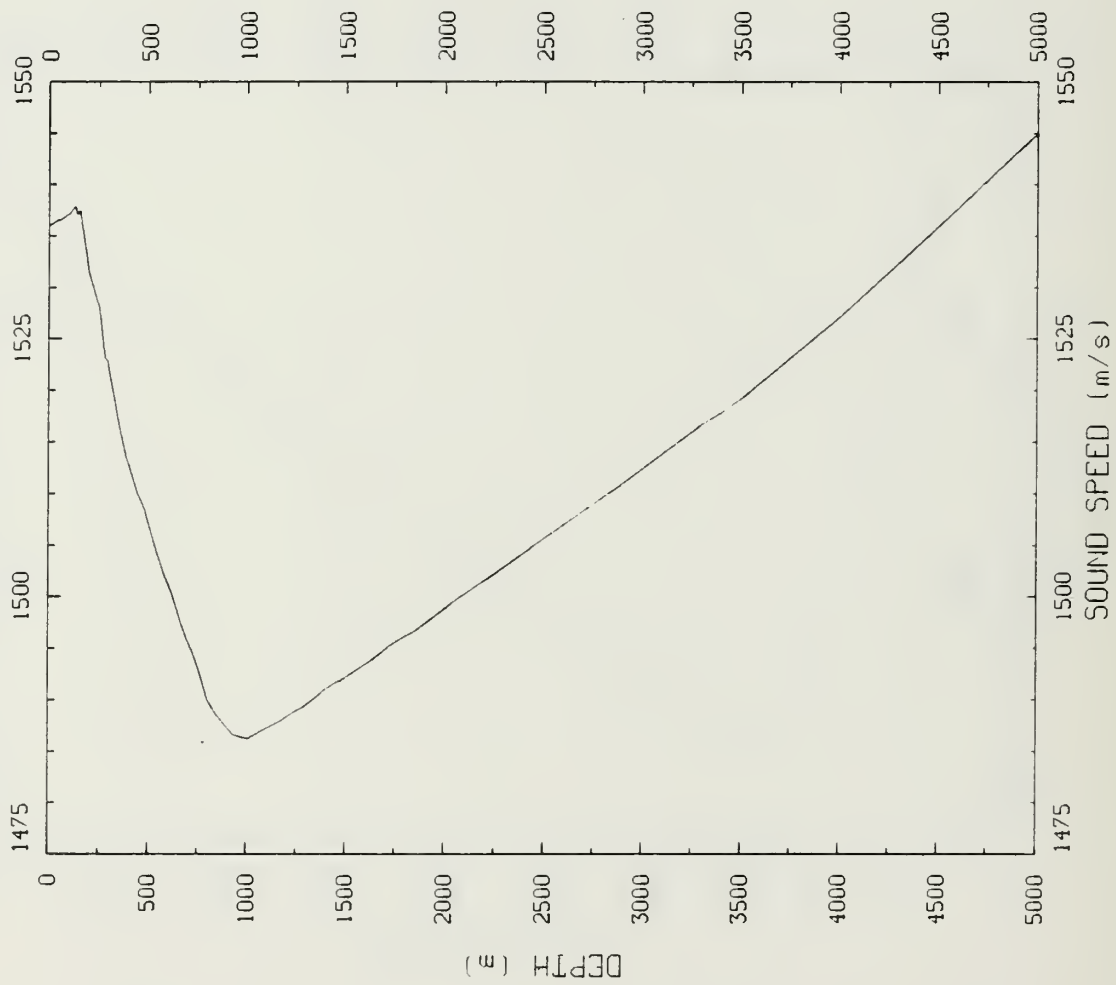
10TRACK1

PROFILE INTERPOLATED AT RANGE - 52.152



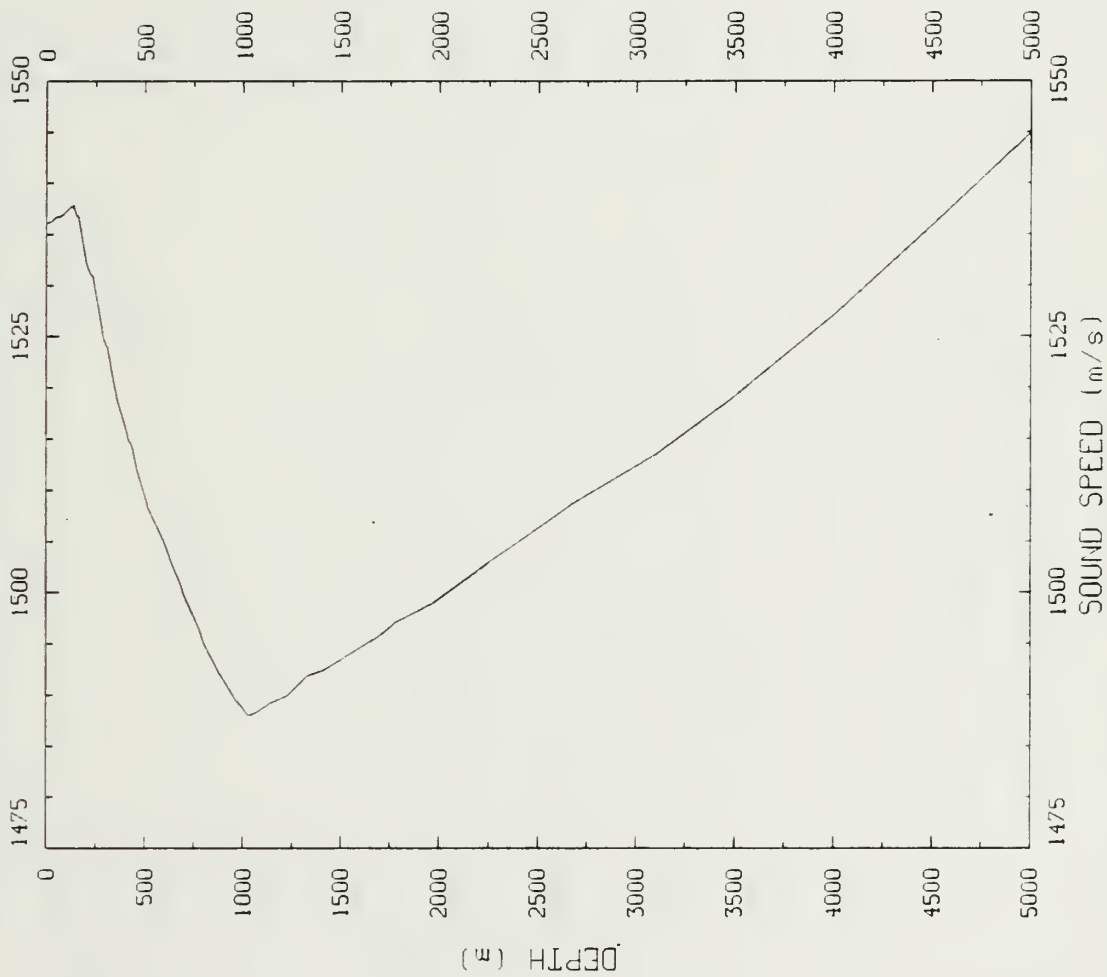
11TRACK1

PROFILE INTERPOLATED AT RANGE = 59.967



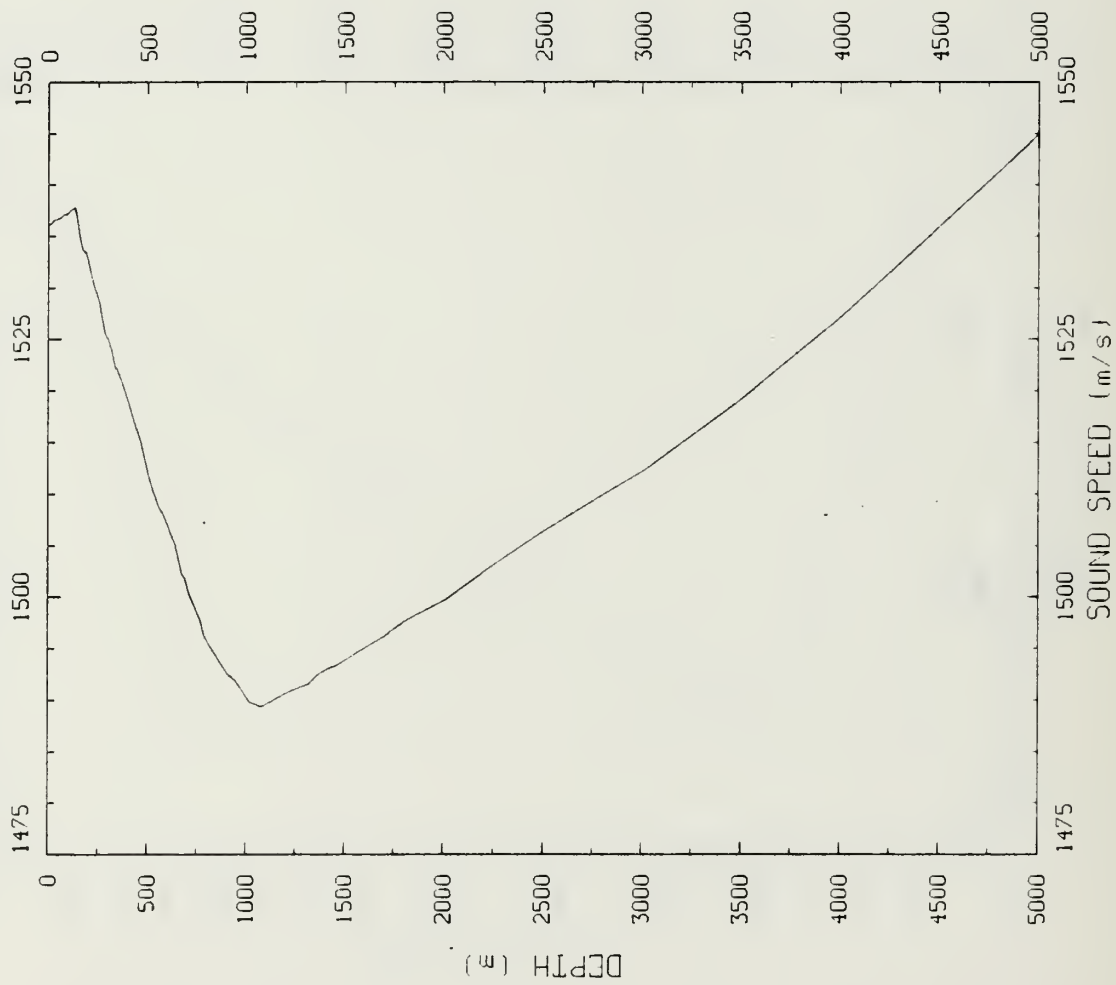
11TRACK1

PROFILE INTERPOLATED AT RANGE = 65.967



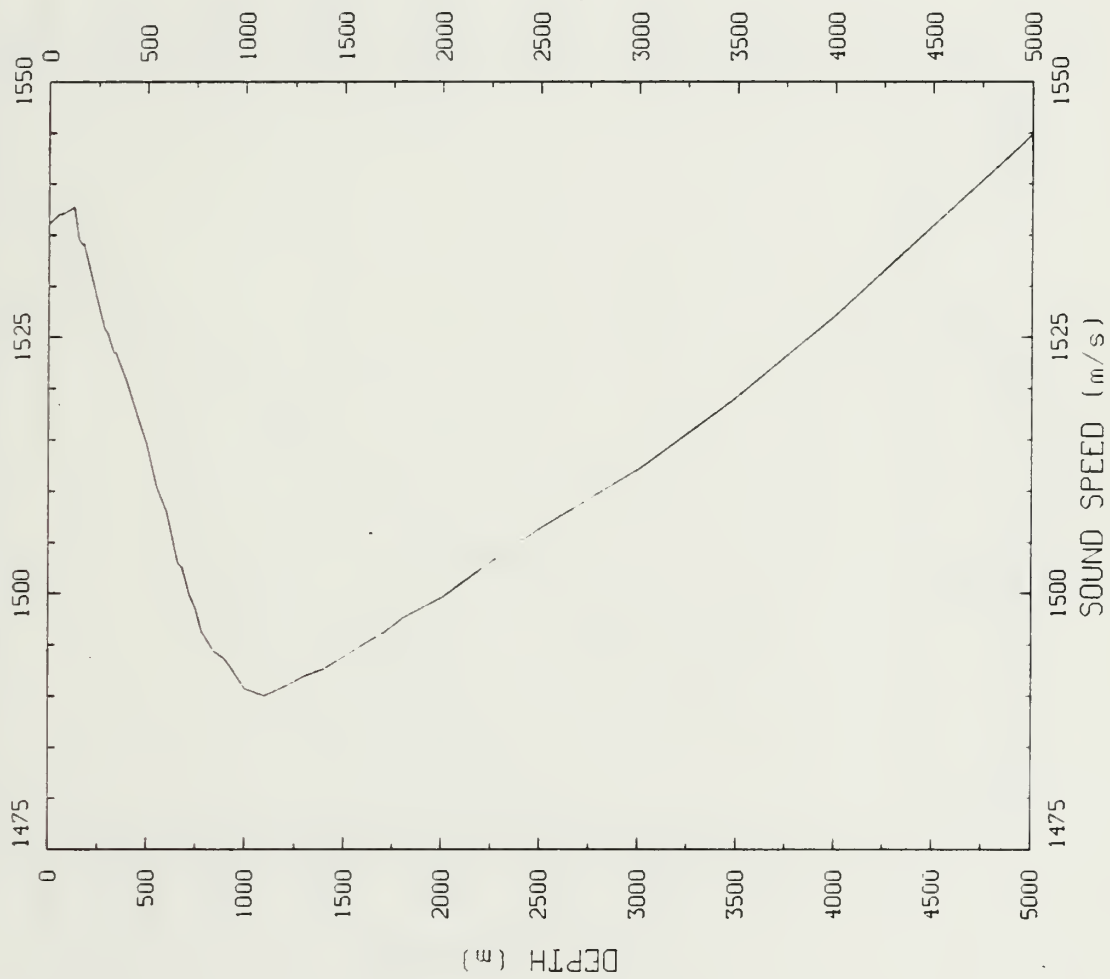
12TRACK1

PROFILE INTERPOLATED AT RANGE = 73.783



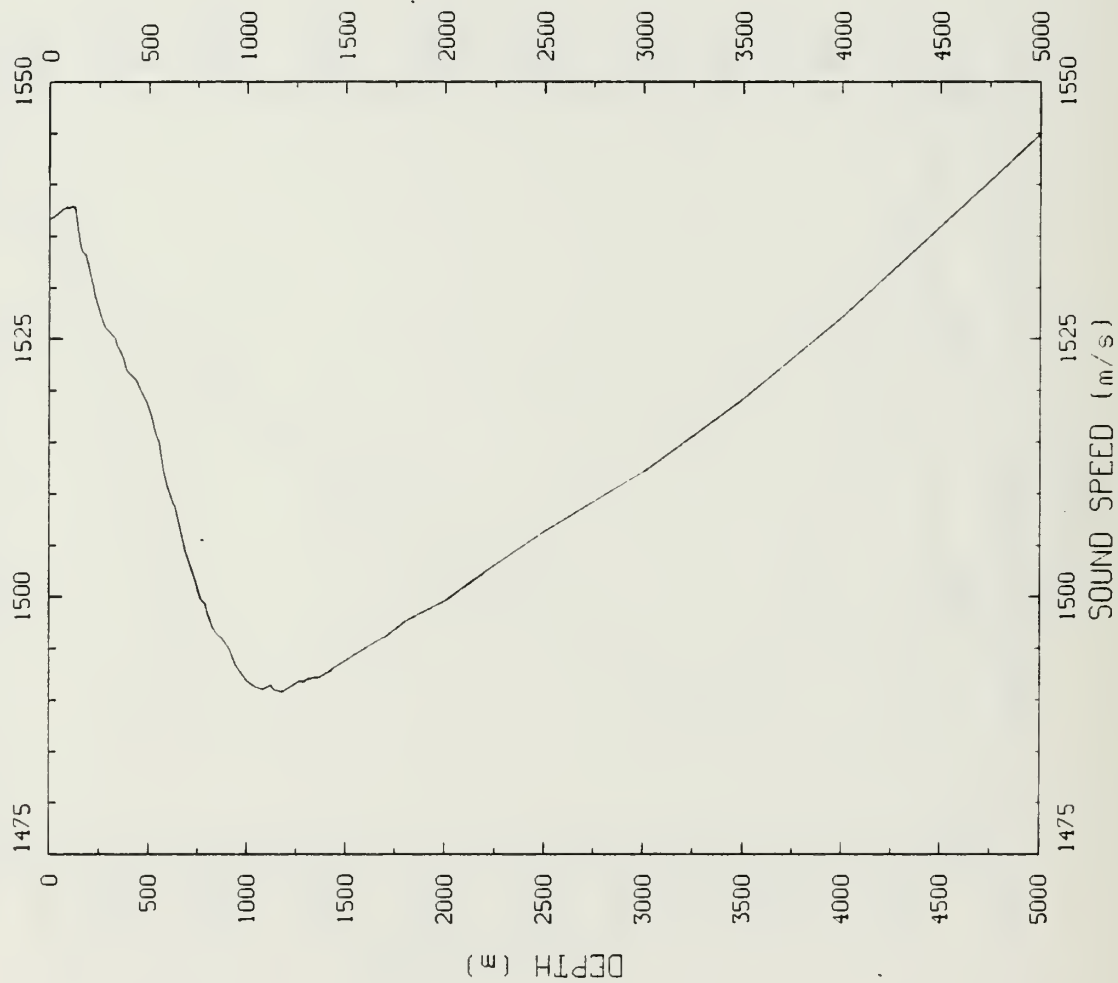
13TRACK1

PROFILE AT RANGE - 77.969



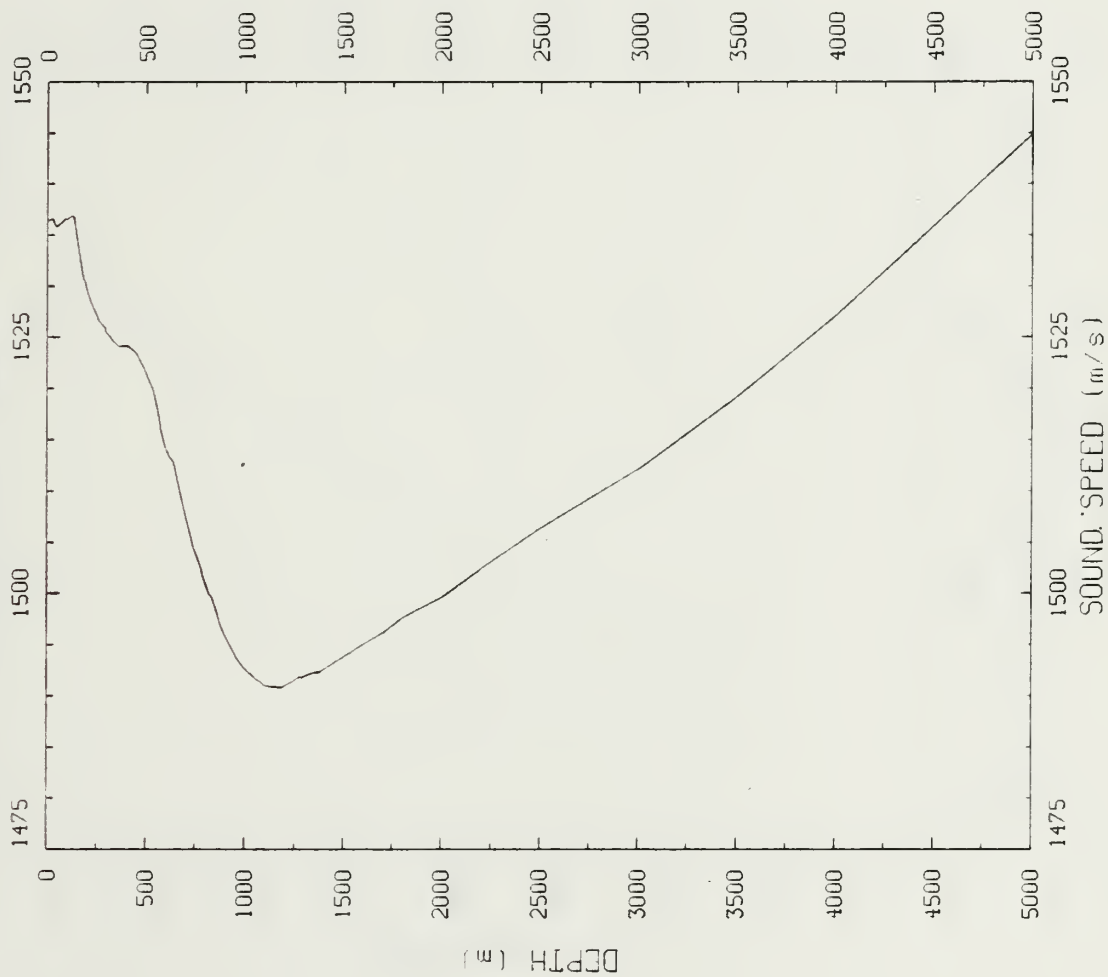
13TRACK1

PROFILE INTERPOLATED AT RANGE - 83.969



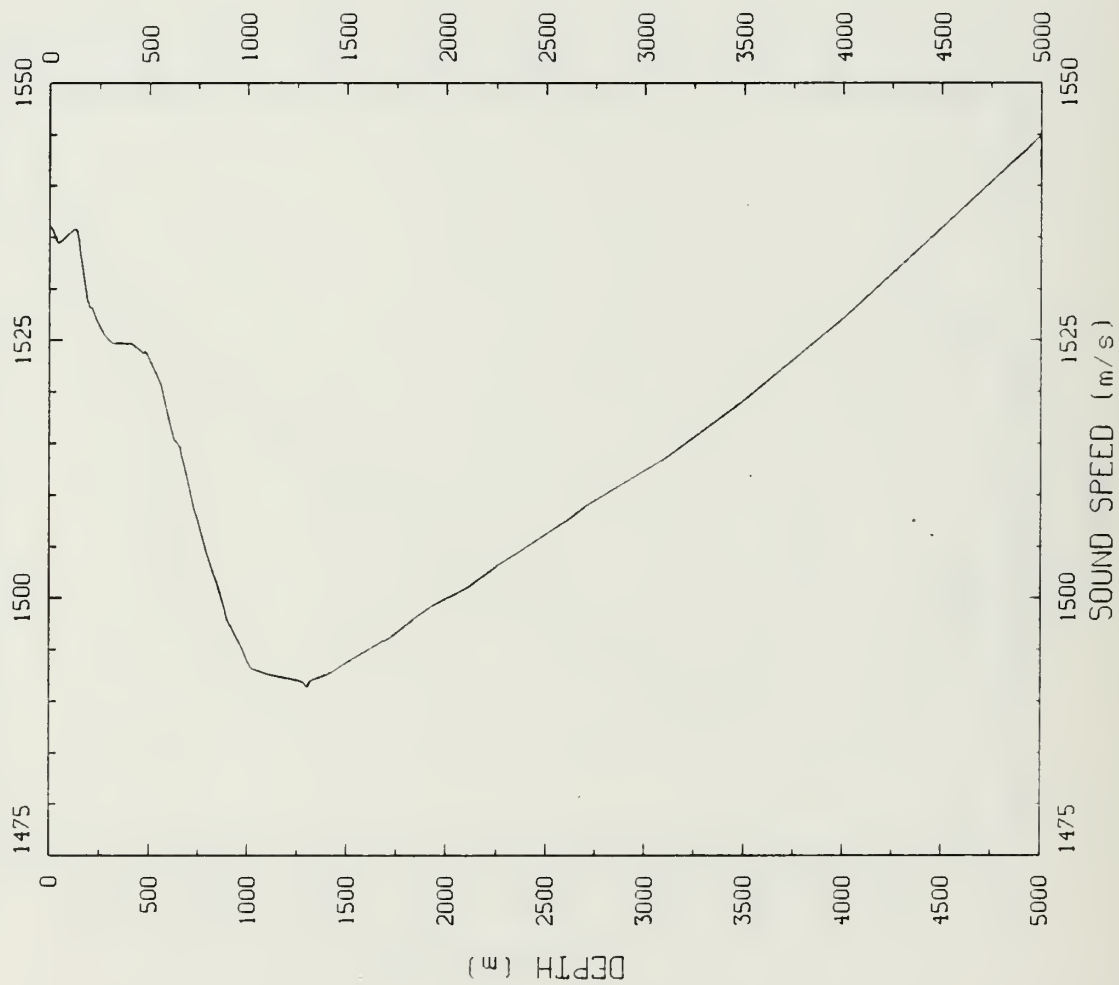
14TRACK1

PROFILE INTERPOLATED AT RANGE - 93.970



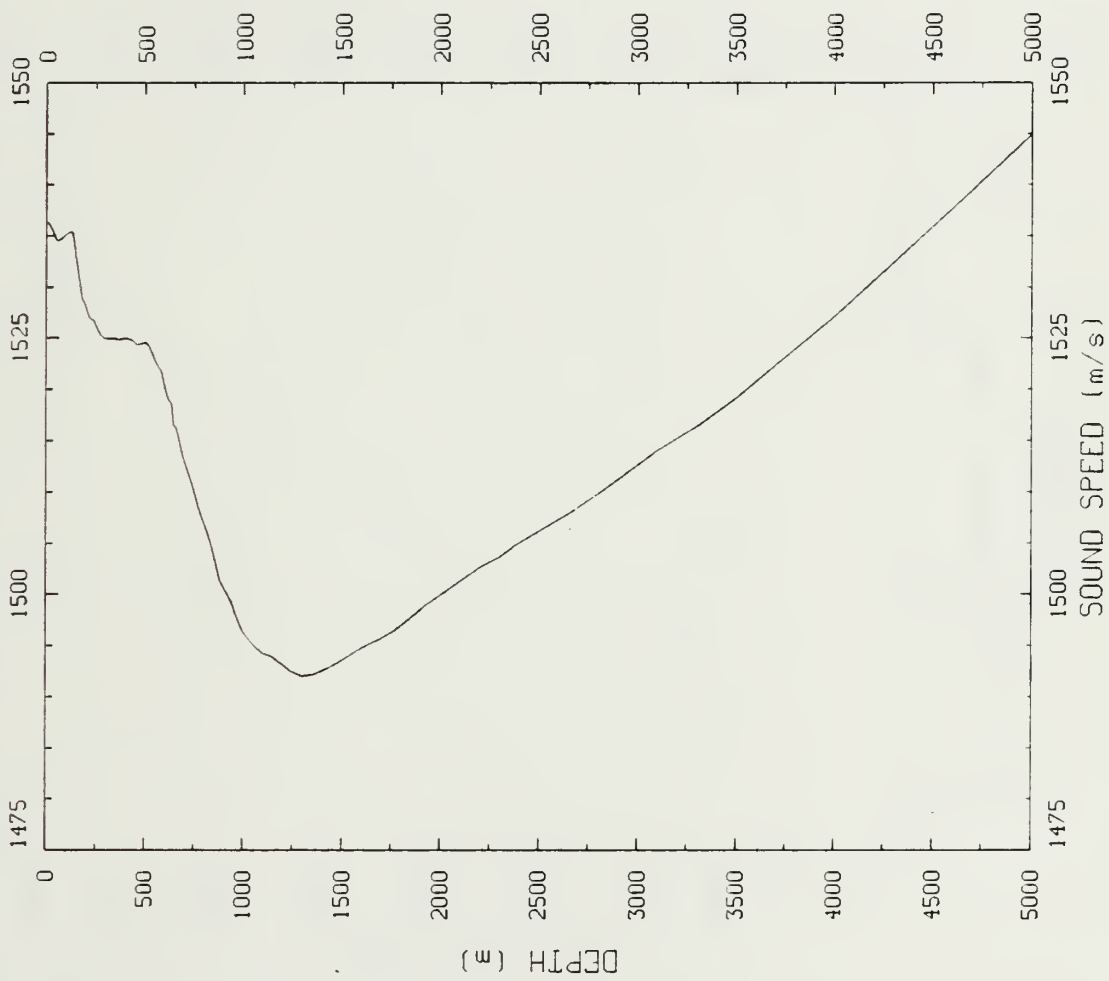
1STRACK1

PROFILE INTERPOLATED AT RANGE = 100.526



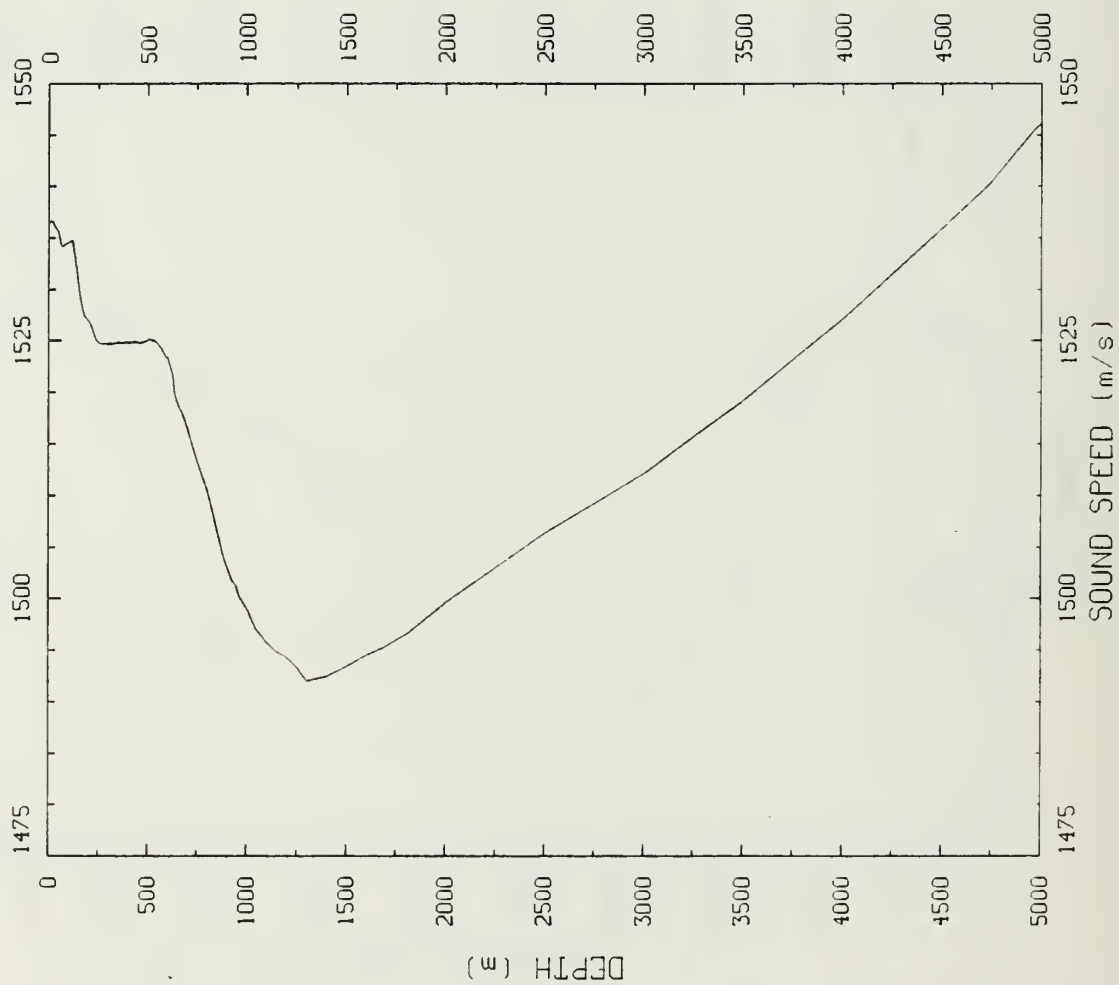
15TRACK1

PROFILE INTERPOLATED AT RANGE - 104.526



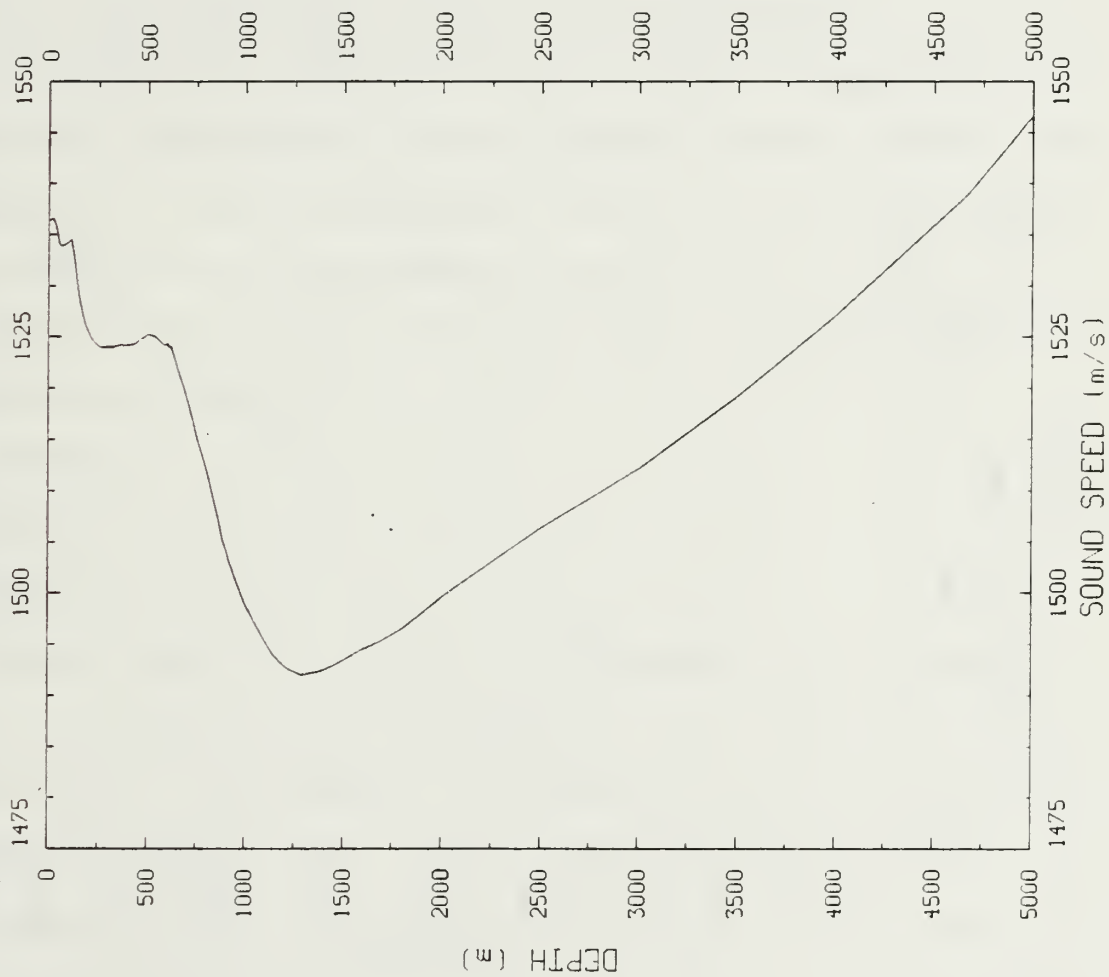
16TRACK1

PROFILE INTERPOLATED AT RANGE = 112.712



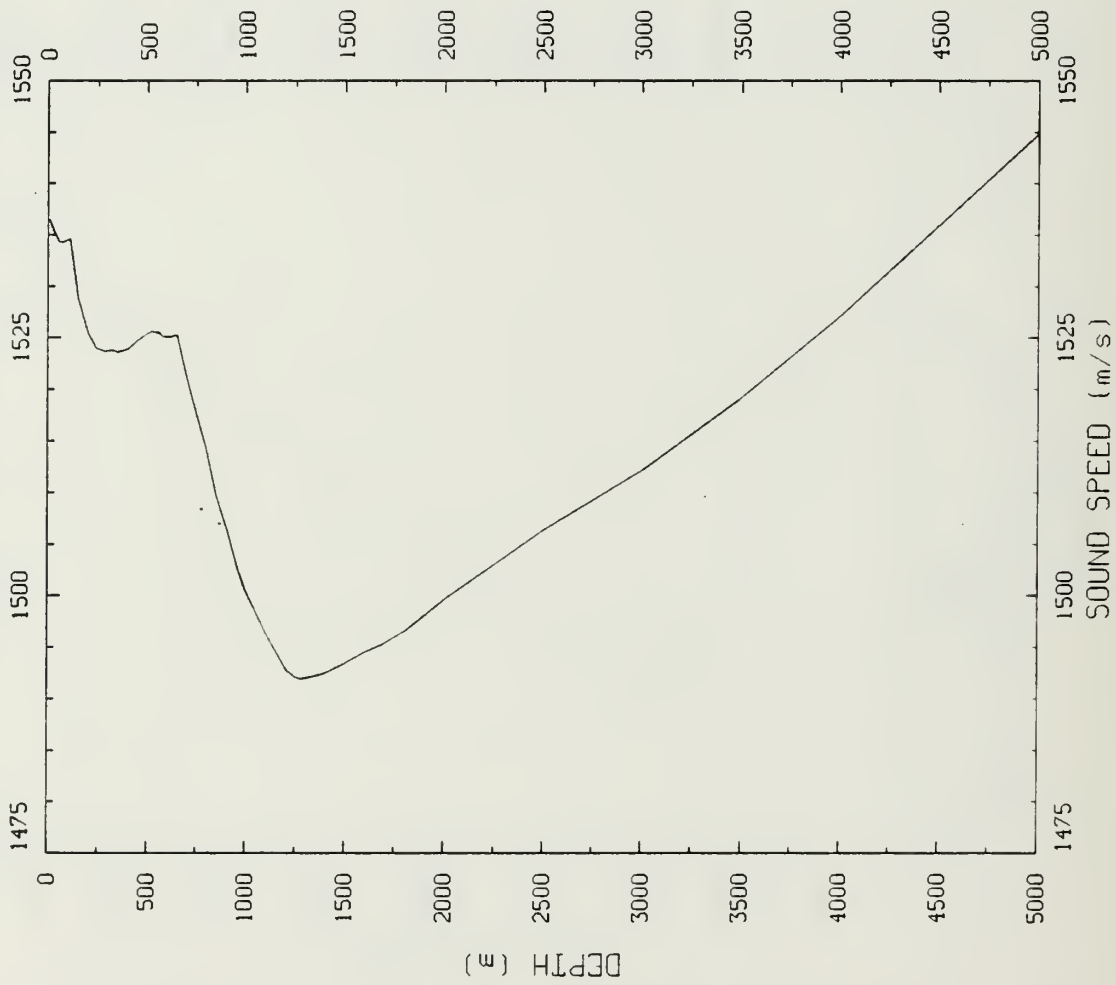
17TRACK1

PROFILE INTERPOLATED AT RANGE - 121.416



18TRACK1

PROFILE AT RANGE - 128.158



APPENDIX D

TL DIFFERENCE AND GRAYSCALE PLOTTING METHODS

Because an IFDPE output file occupies a tremendous amount of computer storage space, the output file is converted to a binary file. This reduces the space needed in the computer to store the information but it is unreadable in this form as far as the user is concerned. Therefore, the output binary file is processed to create grayscale and TL difference plots which are more readily usable than a binary file.

The programs used to generate grayscale and TL difference plots are:

- 1) PREGRAY
- 2) TLDIF
- 3) GRAYTL

PREGRAY carries out the preprocessing required to create a grayscale/TL difference plot from an IFDPE output file. The complex pressures calculated at user specified ranges and depths are averaged over an incremental range and depth to fit the restrictions of plotting grayscale/TL difference (only a 300 X 400 "matrix" of points is allowed). Those averaged values are then converted to transmission loss values and placed in another file to be called up when needed by the next program in creating these graphs.

TLDIF is different from PREGRAY in that it determines the difference in transmission loss values between two different IFDPE output files. If both TL values being differenced are greater than 105 dB, the difference is set to a very small number, since it would not be very significant.

Both PREGRAY and TLDIF supply the necessary axes in range and depth for grayscale/TL difference plotting as well as the bathymetry curves (from the IFDPE input files which includes the bathymetric profile at each SSP along the track) for grayscale/TL difference plotting by using calls to a DISPLA library.

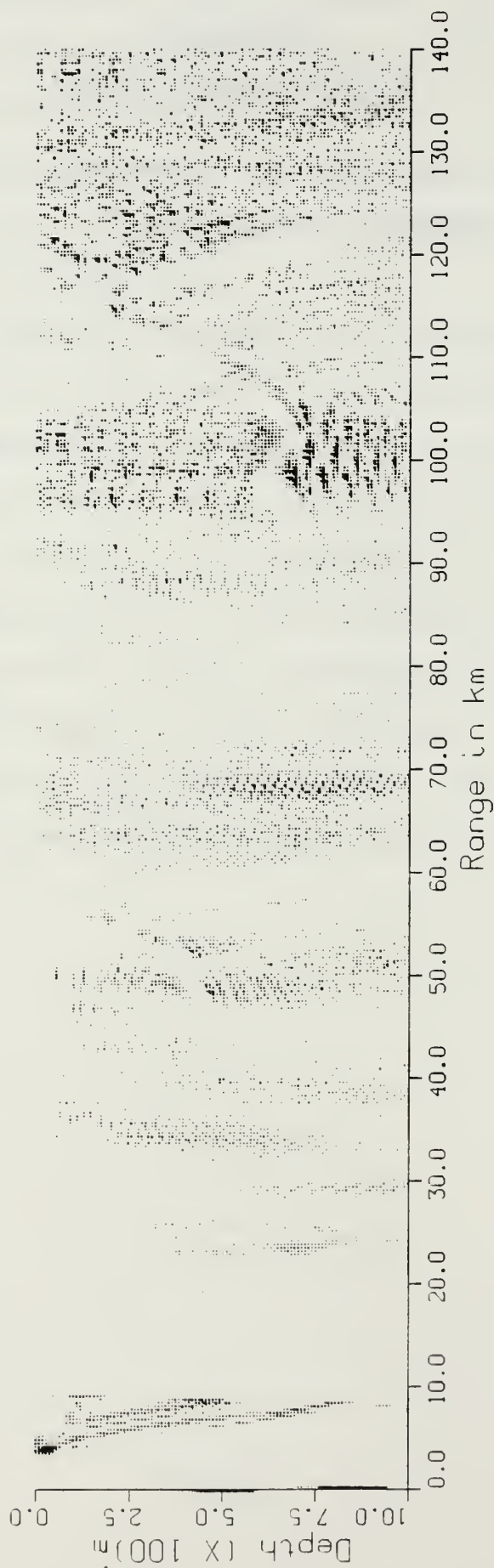
GRAYTL uses the TL values calculated from PREGRAY or TLDIF and calculates a level of gray to represent each of those values. The user inputs a min and max TL value and the grayscale plot graphs only that range of values.

APPENDIX E

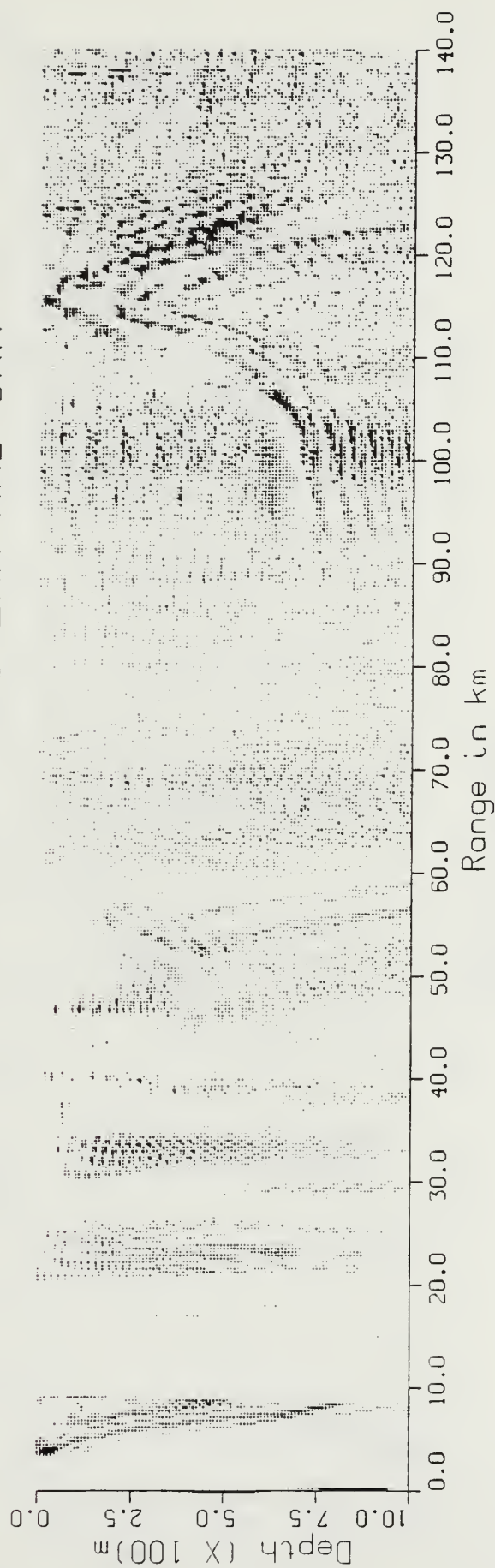
TL DIFFERENCE GRAPHS

Enclosed are the TL difference graphs used for qualitative analysis in this report.

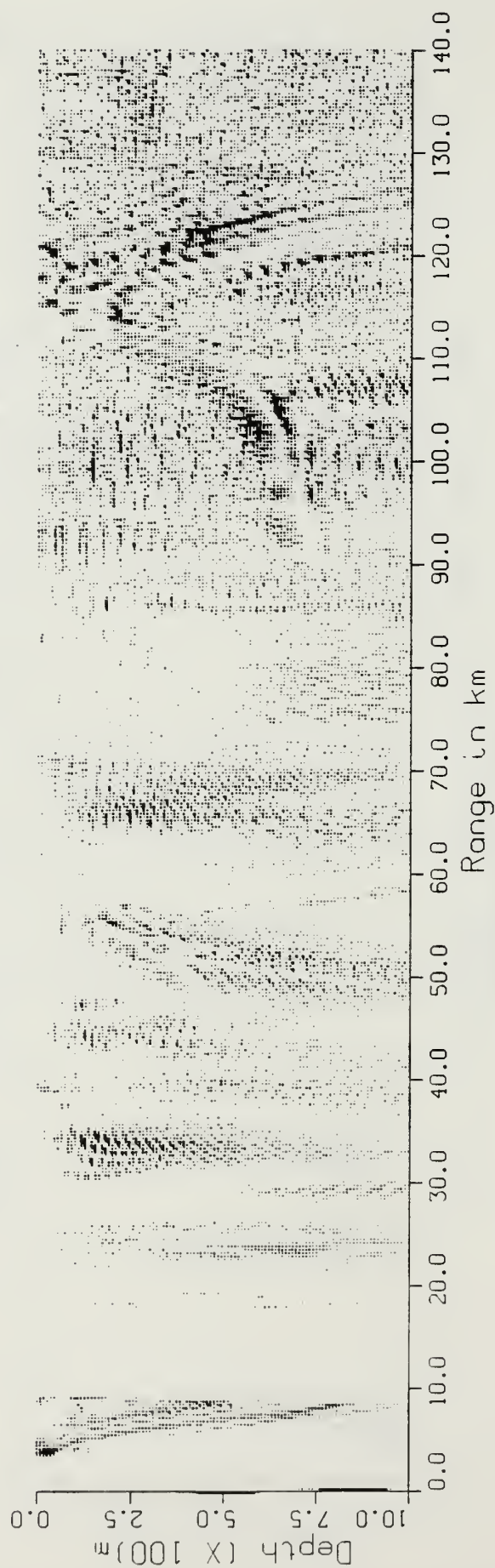
SOURCE DEPTH = 100M
GULF STREAM DIFF RES 2KM AND 6KM



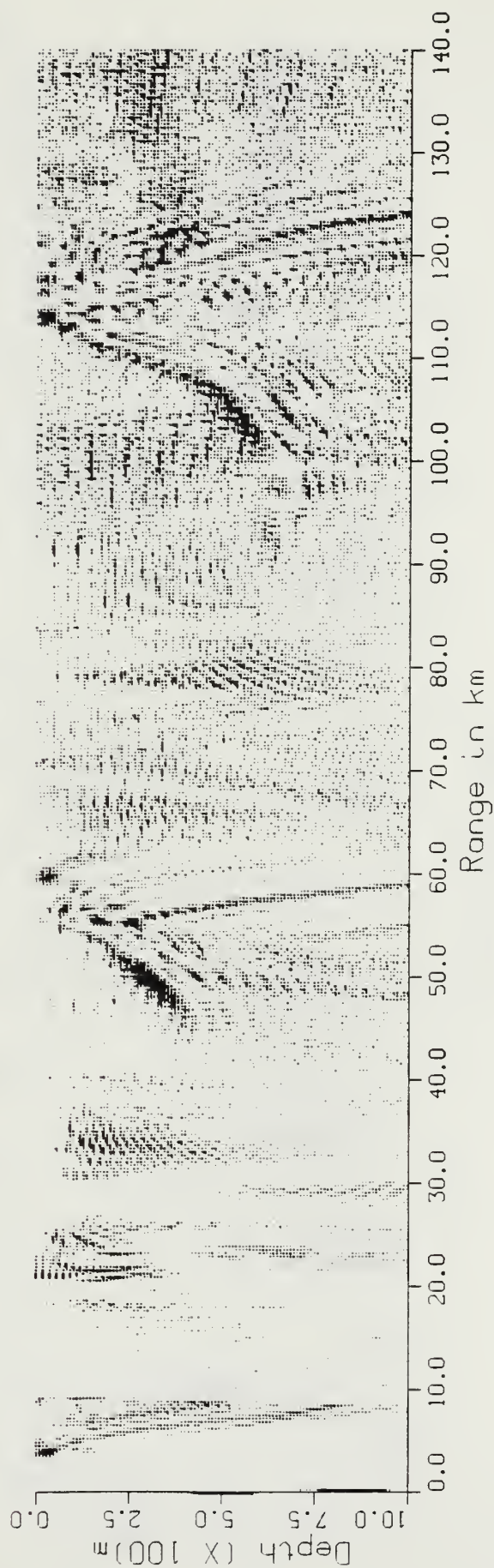
SOURCE DEPTH = 100m
GULF STREAM DIFF RES 2KM AND 8KM



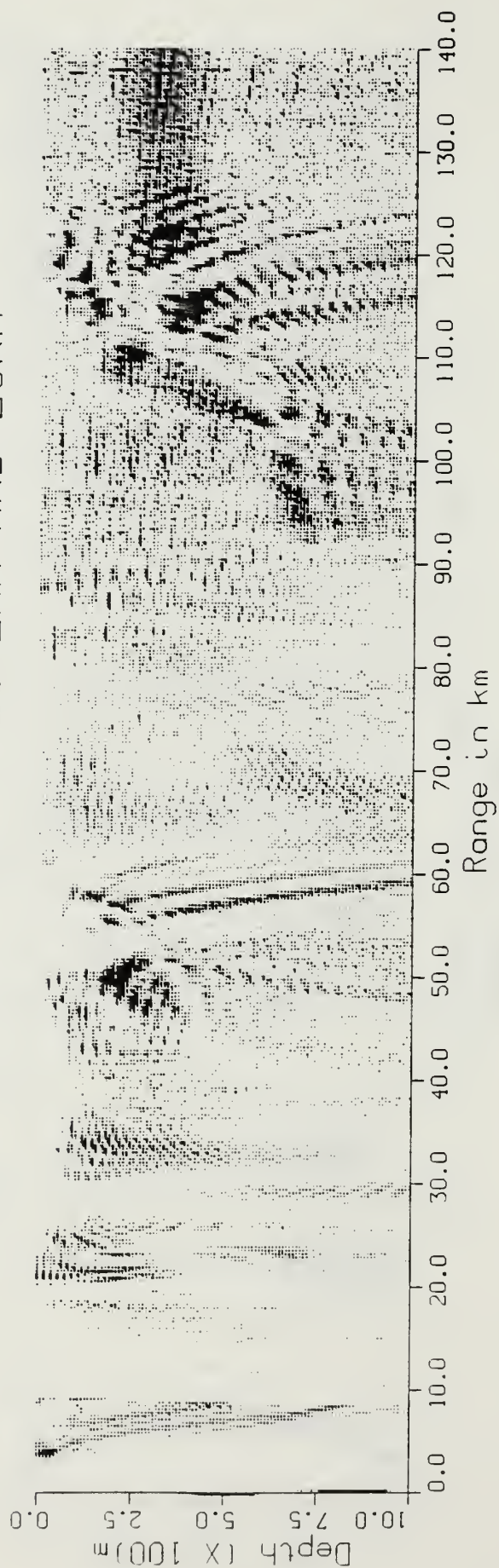
SOURCE DEPTH = 100M
GULF STREAM DIFF RES 2KM AND 10KM



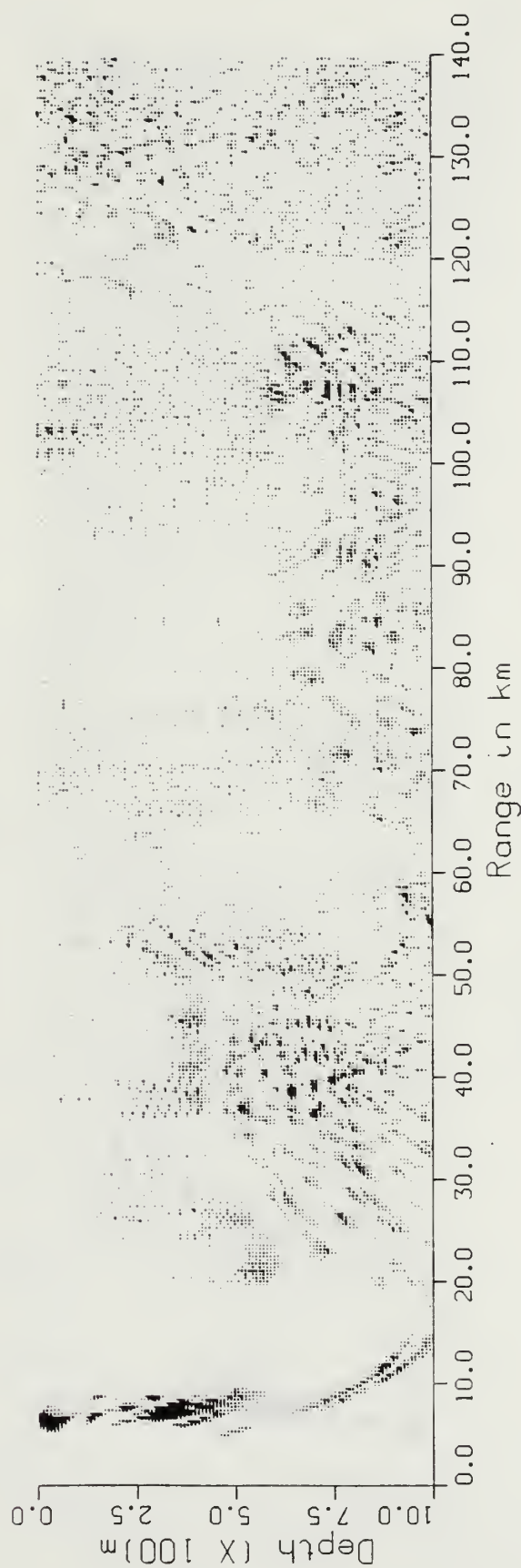
SOURCE DEPTH = 100m
GULF STREAM DIFF RES 2KM AND 20KM



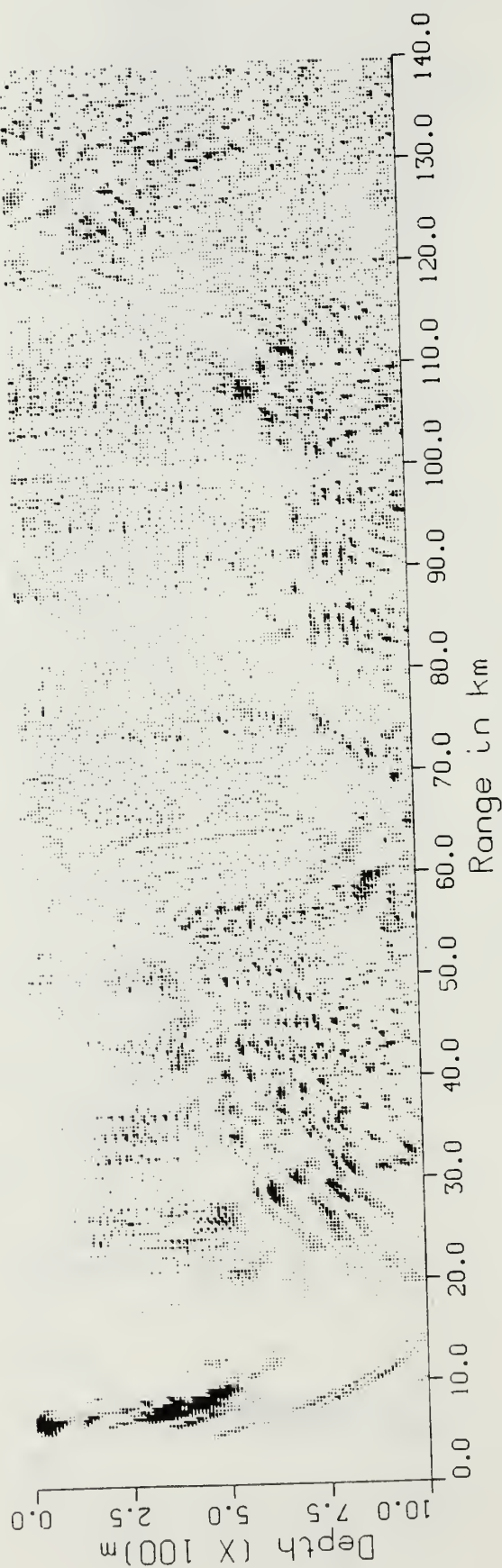
SOURCE DEPTH = 100m
GULF STREAM DIFF RES 2KM AND 25KM



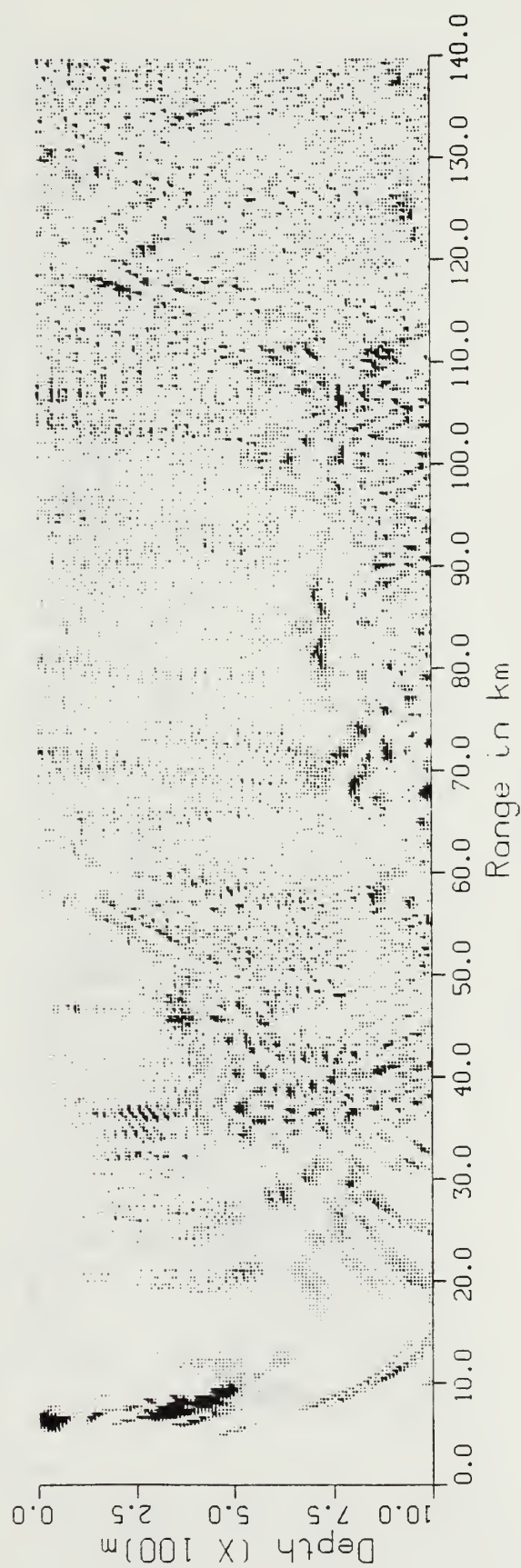
GULF STREAM DIFF RES 2KM AND 6KM
SOURCE DEPTH = 500 M



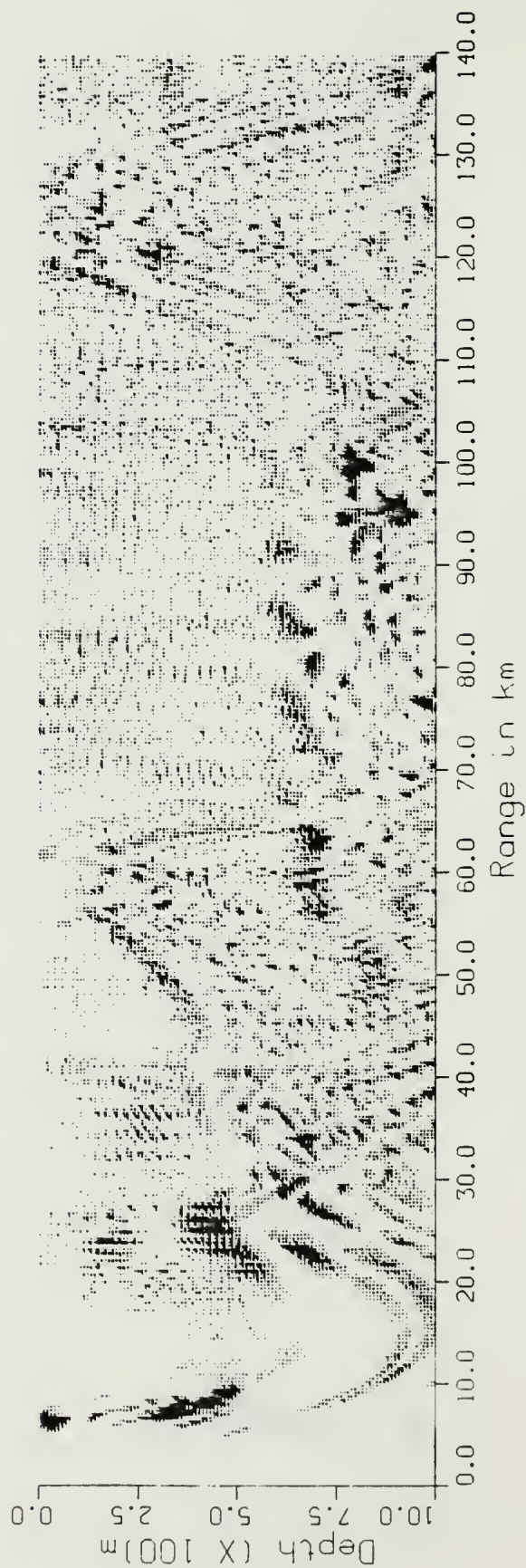
GULF STREAM DIFF RES 2KM AND 8KM
SOURCE DEPTH = 500 M



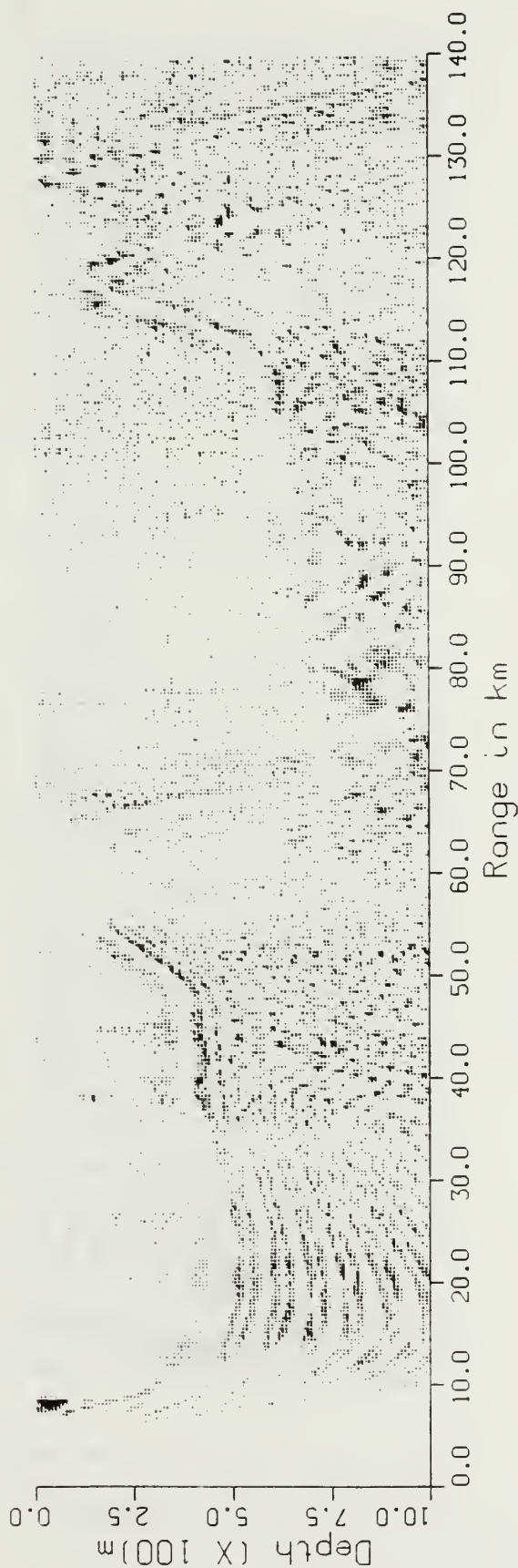
GULF STREAM DIFF RES 2KM AND 10KM
SOURCE DEPTH = 500 M



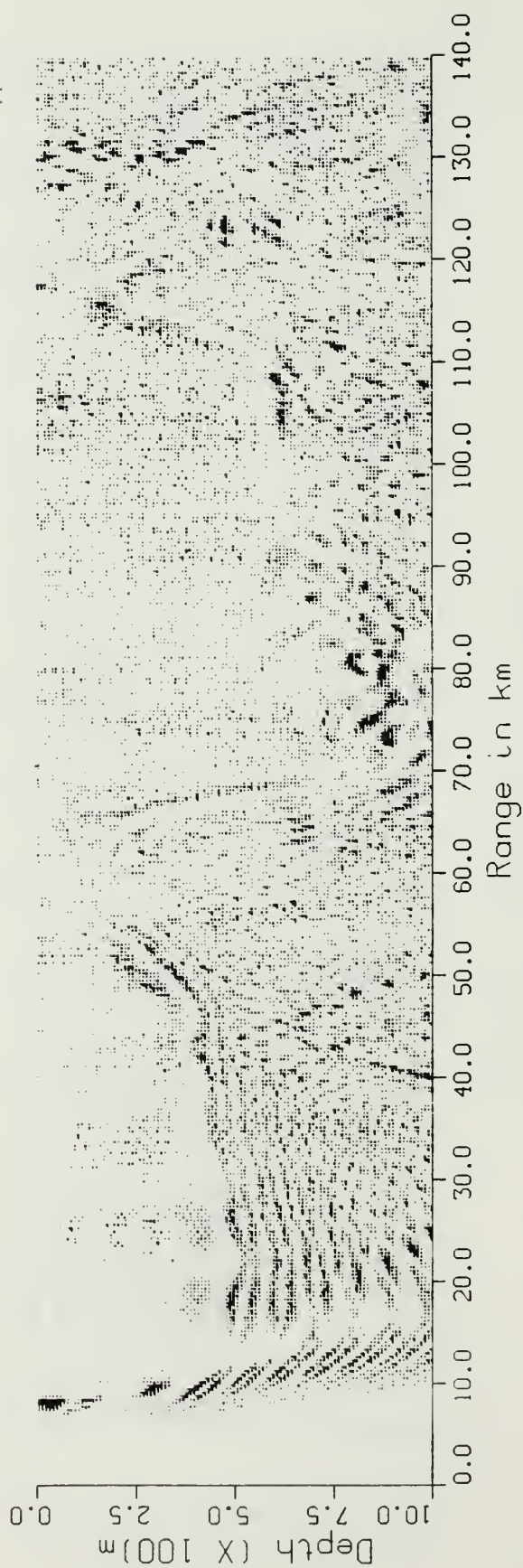
GULF STREAM DIFF RES 2KM AND 20KM
SOURCE DEPTH = 500 M



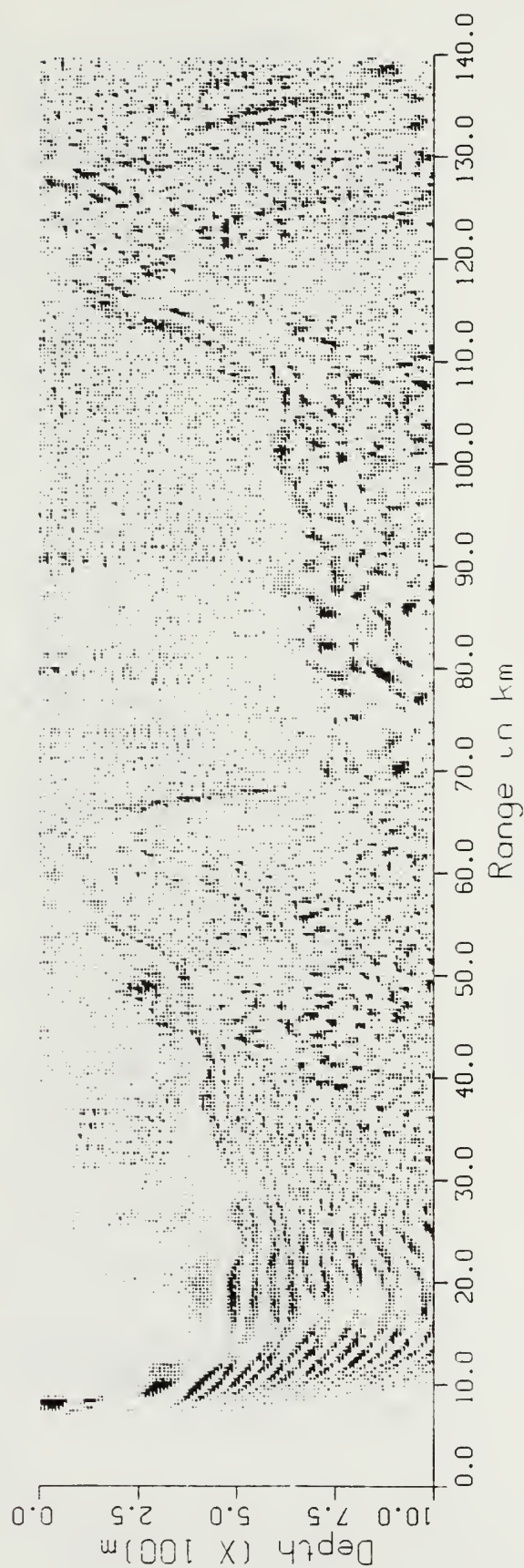
GULF STREAM DIFF RES 2KM AND 6KM
SOURCE DEPTH = 1000 M



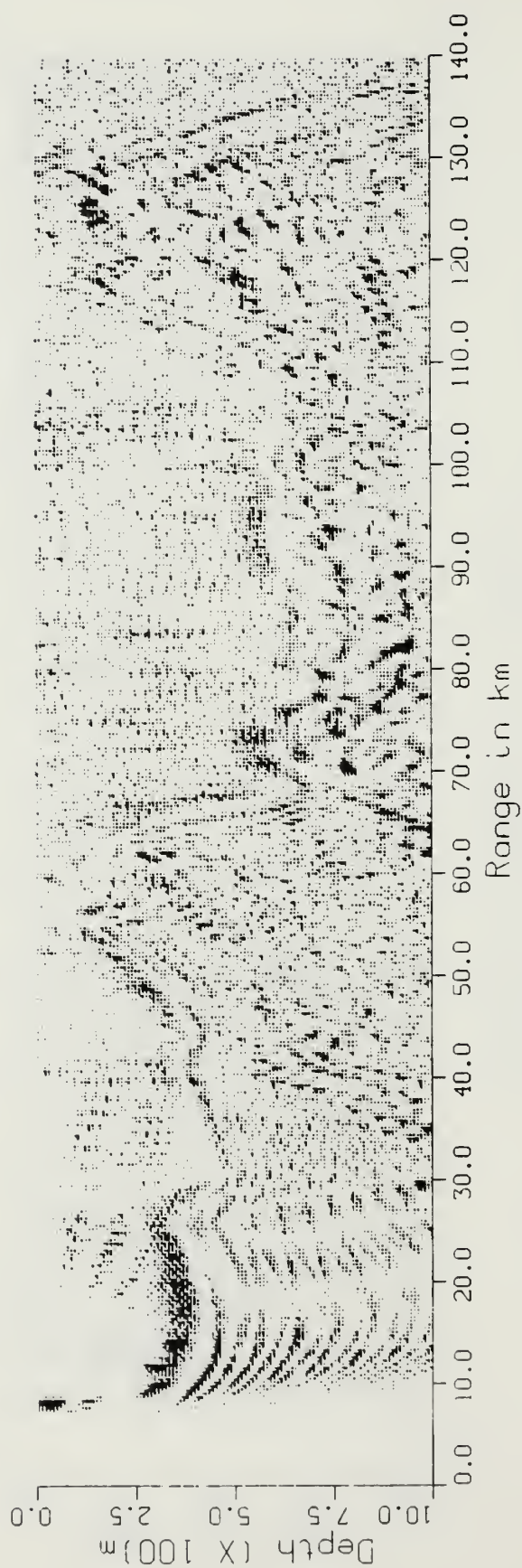
GULF STREAM DIFF RES 2KM AND 8KM
SOURCE DEPTH = 1000 M



GULF STREAM DIFF RES 2KM AND 10KM
SOURCE DEPTH = 1000 M



GULF STREAM DIFF RES 2KM AND 20KM
SOURCE DEPTH = 1000 M



APPENDIX F

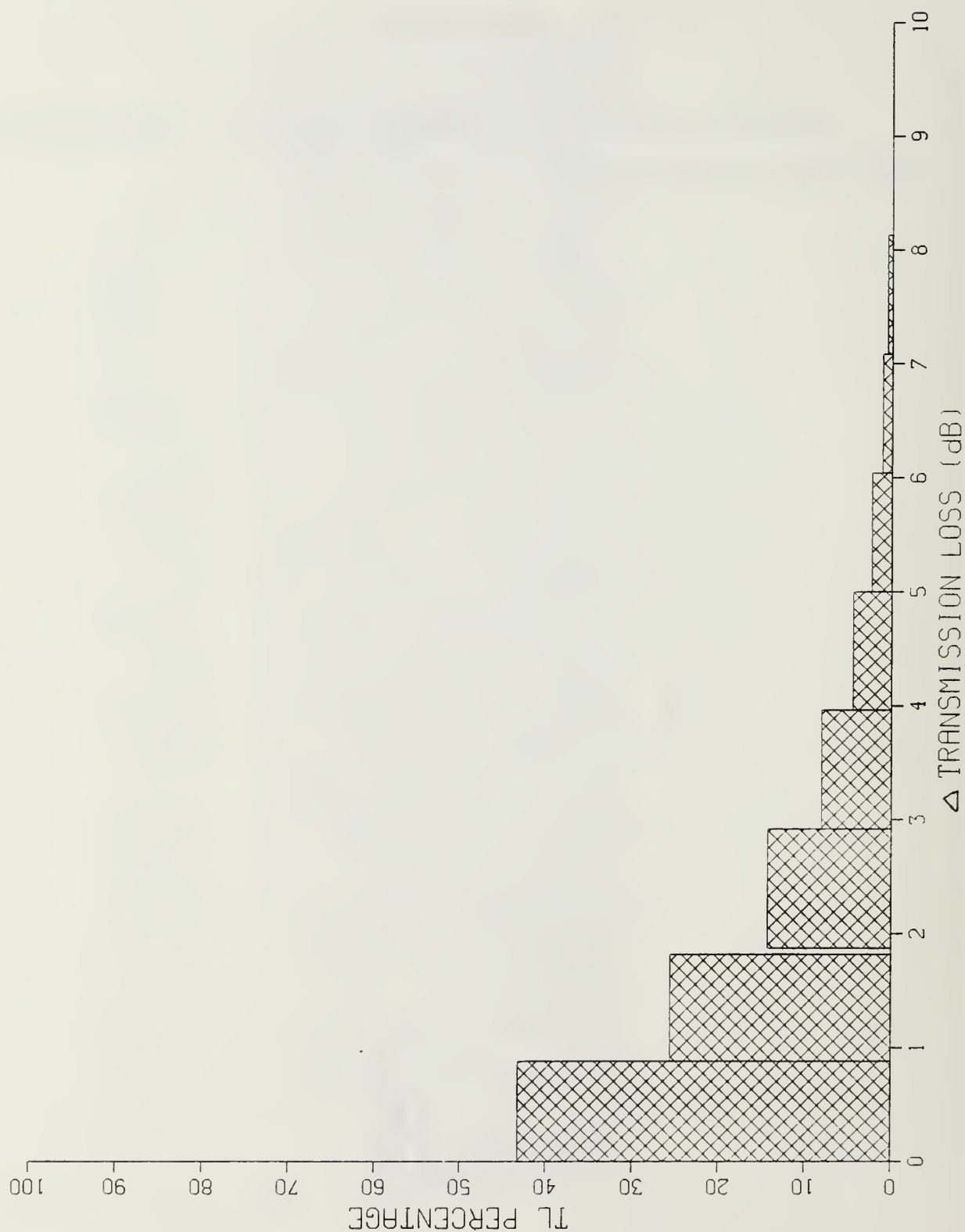
HISTOGRAMS

Enclosed are the histograms used for quantitative analysis in this study.

GULF STREAM DIFF RES 2KM AND 6KM

SOURCE DEPTH = 100M

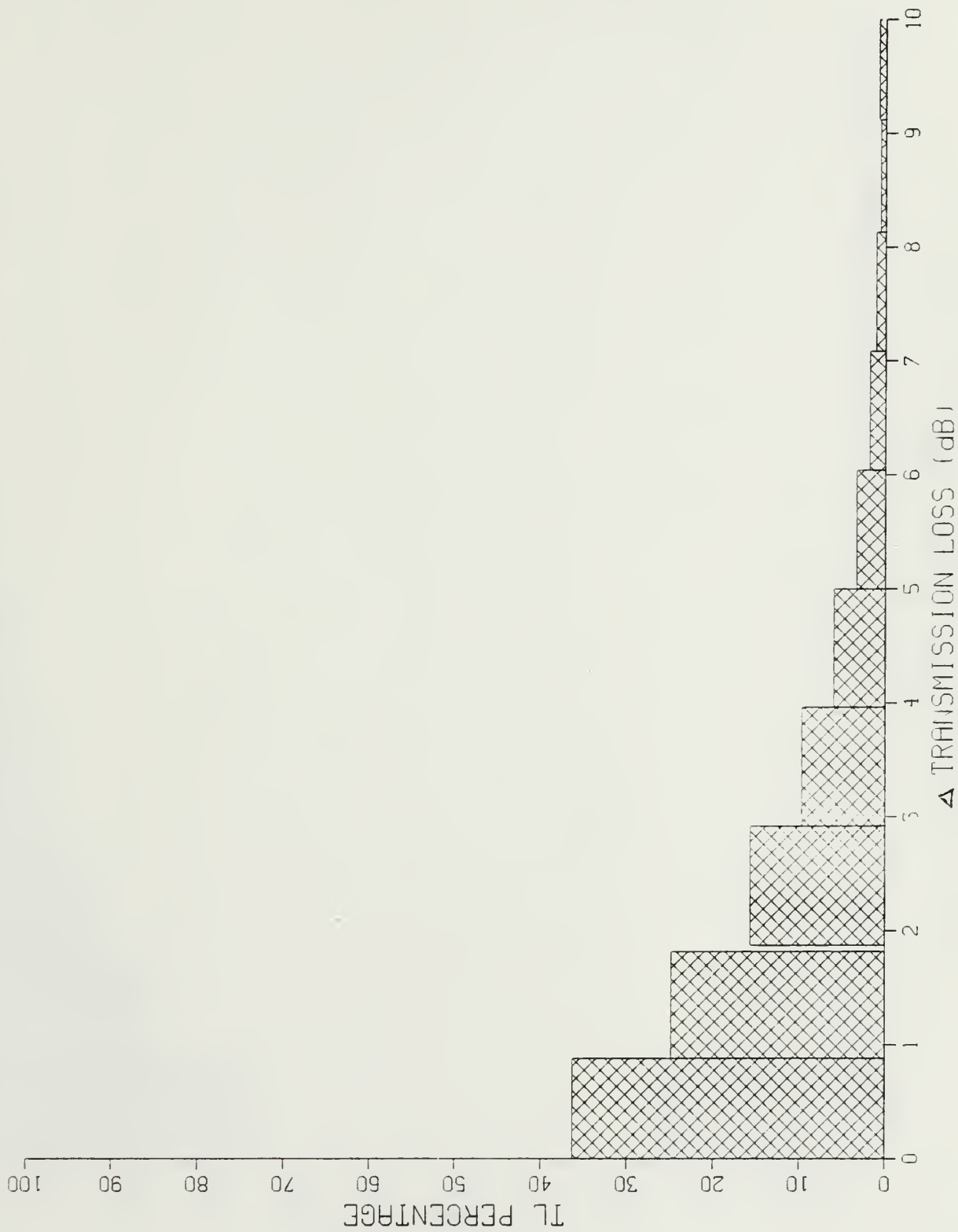
CALCULATED STATISTICS ON TL VALUES ABOVE 1000M



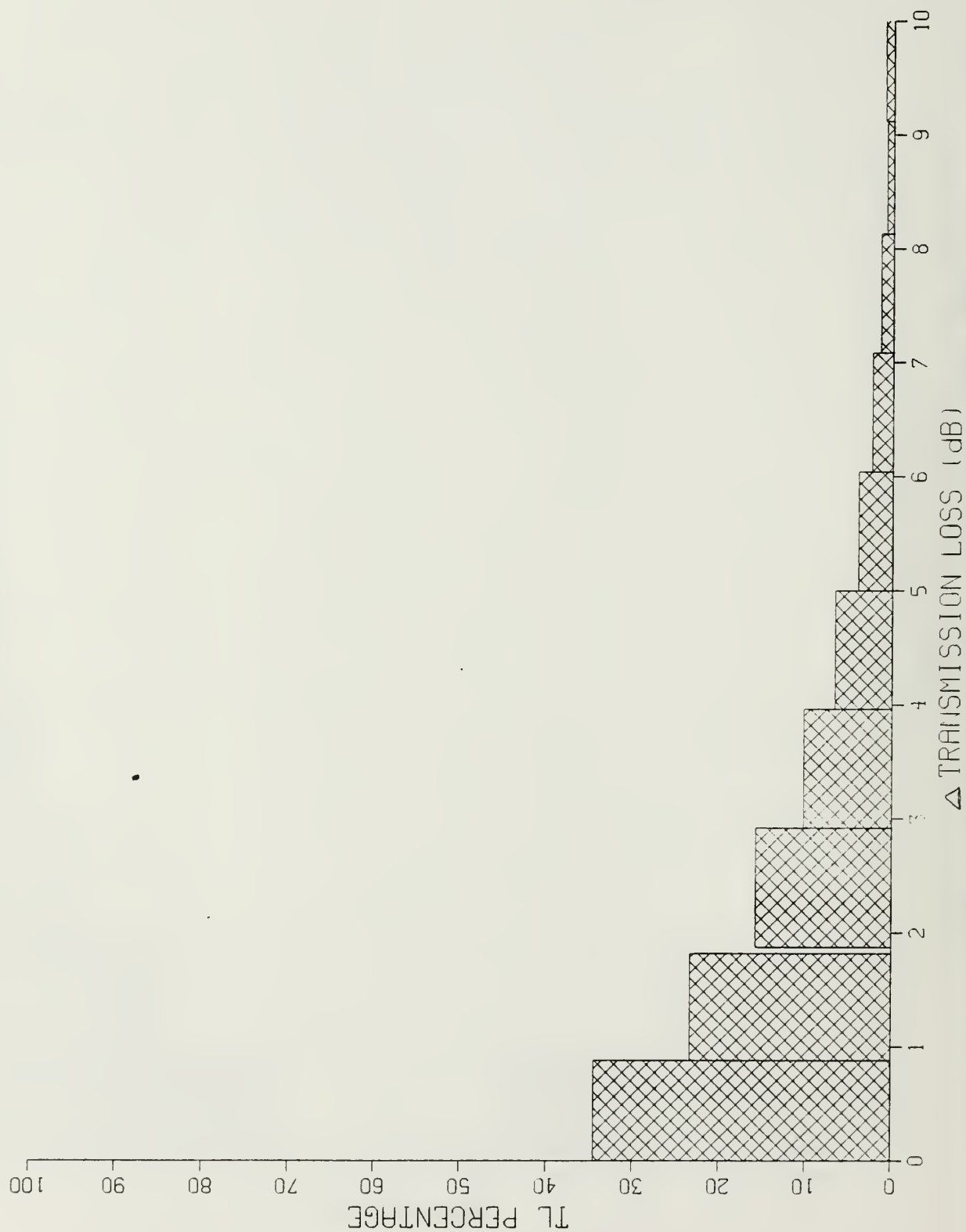
GULF STREAM DIFF RES 2KM AND 8KM

SOURCE DEPTH = 100M

CALCULATED STATISTICS ON TL VALUES ABOVE 1000M



GULF STREAM DIFF RES 2KM AND 10KM
 SOURCE DEPTH = 100M
 CALCULATED STATISTICS ON TL VALUES ABOVE 1000M



GULF STREAM DIFF RES 2KM AND 25KM

SOURCE DEPTH = 100M

CALCULATED STATISTICS ON TL VALUES ABOVE 1000M



GULF STREAM DIFF RES 2KM AND 30KM SOURCE DEPTH = 100M

CALCULATED STATISTICS ON TL VALUES ABOVE 1000M



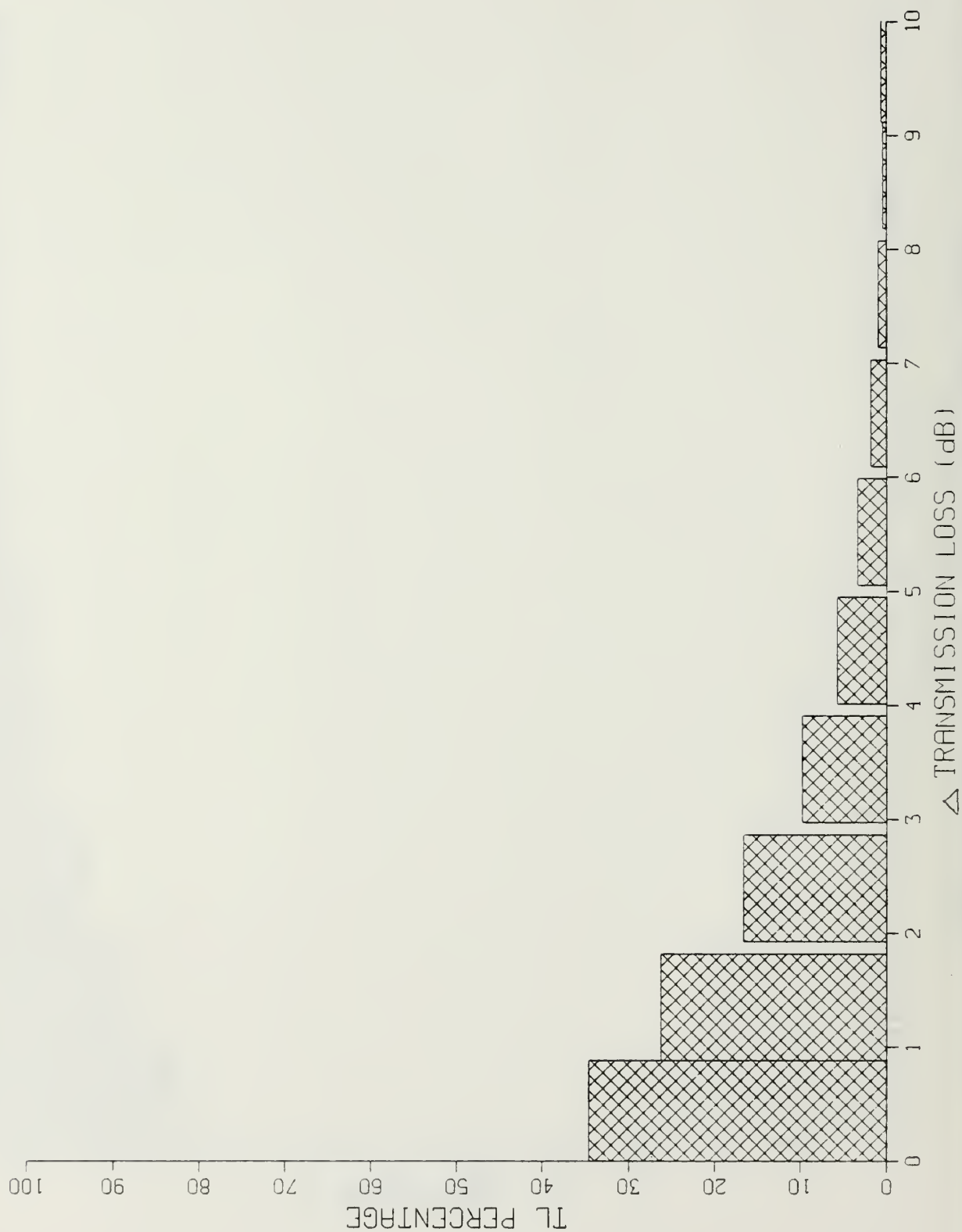
GULF STREAM DIFF RES 2KM AND 60KM

SOURCE DEPTH = 100M

CALCULATED STATISTICS ON TL VALUES ABOVE 1000M



GULF STREAM DIFF RES 2KM AND 6KM
 SOURCE DEPTH = 500 M
 CALCULATED STATISTICS ON TL VALUES ABOVE 1000M



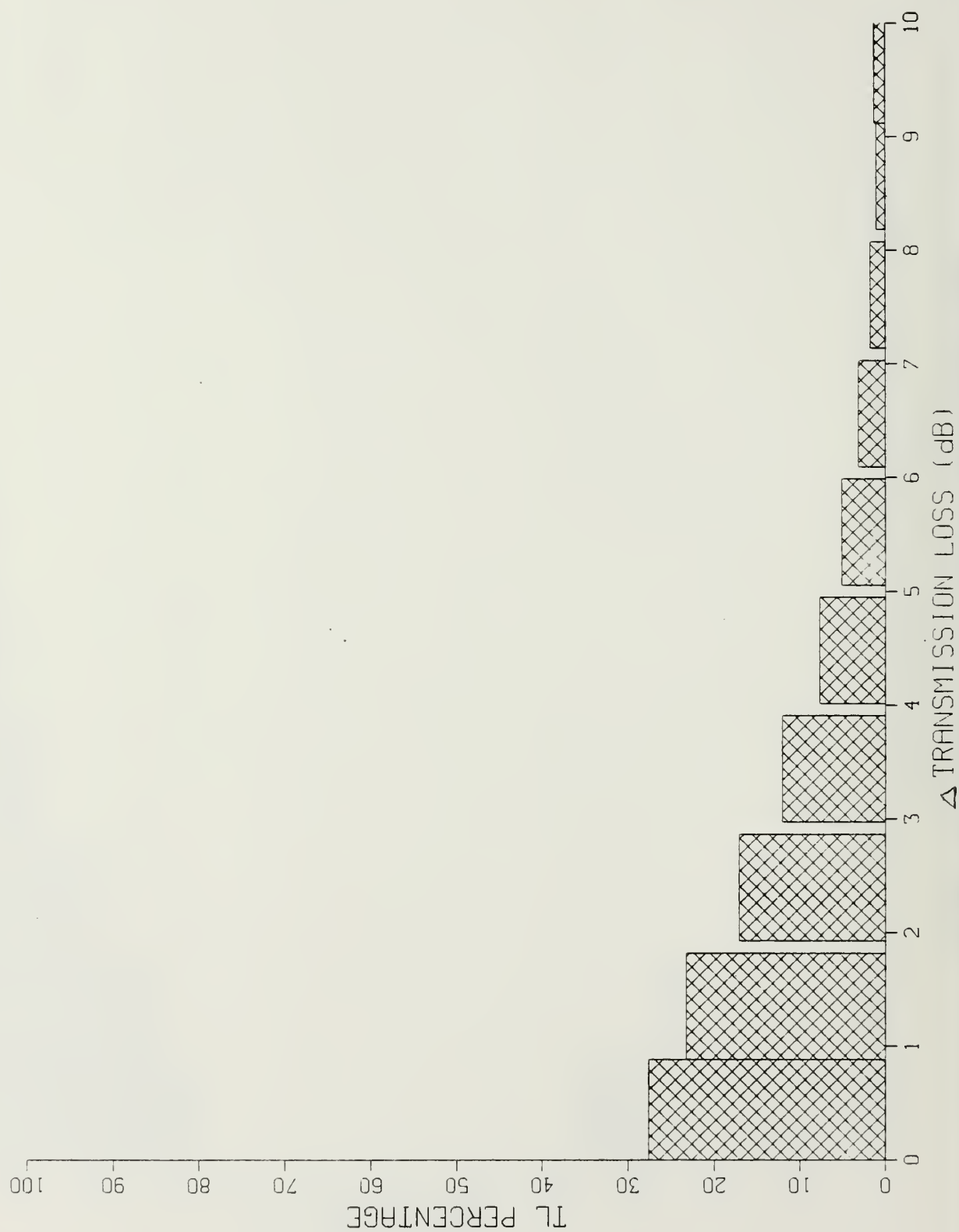
GULF STREAM DIFF RES 2KM AND 8KM

SOURCE DEPTH = 500 M

CALCULATED STATISTICS ON TL VALUES ABOVE 1000M



GULF STREAM DIFF RES 2KM AND 10KM
 SOURCE DEPTH = 500 M
 CALCULATED STATISTICS ON TL VALUES ABOVE 1000M



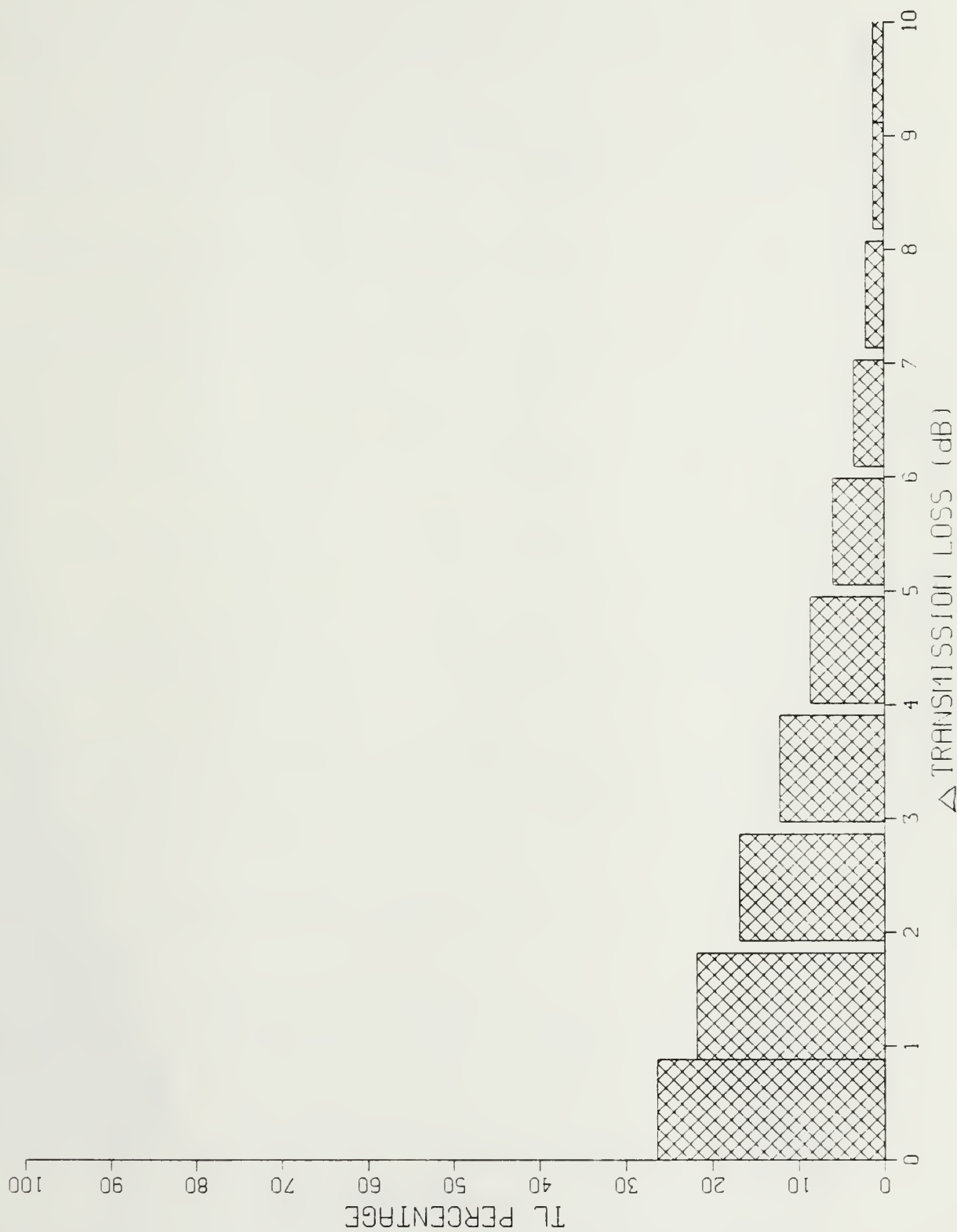
GULF STREAM DIFF RES 2KM AND 20KM
 SOURCE DEPTH = 500 M
 CALCULATED STATISTICS ON TL VALUES ABOVE 1000M



GULF STREAM DIFF RES 2KM AND 6KM
 SOURCE DEPTH = 1000 M
 CALCULATED STATISTICS ON TL VALUES ABOVE 1000M



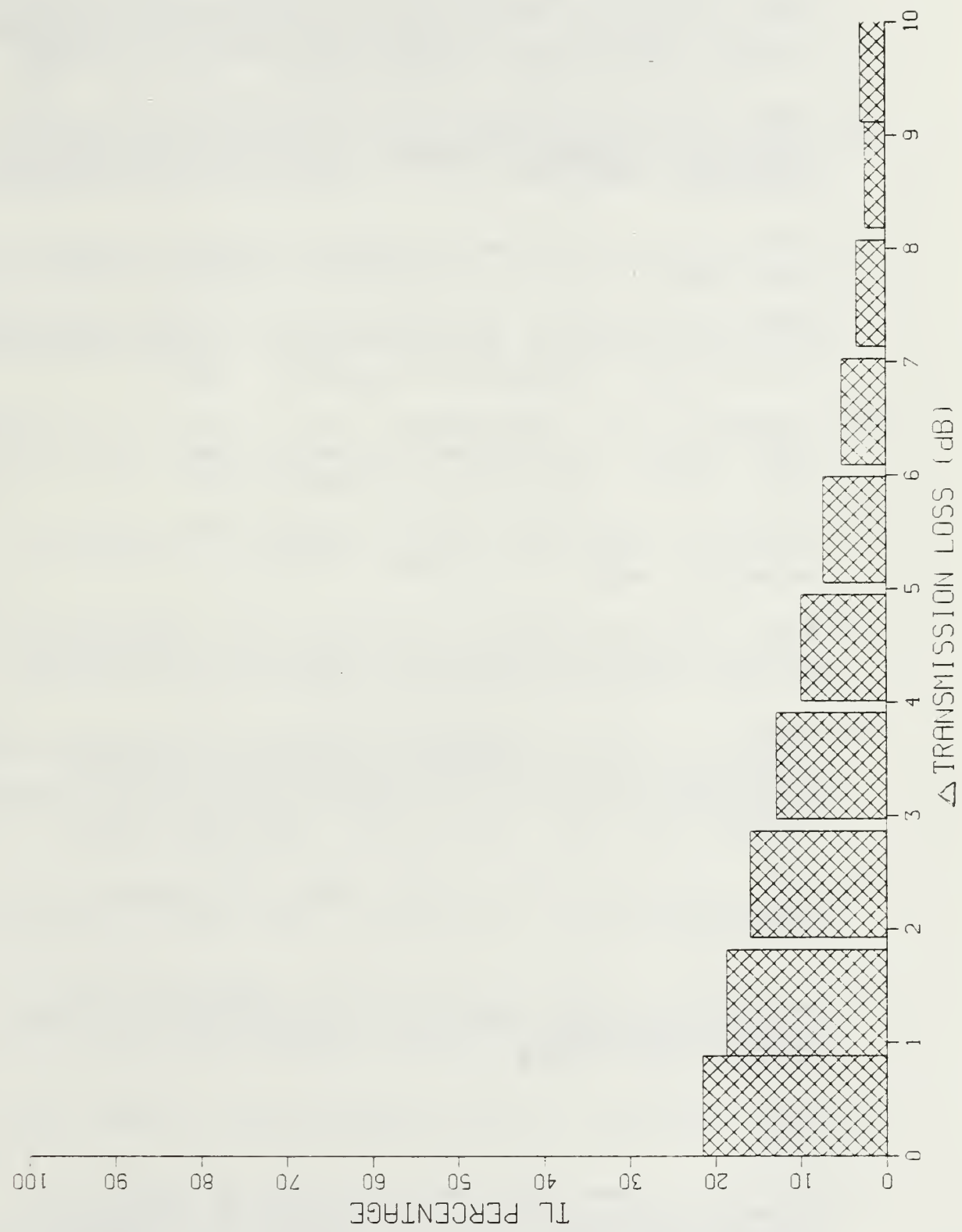
GULF STREAM DIFF RES 2KM AND 8KM
 SOURCE DEPTH = 1000 M
 CALCULATED STATISTICS ON TL VALUES ABOVE 1000M



GULF STREAM DIFF RES 2KM AND 10KM
 SOURCE DEPTH = 1000 M
 CALCULATED STATISTICS ON TL VALUES ABOVE 1000M



GULF STREAM DIFF RES 2KM AND 20KM
 SOURCE DEPTH = 1000 M
 CALCULATED STATISTICS ON TL VALUES ABOVE 1000M



LIST OF REFERENCES

1. NUSC Technical Memo 811054, Tactical Implications for Mobile Sensors Derived from the Gulf Stream Frontal Experiment (Project GSFE), 19 June 1981.
2. NUSC Technical Report 6659, IFD--An Implicit Finite-Difference Computer Model for Solving the Parabolic Equation, by D. Lee and G. Botseas, 27 May 1982.
3. NORDA Technical Note 293, NORDA Acoustic Models and Data Bases, by Edward Estalote, October 1984.
4. NORDA Report 115, An Evaluation of Range Dependent Ray Theory Models, by R.W. McGirr, D.B. King, J.A. Davis, and J. Campbell, September 1985.
5. Siegmann, W.L., Kriegsmann, G.A., Lee, D., "A Wide-Angle Three Dimensional Parabolic Wave Equation," JASA, 78(2), pp. 659-672, August 1985.
6. Tappert, F.D., Lee, D., "A Range Refraction Parabolic Equation," JASA, 76(6), pp. 1797-1804, December 1984.
7. NPS Technical Report 61-83-002, An Introduction to the Parabolic Equation for Acoustic Propagation, by A.B. Coppins, November 1982.
8. Jaeger, L.E., A Computer Program for Solving the Parabolic Equation Using an Implicit Finite-Difference Solution Incorporating Exact Interface Conditions, M.S. Thesis, Naval Postgraduate School, Monterey, California, September 1983.
9. NUSC Technical Note 6905, IFD: Wide-Angle Capability, by G. Botseas, D. Lee, and K. Gilbert, 28 October 1983.
10. NUC (NUSC) Technical Note 1516, RAYWAVE II: A Propagation Loss Model for the Analysis of Complex Ocean Environments, by W.H. Watson and R.W. McGirr, April 1975.
11. Kerr, George, Private Communication, NORDA, May 1986.
12. Daubin Systems Corporation Technical Report No. 02-84, The Parabolic Equation as an On-Board Operational Model, by S.C. Daubin, L. Nghiem-Phu, and F.D. Tappert, 15 August 1984.

13. Daubin Systems Corporation Technical Report No. 02-86, On the Environmental Data Requirements to Support the Parabolic Equation as an Operational Acoustic Propagation Model, by S.C. Daubin, L. Nghiem-Phu, and F.D. Tappert, 14 February 1986.
14. The Johns Hopkins University Applied Physics Laboratory STD-N-077, A Cautionary Note on the Use of Range-Dependent Propagation Models in Under-water Acoustics, by R. F. Henrick, May 1982.

INITIAL DISTRIBUTION LIST

	No. Copies
1. Defense Technical Information Center Cameron Station Alexandria, Va. 22304-6145	2
2. Library, Code 0142 Naval Postgraduate School Monterey, Ca. 93943-5002	2
3. Dr. George Heburn Naval Oceanographic and Research Activity Code 323 Tactical Oceanography Program Bay St. Louis, Ms. 39529	10
4. Dr. David King Naval Oceanographic and Research Activity Code 223 Bay St. Louis, Ms. 39529	2
5. Dr. Alan Coppens Naval Postgraduate School Code 61Cz Monterey, Ca. 93943	1
6. Ding Lee Naval Underwater Systems Center Newport, R.I. 02841	1
7. Calvin Dunlap Naval Postgraduate School Code 68Du Monterey, Ca. 93943	1
8. Dr. George Kerr Naval Oceanographic and Research Activity Bay St. Louis, Ms. 39529	1
9. Robert McGirr Naval Oceanographic and Research Activity Bay St. Louis, Ms. 39529	1
10. CDR R. Hillyer Chief of Naval Operations Op-006 Wash. D.C. 20350-2000	1

- | | |
|---|---|
| 11. CDR R. Pentimonte
Commander, Naval Oceanographic Command
N311
Bay St. Louis, Ms. 39529 | 1 |
| 12. Research Administration
Naval Postgraduate School
Code 012
Monterey, Ca. 93943-5002 | 1 |
| 13. Lt. K. L. Cease
Box 7
Naval Facility
FPO NY 09571-0407 | 1 |

DUDLEY B. BOK JANUARY
NAVAL POSTGRADUATE SCHOOL
MONTEREY, CALIFORNIA 94064-5002

Thesis
C338343 Cease
c.1

A horizontal spatial
requirement study of the
Gulf Stream as modelled
by the IFDPE acoustic
model.

Thesis
C338343 Cease
c.1

A horizontal spatial
requirement study of the
Gulf Stream as modelled
by the IFDPE acoustic
model.

thesC338343
A horizontal spatial requirement study o



3 2768 000 72890 1
DUDLEY KNOX LIBRARY